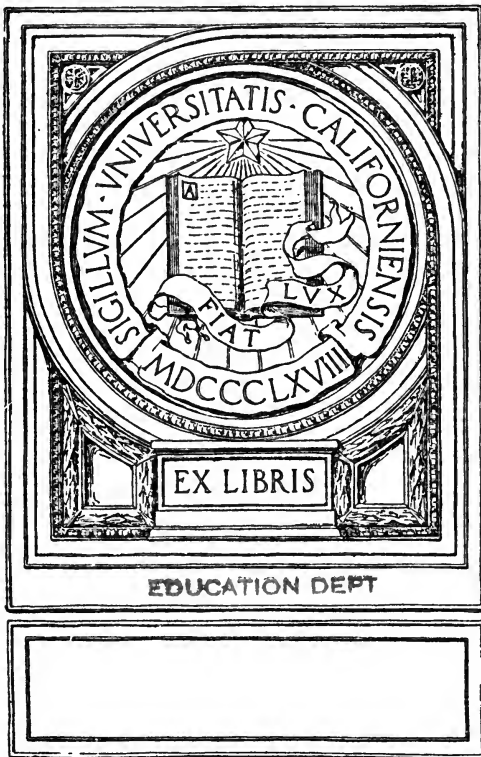


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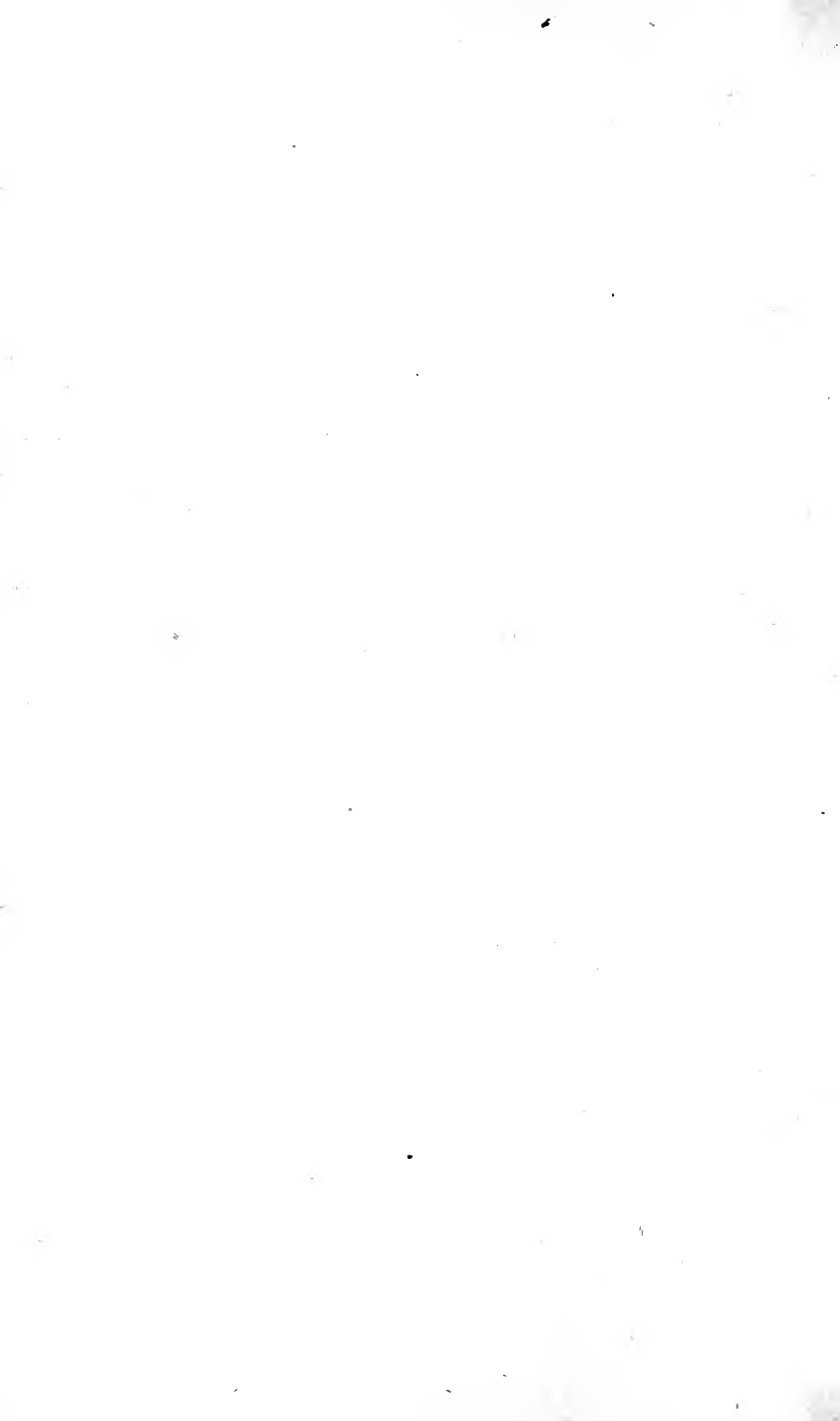


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ELEMENTS

OF

PLANE AND SPHERICAL

TRIGONOMETRY,

WITH

NUMEROUS PRACTICAL PROBLEMS.

BY

HORATIO N. ROBINSON, ELL.D

AUTHOR OF A FULL COURSE OF MATHEMATICS.

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## NOTICE.



Upon the suggestion of many Teachers, the Publishers have thought best to bind in a *separate* volume this Treatise on Plane and Spherical Trigonometry; continuing, however, as heretofore, to bind it up with Robinson's New Geometry, in one volume.

In this form it will be more convenient, and less expensive for those Teachers and Students who do not wish to take up the Geometry in connection with it, or who desire to use this Treatise on Trigonometry and some other author on Geometry.

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# TRIGONOMETRY

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## PART I.

### PLANE TRIGONOMETRY.

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#### SECTION I.

##### ELEMENTARY PRINCIPLES.

TRIGONOMETRY, in its literal and restricted sense, has for its object the measurement of triangles. When it treats of plane triangles it is called *Plane Trigonometry*. In a more enlarged sense, trigonometry is the science which investigates the relations of all possible arcs of the circumference of a circle to certain straight lines, termed *trigonometrical lines* or *circular functions*, connected with and dependent on such arcs, and the relations of these trigonometrical lines to each other.

The measure of an angle is the arc of a circle intercepted between the two lines which form the angle—the center of the arc always being at the point where the two lines meet.

The arc is measured by *degrees*, *minutes*, and *seconds*; there being 360 degrees to the whole circle, 60 minutes in one degree, and 60 seconds in one minute. Degrees, minutes, and seconds, are designated by °, ', '' ; thus, 27° 14' 21'', is read 27 degrees 14 minutes 21 seconds.

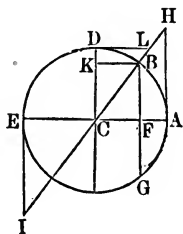
The circumferences of all circles contain the same number of degrees, but the greater the radius the greater

is the absolute length of a degree. The circumference of a carriage wheel, the circumference of the earth, or the still greater and indefinite circumference of the heavens, has the same number of degrees; yet the same number of degrees in each and every circumference is the measure of precisely the same angle.

## DEFINITIONS.

1. The Complement of an arc is  $90^\circ$  minus the arc.
2. The Supplement of an arc is  $180^\circ$  minus the arc.
3. The Sine of an angle, or of an arc, is a line drawn from one end of an arc, perpendicular to a diameter drawn through the other end. Thus,  $BF$  is the sine of the arc  $AB$ , and also of the arc  $BDE$ .  $BK$  is the sine of the arc  $BD$ .

4. The Cosine of an arc is the perpendicular distance from the center of the circle to the sine of the arc; or, it is the same in magnitude as the sine of the complement of the arc. Thus,  $CF$  is the cosine of the arc  $AB$ ; but  $CF = KB$ , which is the sine of  $BD$ .



5. The Tangent of an arc is a line touching the circle in one extremity of the arc, and continued from thence, to meet a line drawn through the center and the other extremity. Thus,  $AH$  is the tangent to the arc  $AB$ , and  $DL$  is the tangent of the arc  $DB$ .

6. The Cotangent of an arc is the tangent of the complement of the arc. Thus,  $DL$ , which is the tangent of the arc  $DB$ , is the cotangent of the arc  $AB$ .

REMARK.—The *co* is but a contraction of the word complement.

7. The Secant of an arc is a line drawn from the center of the circle to the extremity of the tangent. Thus,  $CH$  is the secant of the arc  $AB$ , or of its supplement  $BDE$ .

8. The Cosecant of an arc is the secant of the complement. Thus,  $CL$ , the secant of  $BD$ , is the cosecant of  $AB$ .

9. The **Versed Sine** of an arc is the distance from the extremity of the arc to the foot of the sine. Thus,  $AF$  is the versed sine of the arc  $AB$ , and  $DK$  is the versed sine of the arc  $DB$ .

For the sake of brevity, these technical terms are contracted thus: for sine  $AB$ , we write *sin.*  $AB$ ; for cosine  $AB$ , we write *cos.*  $AB$ ; for tangent  $AB$ , we write *tan.*  $AB$ , etc.

From the preceding definitions we deduce the following obvious consequences:

1st. That when the arc  $AB$  becomes insensibly small, or zero, its sine, tangent, and versed sine are also nothing, and its secant and cosine are each equal to radius.

2d. The sine and versed sine of a quadrant are each equal to the radius; its cosine is zero, and its secant and tangent are infinite.

3d. The chord of an arc is twice the sine of one half the arc. Thus, the chord,  $BG$ , is double the sine,  $BF$ .

4th. The versed sine is equal to the difference between the radius and the cosine.

5th. The sine and cosine of any arc form the two sides of a right-angled triangle, which has a radius for its hypotenuse. Thus,  $CF$  and  $FB$  are the two sides of the right-angled triangle,  $CFB$ .

Also, the radius and tangent always form the two sides of a right-angled triangle, which has the secant of the arc for its hypotenuse. This we observe from the right-angled triangle,  $CAH$ .

To express these relations analytically, we write

$$\sin.^2 + \cos.^2 = R^2 \quad (1)$$

$$R^2 + \tan.^2 = \sec.^2 \quad (2)$$

From the two equiangular triangles  $CFB$ ,  $CAH$ , we have

$$CF : FB = CA : AH.$$



That is,

$$\cos. : \sin. = R : \tan.; \text{ whence, } \tan. = \frac{R \cdot \sin.}{\cos.} \quad (3)$$

Also,  $CF : CB = CA : CH.$

That is,

$$\cos. : R = R : \sec.; \text{ whence, } \cos. \sec. = R^2. \quad (4)$$

The two equiangular triangles,  $CAH$  and  $CDL$ , give

$$CA : AH = DL : DC.$$

That is,

$$R : \tan. = \cot. : R; \text{ whence, } \tan. \cot. = R^2. \quad (5)$$

Also,  $CF : FB = DL : DC.$

That is,

$$\cos. : \sin. = \cot. : R; \text{ whence, } \cos. R = \sin. \cot. \quad (6)$$

From equations (4) and (5), we have

$$\cos. \sec. = \tan. \cot. \quad (7)$$

Or,  $\cos. : \tan. = \cot. : \sec.$

We also have  $\text{ver. sin.} = R - \cos. \quad (8)$

The *ratios* between the various trigonometrical lines are always the same for arcs of the same number of degrees, whatever be the length of the radius; and we may, therefore, assume radius of any length to suit our convenience. The preceding equations will be more concise, and more readily applied, by making the radius equal unity. This supposition being made, we have, for equations 1 to 6, inclusive,

$$\sin.^2 + \cos.^2 = 1. \quad (1)$$

$$1 + \tan.^2 = \sec.^2 \quad (2)$$

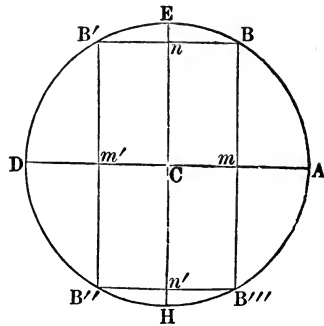
$$\tan. = \frac{\sin.}{\cos.} \quad (3) \quad \cos. = \frac{1}{\sec.} \quad (4)$$

$$\tan. = \frac{1}{\cot.} \quad (5) \quad \cos. = \sin. \cot. \quad (6)$$

Let the circumference,  $AEDH$ , be divided into four equal parts by the diameters,  $AD$  and  $EH$ , the one hori-

zontal and the other vertical. These equal parts are called *quadrants*, and they may be distinguished as the *first, second, third,* and *fourth* quadrants.

The center of the circle is taken as the origin of distances, or the zero point, and the different directions in which distances are esti-



mated from this point are indicated by the signs  $+$  and  $-$ . If those from  $C$  to the right be marked  $+$ , those from  $C$  to the left must be marked  $-$ ; and if distances from  $C$  upwards be considered plus, those from  $C$  downwards must be considered minus.

If one extremity of a varying arc be constantly at  $A$ , and the other extremity fall successively in each of the several quadrants, we may readily determine, by the above rule, the algebraic signs of the sines and cosines of all arcs from  $0^\circ$  to  $360^\circ$ . Now, since all other trigonometrical lines can be expressed in terms of the sine and cosine, it follows that the algebraic signs of all the circular functions result from those of the sine and cosine.

We shall thus find for arcs terminating in the

	sin.	cos.	tan.	cot.	sec.	cosec.	vers.
1st quadrant,	+	+	+	+	+	+	+
2d "	+	-	-	-	-	+	+
3d "	-	-	+	+	-	-	+
4th "	-	+	-	-	+	-	+

#### PROPOSITION 1.

*The chord of  $60^\circ$  and the tangent of  $45^\circ$  are each equal to radius; the sine of  $30^\circ$ , the versed sine of  $60^\circ$ , and the cosine of  $60^\circ$  are each equal to one half the radius.*



of the chord, let fall the perpendiculars  $FM$ ,  $EP$ , and  $IN$ , on the radius  $GC$ . Also draw  $DO$ , the sine of the arc  $CD$ , and let fall the perpendiculars  $IHH$  on  $FM$ , and  $EK$  on  $IN$ .

Now, by the definition of sines and cosines,  $DO = \sin.a$ ;  $GO = \cos.a$ ;  $FI = \sin.b$ ;  $GI = \cos.b$ . We are to find

$$FM = \sin.(a + b); \quad GM = \cos.(a + b);$$

$$EP = \sin.(a - b); \quad GP = \cos.(a - b).$$

Because  $IN$  is parallel to  $DO$ , the two  $\Delta$ 's,  $GDO$ ,  $GIN$ , are equiangular and similar. Also, the  $\Delta FHI$  is similar to the  $\Delta GIN$ ; for the angles,  $FIG$  and  $HIN$ , are right angles; from these two equals, taking away the common angle  $HIL$ , we have the angle  $FIIH =$  the angle  $GIN$ . The angles at  $H$  and  $N$  are right angles; therefore, the  $\Delta$ 's  $FHI$ ,  $GIN$ , and  $GDO$ , are equiangular and similar; and the side  $HI$  is homologous to  $IN$  and  $DO$ .

Again, as  $FI = IE$ , and  $IK$  is parallel to  $FM$ ,

$$FH = IK, \text{ and } HI = KE.$$

By similar triangles we have

$$GD : DO = GI : IN.$$

$$\text{That is, } R : \sin.a = \cos.b : IN; \text{ or, } IN = \frac{\sin.a \cos.b}{R}. \quad (1)$$

$$\text{Also, } GD : GO = FI : FH.$$

$$\text{That is, } R : \cos.a = \sin.b : HF; \text{ or, } FH = \frac{\cos.a \sin.b}{R}. \quad (2)$$

$$\text{Also, } GD : GO = GI : GN.$$

$$\text{That is, } R : \cos.a = \cos.b : GN; \text{ or, } GN = \frac{\cos.a \cos.b}{R}. \quad (3)$$

$$\text{Also, } GD : DO = FI : IH.$$

$$\text{That is, } R : \sin.a = \sin.b : IH; \text{ or, } IH = \frac{\sin.a \sin.b}{R}. \quad (4)$$

By adding the first and second of these equations, we have

$$IN + FH = FM = \sin.(a + b).$$

That is,  $\sin.(a + b) = \frac{\sin.a \cos.b + \cos.a \sin.b}{R}$ .

By subtracting the second from the first, since

$$IN - FH = IN - IK = EP, \text{ we have}$$

$$\sin.(a - b) = \frac{\sin.a \cos.b - \cos.a \sin.b}{R}$$

By subtracting the fourth from the third, we have

$$GN - IH = GM = \cos.(a + b) \text{ for the first member.}$$

Hence,  $\cos.(a + b) = \frac{\cos.a \cos.b - \sin.a \sin.b}{R}$ . (5)

By adding the third and fourth, we have

$$GN + IH = GN + NP = GP = \cos.(a - b).$$

Hence,  $\cos.(a - b) = \frac{\cos.a \cos.b + \sin.a \sin.b}{R}$ . (6)

Collecting these four expressions, and considering the *ca* lius unity, we have *End*

$$(A) \begin{cases} \sin.(a + b) = \sin.a \cos.b + \cos.a \sin.b & (7) \\ \sin.(a - b) = \sin.a \cos.b - \cos.a \sin.b & (8) \\ \cos.(a + b) = \cos.a \cos.b - \sin.a \sin.b & (9) \\ \cos.(a - b) = \cos.a \cos.b + \sin.a \sin.b & (10) \end{cases}$$

Formulae (A) accomplish the objects of the proposition, and from these equations many useful and important deductions can be made. The following are the most essential:

By adding (7) to (8), we have (11); subtracting (8) from (7) gives (12). Also, (9) added to (10) gives (13), (9) taken from (10) gives (14).

$$(B) \begin{cases} \sin.(a + b) + \sin.(a - b) = 2\sin.a \cos.b & (11) \\ \sin.(a + b) - \sin.(a - b) = 2\cos.a \sin.b & (12) \\ \cos.(a + b) + \cos.(a - b) = 2\cos.a \cos.b & (13) \\ \cos.(a - b) - \cos.(a + b) = 2\sin.a \sin.b & (14) \end{cases}$$

If we put  $a + b = A$ , and  $a - b = B$ , then (11) becomes (15), (12) becomes (16), (13) becomes (17), and (14) becomes (18).

$$(C) \begin{cases} \sin.A + \sin.B = 2\sin.\left(\frac{A+B}{2}\right)\cos.\left(\frac{A-B}{2}\right) & (15) \\ \sin.A - \sin.B = 2\cos.\left(\frac{A+B}{2}\right)\sin.\left(\frac{A-B}{2}\right) & (16) \\ \cos.A + \cos.B = 2\cos.\left(\frac{A+B}{2}\right)\cos.\left(\frac{A-B}{2}\right) & (17) \\ \cos.B - \cos.A = 2\sin.\left(\frac{A+B}{2}\right)\sin.\left(\frac{A-B}{2}\right) & (18) \end{cases}$$

If we divide (15) by (16), (observing that  $\frac{\sin.}{\cos.} = \tan.$ , and  $\frac{\cos.}{\sin.} = \cot. = \frac{1}{\tan.}$  as we learn by equations (6) and (5), we shall have

$$\frac{\sin.A + \sin.B}{\sin.A - \sin.B} = \frac{\sin.\left(\frac{A+B}{2}\right)\cos.\left(\frac{A-B}{2}\right)\tan.\left(\frac{A+B}{2}\right)}{\cos.\left(\frac{A+B}{2}\right)\sin.\left(\frac{A-B}{2}\right)\tan.\left(\frac{A-B}{2}\right)} \quad (19)$$

Whence,

$$\sin.A + \sin.B : \sin.A - \sin.B = \tan.\left(\frac{A+B}{2}\right) : \tan.\left(\frac{A-B}{2}\right)$$

That is: *The sum of the sines of any two arcs is to the difference of the same sines, as the tangent of one half the sum of the same arcs is to the tangent of one half their difference.*

By operating in the same way with the different equations in formulæ (C), we find,

$$(D) \begin{cases} \frac{\sin.A + \sin.B}{\cos.A + \cos.B} = \tan.\left(\frac{A+B}{2}\right) & (20) \\ \frac{\sin.A + \sin.B}{\cos.B - \cos.A} = \cot.\left(\frac{A-B}{2}\right) & (21) \\ \frac{\sin.A - \sin.B}{\cos.A + \cos.B} = \tan.\left(\frac{A-B}{2}\right) & (22) \\ \frac{\sin.A - \sin.B}{\cos.B - \cos.A} = \cot.\left(\frac{A+B}{2}\right) & (23) \\ \frac{\cos.A + \cos.B}{\cos.B - \cos.A} = \frac{\cot.\left(\frac{A+B}{2}\right)}{\tan.\left(\frac{A-B}{2}\right)} & (24) \end{cases}$$

These equations are all true, whatever be the value of the arcs designated by  $A$  and  $B$ ; we may, therefore, assign any possible value to either of them, and if in equations (20), (21), and (24), we make  $B = 0$ , we shall have,

$$\frac{\sin.A}{1 + \cos.A} = \tan.\frac{A}{2} = \frac{1}{\cot.\frac{1}{2}A} \quad (25)$$

$$\textcircled{a} \quad \frac{\sin.A}{1 - \cos.A} = \cot.\frac{A}{2} = \frac{1}{\tan.\frac{1}{2}A} \quad (26)$$

$$\frac{1 + \cos.A}{1 - \cos.A} = \frac{\cot.\frac{1}{2}A}{\tan.\frac{1}{2}A} = \frac{1}{\tan^2.\frac{1}{2}A} \quad (27)$$

If we now turn back to formulæ ( $A$ ), and divide equation (7) by (9), and (8) by (10), observing at the same time that  $\frac{\sin.}{\cos.} = \tan.$ , we shall have,

$$\tan.(a + b) = \frac{\sin.a \cos.b + \cos.a \sin.b}{\cos.a \cos.b - \sin.a \sin.b}$$

$$\tan.(a - b) = \frac{\sin.a \cos.b - \cos.a \sin.b}{\cos.a \cos.b + \sin.a \sin.b}$$

By dividing the numerators and denominators of the second members of these equations by  $(\cos.a \cos.b)$ , we find,

$$\tan.(a + b) = \frac{\frac{\sin.a \cos.b}{\cos.a \cos.b} + \frac{\cos.a \sin.b}{\cos.a \cos.b}}{\frac{\cos.a \cos.b}{\cos.a \cos.b} - \frac{\sin.a \sin.b}{\cos.a \cos.b}} = \frac{\tan.a + \tan.b}{1 - \tan.a \tan.b} \quad (28)$$

$$\tan.(a - b) = \frac{\frac{\sin.a \cos.b}{\cos.a \cos.b} - \frac{\cos.a \sin.b}{\cos.a \cos.b}}{\frac{\cos.a \cos.b}{\cos.a \cos.b} + \frac{\sin.a \sin.b}{\cos.a \cos.b}} = \frac{\tan.a - \tan.b}{1 + \tan.a \tan.b} \quad (29)$$

If in equation (11), formulæ ( $B$ ), we make  $a = b$ , we shall have,

$$\sin.2a = 2\sin.a \cos.a \quad (30)$$

Making the same hypothesis in equation (13), gives,

$$\cos.2a + 1 = 2\cos^2.a \quad (31)$$

The same hypothesis reduces equation (14) to

$$1 - \cos.2a = 2\sin^2.a \quad (32)$$

The same hypothesis reduces equation (28) to

$$\tan.2a = \frac{2\tan.a}{1 - \tan^2.a} \quad (33)$$

If we substitute  $a$  for  $2a$  in (31) and (32), we shall have

$$1 + \cos.a = 2\cos.^2\frac{1}{2}a. \quad (34)$$

$$\text{and } 1 - \cos.a = 2\sin.^2\frac{1}{2}a. \quad (35)$$

### PROPOSITION III.

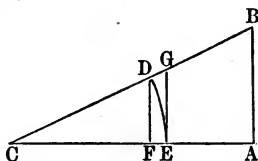
*In any right-angled plane triangle, we may have the following proportions :*

1st. *The hypotenuse is to either side, as the radius is to the sine of the angle opposite to that side.*

2d. *One side is to the other side, as the radius is to the tangent of the angle adjacent to the first side.*

3d. *One side is to the hypotenuse, as the radius is to the secant of the angle adjacent to that side.*

Let  $CAB$  represent any right-angled triangle, right-angled at  $A$ .



(Here, and in all cases hereafter, we shall represent the angles of a triangle by the large letters  $A, B, C$ , and the sides opposite to them, by the small letters  $a, b, c$ .)

From either acute angle, as  $C$ , take any distance, as  $CD$ , greater or less than  $CB$ , and describe the arc  $DE$ . This arc measures the angle  $C$ . From  $D$ , draw  $DF$  parallel to  $BA$ ; and from  $E$ , draw  $EG$ , also parallel to  $BA$  or  $DF$ .

By the definitions of sines, tangents, secants, etc,  $DF$  is the sine of the angle  $C$ ;  $EG$  is the tangent,  $CG$  the secant, and  $CF$  the cosine.



Now, by proportional triangles we have,

$$CB : BA = CD : DF \quad \text{or, } a : c = R : \sin.C$$

$$CA : AB = CE : EG \quad \text{or, } b : c = R : \tan.C$$

$$CA : CB = CE : CG \quad \text{or, } b : a = R : \sec.C$$

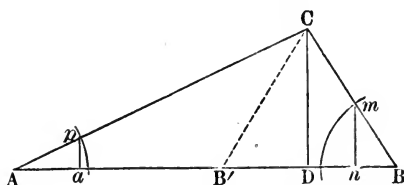
Hence the proposition.

SCHOLIUM.—If the hypotenuse of a triangle is made radius, one side is the sine of the angle opposite to it, and the other side is the cosine of the same angle. This is obvious from the triangle  $CDF$ .

#### PROPOSITION IV.

*In any triangle, the sines of the angles are to one another as the sides opposite to them.*

Let  $ABC$  be any triangle. From the points  $A$  and  $B$ , as centers, with any radius, describe the arcs measuring these angles, and draw  $pa$ ,  $CD$ , and  $mn$ , perpendicular to  $AB$ .



Then,  $pa = \sin.A$ , and  $mn = \sin.B$ .

By the similar  $\triangle$ 's,  $Apa$  and  $ACD$ , we have,

$$R : \sin.A = b : CD; \quad \text{or, } R(CD) = b \sin.A \quad (1)$$

By the similar  $\triangle$ 's,  $Bmn$  and  $BCD$ , we have,

$$R : \sin.B = a : CD; \quad \text{or, } R(CD) = a \sin.B \quad (2)$$

By equating the second members of equations (1) and (2)

$$b \sin.A = a \sin.B.$$

Hence,  $\sin.A : \sin.B = a : b$

Or,  $a : b = \sin.A : \sin.B.$

SCHOLIUM 1.—When either angle is  $90^\circ$ , its sine is radius.

SCHOLIUM 2.—When  $CB$  is less than  $AC$ , and the angle  $B$ , acute, the triangle is represented by  $ACB$ . When the angle  $B$  becomes  $B'$ , it is obtuse, and the triangle is  $ACB'$ ; but the proportion is equally

true with either triangle; for the angle  $CB'D = CBA$ , and the sine of  $CB'D$  is the same as the sine of  $AB'C$ . In practice we can determine which of these triangles is proposed, by the side  $AB$  being greater or less than  $AC$ ; or, by the angle at the vertex  $C$  being large, as  $ACB$ , or small, as  $ACB'$ .

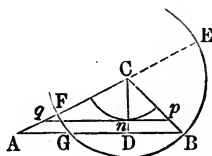
In the solitary case in which  $AC$ ,  $CB$ , and the angle  $A$ , are given, and  $CB$  less than  $AC$ , we can determine both of the  $\Delta$ 's  $ACB$  and  $ACB'$ ; and then we surely have the right one.

### PROPOSITION V.

*If from any angle of a triangle, a perpendicular be let fall on the opposite side, or base, the tangents of the segments of the angle are to each other as the segments of the base.*

Let  $ABC$  be the triangle. Let fall the perpendicular  $CD$ , on the side  $AB$ .

Take any radius, as  $Cn$ , and describe the arc which measures the angle  $C$ . From  $n$ , draw  $qnp$  parallel to  $AB$ . Then it is obvious that  $np$  is the tangent of the angle  $DCB$ , and  $nq$  is the tangent of the angle  $ACD$ .



Now, by reason of the parallels  $AB$  and  $qp$ , we have,

$$qn : np = AD : DB$$

That is,  $\tan.ACD : \tan.DCB = AD : DB$ .

### PROPOSITION VI.

*If a perpendicular be let fall from any angle of a triangle to its opposite side or base, this base is to the sum of the other two sides, as the difference of the sides is to the difference of the segments of the base.*

(See figure to Proposition 5.)

Let  $AB$  be the base, and from  $C$ , as a center, with the shorter side as radius, describe the circle, cutting  $AB$  in  $G$ , and  $AC$  in  $F$ ; produce  $AC$  to  $E$ .

It is obvious that  $AE$  is the sum of the sides  $AC$  and  $CB$ , and  $AF$  is their difference.

Also,  $AD$  is one segment of the base made by the perpendicular, and  $BD = DG$  is the other; therefore, the difference of the segments is  $AG$ .

As  $A$  is a point without a circle, by Cor. Th. 18, B. III, we have

$$AE \times AF = AB \times AG$$

Hence,  $AB : AE = AF : AG.$

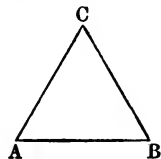
### PROPOSITION VII.

*The sum of any two sides of a triangle is to their difference, as the tangent of one half the sum of the angles opposite to these sides, is to the tangent of one half their difference.*

Let  $ABC$  be any plane triangle.  
Then, by Proposition 4, we have,

$$BC : AC = \sin.A : \sin.B.$$

Hence,



$$BC + AC : BC - AC = \sin.A + \sin.B : \sin.A - \sin.B \text{ (Th. 9, B. II).}$$

But,

$$\tan. \left( \frac{A + B}{2} \right) : \tan. \left( \frac{A - B}{2} \right) = \sin.A + \sin.B : \sin.A - \sin.B, \text{ (eq. (19), Trig.)}$$

Comparing the two latter proportions, (Th. 6, B. II), we have,

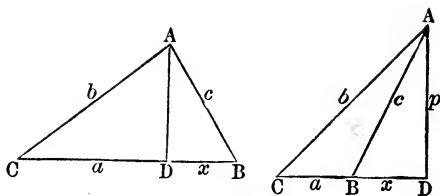
$$BC + AC : BC - AC = \tan. \left( \frac{A + B}{2} \right) : \tan. \left( \frac{A - B}{2} \right)$$

Hence the proposition.

### PROPOSITION VIII.

*Given, the three sides of any plane triangle, to find some relation which they must bear to the sines and cosines of the respective angles.*

Let  $ABC$  be the triangle, and let the perpendicular fall either upon, or without the base, as shown in the figures.



By recurring to Th. 41, B. I, we shall find

$$CD = \frac{a^2 + b^2 - c^2}{2a}. \quad (1)$$

Now, by Proposition 3, we have

$$R : \cos. C = b : CD.$$

Therefore, 
$$CD = \frac{b \cos. C}{R}. \quad (2)$$

Equating these two values of  $CD$ , and reducing, we have

$$\cos. C = \frac{R(a^2 + b^2 - c^2)}{2ab}. \quad (m)$$

In this expression we observe, that the part  $c$ , whose square is found in the numerator with the minus sign, is the side opposite to the angle; and that the denominator is twice the rectangle of the sides adjacent to the angle. From these observations we at once draw the following expressions for the cosine  $A$ , and cosine  $B$ :

$$\cos. A = \frac{R(b^2 + c^2 - a^2)}{2bc}. \quad (n)$$

$$\cos. B = \frac{R(a^2 + c^2 - b^2)}{2ac}. \quad (p)$$

As these expressions are not convenient for logarithmic computation, we modify them as follows:

If we put  $2a = A$ , in equation (31), we have

$$\cos. A + 1 = 2\cos.^2 \frac{1}{2}A.$$

In the preceding expression, (n), if we consider radius unity, and add 1 to both members, we shall have

$$\cos. A + 1 = 1 + \frac{b^2 + c^2 - a^2}{2bc}.$$

$$\begin{aligned} \text{Therefore, } 2\cos.^2 \frac{1}{2}A &= \frac{2bc + b^2 + c^2 - a^2}{2bc} \\ &= \frac{(b + c)^2 - a^2}{2bc}. \end{aligned}$$

Considering  $b + c$  as one quantity, and observing that  $(b + c)^2 - a^2$  is the difference of *two squares*, we have

$$(b + c)^2 - a^2 = (b + c + a)(b + c - a); \text{ but } (b + c - a) = b + c + a - 2a.$$

$$\text{Hence, } 2\cos.^2 \frac{1}{2}A = \frac{(b + c + a)(b + c + a - 2a)}{2bc}.$$

$$\text{Or, } \cos.^2 \frac{1}{2}A = \frac{\left(\frac{b + c + a}{2}\right) \left(\frac{b + c + a}{2} - a\right)}{bc}.$$

By putting  $\frac{a + b + c}{2} = s$ , and extracting square root, the final result for radius unity is

$$\cos. \frac{1}{2}A = \sqrt{\frac{s(s - a)}{bc}}.$$

For any other radius we must write

$$\cos. \frac{1}{2}A = \sqrt{\frac{R^2 s(s - a)}{bc}}.$$

$$\text{By inference, } \cos. \frac{1}{2}B = \sqrt{\frac{R^2 s(s - b)}{ac}}.$$

$$\text{Also, } \cos. \frac{1}{2}C = \sqrt{\frac{R^2 s(s - c)}{ab}}.$$

In every triangle, the sum of the three angles is equal to  $180^\circ$ ; and if one of the angles is small, the other two must be comparatively large; if two of them are small, the third one must be large. The greater angle is always opposite the greater side; hence, by merely inspecting the given sides, any person can decide at once which is the greater angle; and of the three pre-

ceding equations, *that one* should be taken which applies to the greater angle, whether that be the particular angle required or not; because the equations bring out the *cosines* to the angles; and the cosines to very small arcs vary so slowly, that it may be impossible to decide, with sufficient numerical accuracy, to what particular arc the cosine belongs. For instance, the cosine 9.999999, carried to the table, applies to several arcs; and, of course, we should not know which one to take; but this difficulty does not exist when the angle is large; therefore, compute the largest angle first, and then compute the other angles by Proposition 4.

But we can deduce an expression for the sine of any of the angles, as well as the cosine. It is done as follows:

#### EQUATIONS FOR THE SINES OF THE ANGLES.

Resuming equation (*m*), and considering radius unity, we have

$$\cos. C = \frac{a^2 + b^2 - c^2}{2ab}.$$

Subtracting each member of this equation from unity, gives

$$1 - \cos. C = 1 - \left( \frac{a^2 + b^2 - c^2}{2ab} \right). \quad (1)$$

Make  $2a = C$ , in equation (32); then  $a = \frac{1}{2}C$ ,

and  $1 - \cos. C = 2\sin.^2 \frac{1}{2}C$ . (2)

Equating the second members of (1) and (2),

$$\begin{aligned} 2\sin.^2 \frac{1}{2}C &= \frac{2ab - a^2 - b^2 + c^2}{2ab} \\ &= \frac{c^2 - (a - b)^2}{2ab} \\ &= \frac{(c + b - a)(c + a - b)}{2ab}. \end{aligned}$$

$$\text{Or, } \sin. \frac{1}{2}C = \frac{\left(\frac{c+b-a}{2}\right) \left(\frac{c+a-b}{2}\right)}{ab}.$$

$$\text{But, } \frac{c+b-a}{2} = \frac{c+b+a}{2} - a, \text{ and } \frac{c+a-b}{2} = \frac{c+a+b}{2} - b.$$

$$\text{Put } \frac{a+b+c}{2} = s, \text{ as before; then,}$$

$$\sin. \frac{1}{2}C = \sqrt{\frac{(s-a)(s-b)}{ab}}.$$

By taking equation (p), and proceeding in the same manner, we have

$$\sin. \frac{1}{2}B = \sqrt{\frac{(s-a)(s-c)}{ac}}.$$

$$\text{From (n), } \sin. \frac{1}{2}A = \sqrt{\frac{(s-b)(s-c)}{cb}}.$$

The preceding results are for radius unity; for any other radius, we must multiply by the number of units in such radius. For the radius of the tables we write  $R$ ; and if we put it under the radical sign, we must write  $R^2$ ; hence, for the sines corresponding with our logarithmic table, we must write the equations thus,

$$\sin. \frac{1}{2}A = \sqrt{\frac{R^2(s-b)(s-c)}{bc}}.$$

$$\sin. \frac{1}{2}B = \sqrt{\frac{R^2(s-a)(s-c)}{ac}}.$$

$$\sin. \frac{1}{2}C = \sqrt{\frac{R^2(s-a)(s-b)}{ab}}.$$

A large angle should not be determined by these equations, for the same reason that a small angle should not be determined from an equation expressing the cosine.

In practice, the equations for cosine are more generally used, because more easily applied.

The formulæ which we have thus analytically developed, express nearly all the important relations between the sines, cosines, and tangents of arcs or angles; and we have also demonstrated all the theorems required for the determination of the unknown parts of any plane triangle, three of the parts of which are given, one at least being a side.

Such relations might be indefinitely multiplied, but those already established are sufficient for most practical purposes, and when others are required, no difficulty will be found in deducing them from these.

The following geometrical demonstrations of many of the preceding relations, are offered, in the belief that they will prove useful disciplinary exercises to the student.

1st. Let the arc  $AD = A$ ; then  $DG = \sin. A$ ;  $CG = \cos. A$ ,  
 $DI = \sin. \frac{1}{2} A$ ;  $AD = 2 \sin. \frac{1}{2} A$ ;  $CI = \cos. \frac{1}{2} A$ ;  
 $CI = DO$ ; and  $DB = 2DO = 2 \cos. \frac{1}{2} A$ .

The angle,  $DBA$ , is measured by one half the arc  $AD$ ; that is, by  $\frac{1}{2} A$ .

Also,  $ADG = DBA = \frac{1}{2} A$ .

Now, in the triangle,  $BDG$ , we have

$$\sin. DBG : DG = \sin. 90^\circ : BD.$$

That is,  $\sin. \frac{1}{2} A : \sin. A = 1 : 2 \cos. \frac{1}{2} A$ .

Or,  $\sin. A = 2 \sin. \frac{1}{2} A \cos. \frac{1}{2} A$ ;

which corresponds to equation (30).

In the same triangle,

$\sin. 90^\circ \cdot BD = \sin. BDG : BG$ ; and  $\sin. BDG = \cos. DBG$

That is,  $1 : 2 \cos. \frac{1}{2} A = \cos. \frac{1}{2} A : 1 + \cos. A$ .

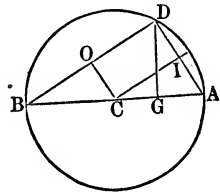
Or,  $2 \cos.^2 \frac{1}{2} A = 1 + \cos. A$ , same as equation (34).

In the triangle,  $DGA$ , we have,

$$\sin. 90^\circ : AD = \sin. GDA : GA.$$

That is,  $1 : 2 \sin. \frac{1}{2} A = \sin. \frac{1}{2} A : 1 - \cos. A$ .

Or,  $2 \sin.^2 \frac{1}{2} A = 1 - \cos. A$ , same as equation (35).





By similar triangles, we have,

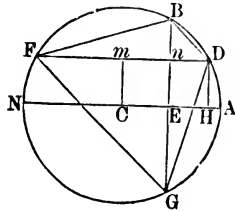
$$BA : AD = AD : AG.$$

That is,  $2 : 2\sin.\frac{1}{2}A = 2\sin.\frac{1}{2}A : \text{versed } \sin.A.$

Or,  $\text{versed } \sin.A = 2\sin.^2 \frac{1}{2}A.$

2d. From  $C$  as the center, with  $CA$  as the radius,

describe a circle. Take any arc,  $AB$ , and call it  $A$ ; and  $AD$  a less arc, and call it  $B$ ; then  $BD$  is the difference of the two arcs, and must be designated by  $(A-B)$ ; arc  $AG = \text{arc } AB$ ; therefore,



arc  $DG = A + B$ ;  $EG = \sin.A$ ;

$$En = \sin.B; Gn = \sin.A + \sin.B;$$

$$Bn = \sin.A - \sin.B.$$

$$Fm = mD = CH = \cos.B; mn = \cos.A;$$

therefore,  $Fm + mn = \cos.A + \cos.B = Fn$ ;

$$mD - mn = \cos.B - \cos.A = nD;$$

and  $DG = 2\sin.\left(\frac{A+B}{2}\right).$

Because,  $NF = AD$ ;  $AB + NF = A + B$ ;

therefore,  $180^\circ - (A + B) = \text{arc } FB$ ;

or,  $90^\circ - \left(\frac{A+B}{2}\right) = \frac{1}{2}\text{arc } FB.$

But the chord,  $FB$ , is twice the sine of  $\frac{1}{2}$  arc  $FB$ ;

that is,  $FB = 2\sin.\left(90^\circ - \frac{A+B}{2}\right) = 2\cos.\left(\frac{A+B}{2}\right).$

The  $\sphericalangle nGD = \sphericalangle BFD$ , because both are measured by one half of the arc  $BD$ ; that is, by  $\left(\frac{A-B}{2}\right)$ , and the two triangles,  $GnD$  and  $FnB$ , are similar.

The angle,  $GFn$ , is measured by  $\left(\frac{A+B}{2}\right).$

In the triangle,  $FBG$ ,  $Fn$  is drawn from an angle per

pendicular to the opposite side; therefore, by Proposition 5, we have,

$$Gn : nB = \tan. GFn : \tan. BFn.$$

That is,  $\sin. A + \sin. B : \sin. A - \sin. B = \tan. \left( \frac{A+B}{2} \right) : \tan. \left( \frac{A-B}{2} \right)$ . This is equation (19). Q.E.D.

In the triangle,  $GnD$ , we have,

$$\sin. 90^\circ : DG = \sin. nDG : Gn; \sin. nDG = \cos. nGD.$$

That is,  $1 : 2\sin. \left( \frac{A+B}{2} \right) = \cos. \left( \frac{A-B}{2} \right) : \sin. A + \sin. B$ .

Or,  $\sin. A + \sin. B = 2\sin. \left( \frac{A+B}{2} \right) \cos. \left( \frac{A-B}{2} \right)$ ,

the same as equation (15).

3d. In the triangle,  $FnB$ , we have,

$$\sin. 90 : FB = \sin. BFn : Bn.$$

That is,  $1 : 2\cos. \left( \frac{A+B}{2} \right) = \sin. \left( \frac{A-B}{2} \right) : \sin. A - \sin. B$ .

Or,  $\sin. A - \sin. B = 2\cos. \left( \frac{A+B}{2} \right) \sin. \left( \frac{A-B}{2} \right)$ ,

the same as equation (16).

4th. In the triangle,  $FBn$ , we have,

$$\sin. 90 : FB = \cos. BFn : Fn.$$

That is,  $1 : 2\cos. \left( \frac{A+B}{2} \right) = \cos. \left( \frac{A-B}{2} \right) : \cos. A + \cos. B$ .

Or,  $\cos. A + \cos. B = 2\cos. \left( \frac{A+B}{2} \right) \cos. \left( \frac{A-B}{2} \right)$ , the

same as equation (17).

5th. In the triangle,  $GnD$ , we have,

$$\sin. 90^\circ : GD = \sin. nGD : nD.$$

That is,  $1 : 2\sin. \left( \frac{A+B}{2} \right) = \sin. \left( \frac{A-B}{2} \right) : \cos. B - \cos. A$ .

the same as equation (18).

6th. In the triangle,  $FGn$ , we have,

$$\sin. GFn : Gn = \cos. GFn : Fn.$$

That is,  $\sin. \frac{A+B}{2} : \sin. A + \sin. B = \cos. \frac{A+B}{2} : \cos. A + \cos. B$ .

Or,  $(\sin. A + \sin. B) \cos. \left(\frac{A+B}{2}\right) = (\cos. A + \cos. B) \sin. \left(\frac{A+B}{2}\right)$ .

Or,  $\frac{\sin. A + \sin. B}{\cos. A + \cos. B} = \frac{\sin. \frac{A+B}{2}}{\cos. \frac{A+B}{2}} = \tan. \left(\frac{A+B}{2}\right)$ , the

same as equation (20).

7th. In the triangle,  $FnB$ , we have,

$$Fn : nB :: 1 : \tan. BF_n.$$

That is,  $\cos. B + \cos. A : \sin. A - \sin. B :: 1 : \tan. \frac{1}{2}(A-B)$ .

Or,  $\frac{\sin. A - \sin. B}{\cos. A + \cos. B} = \tan. \left(\frac{A-B}{2}\right)$ , the same as equation (22).

8th. In the triangle,  $GnD$ , we have,

$$Gn : nD :: 1 : \tan. nGD.$$

That is,

$$\sin. A + \sin. B : \cos. B - \cos. A :: 1 : \tan. \left(\frac{A-B}{2}\right),$$

$$\text{or, } \frac{\cos. B - \cos. A}{\sin. A + \sin. B} = \tan. \left(\frac{A-B}{2}\right).$$

#### NATURAL SINES, COSINES, ETC.

When the radius of the circle is taken as the unit of measure, the numerical values of the trigonometrical lines belonging to the different arcs of the quadrant, become *natural* sines, cosines, etc. They are then, in fact, but numbers expressing the number of times that these lines contain the radius of the circle in which they are taken. The tables usually contain only the sines and cosines, because these are generally sufficient for practi-

cal purposes, and the others, when required, are readily expressed in terms of them.

We proceed to explain a method for computing a table of natural sines and cosines.

It was shown, in Book V, that the linear value of the arc  $180^\circ$ , in a circle whose radius is unity, is

$$3.141592653.$$

This divided by  $180 \times 60$ , the number of minutes in  $180^\circ$ , will give the length of one minute of arc, which is

$$.00029088820867.$$

But there can be no sensible difference between the length of the arc  $1'$  and its sine; and, within narrow limits, that sine will increase directly with the arc.

Hence,	$\sin. 1' = .0002908882.$
	$\sin. 2' = .0005817764.$
	$\sin. 3' = .0008726646.$
	$\sin. 4' = .0011635528.$
	$\sin. 5' = .0014544410.$
	$\sin. 6' = .0017453292.$
	$\sin. 7' = .0020362175.$
	$\sin. 8' = .0023271057.$
	$\sin. 9' = .0026179939.$
	$\sin. 10' = .0029088821.$

Beyond this, the error which would arise from taking the arc for its sine, upon which the above proceeds, would affect the final decimal figures; and we must, therefore, continue the computation of the series by other processes. To find the values of the cosines of arcs, from  $1'$  to  $10'$ , we have

$$\cos. = \sqrt{1 - \sin.^2} = 1 - \frac{1}{2} \sin.^2, \text{ nearly.}$$

That is, when the sines are very small fractions, as is the case for all arcs below  $10'$ , we can find the cosine by *subtracting one half of the square of the sine from unity.*

Whence,

cos. 1'	= .9999999577.
cos. 2'	= .9999998308.
cos. 3'	= .9999993204.
cos. 4'	= .99999932304.
cos. 5'	= .99999894290.
cos. 6'	= .99999847753.
cos. 7'	= .99999792735.
cos. 8'	= .9999973035.
cos. 9'	= .9999965730.
cos. 10'	= .9999957703.

The natural sines of arcs, differing by 1', from 10 up to 1°, may be computed from those of arcs less than 10', by means of equation (11), group B, which is

$$\sin. (a + b) = 2\sin. a \cos. b - \sin. (a - b);$$

And when  $a = b$ , this equation becomes

$$\sin. 2a = 2\sin. a \cos. a. \quad \text{Eq. (30).}$$

To find the sine of 11', we make  $a = 6'$ , and  $b = 5'$ ;

$$\begin{aligned} \text{then} \quad \sin. 11' &= 2\sin. 6' \cos. 5' - \sin. 1' = .00319976413 \\ a = b = 6', \quad \sin. 12' &= 2\sin. 6' \cos. 6'. \\ a = 7', b = 6', \quad \sin. 13' &= 2\sin. 7' \cos. 6' - \sin. 1'. \\ a = b = 7', \quad \sin. 14' &= 2\sin. 7' \cos. 7'. \\ a = 8', b = 7', \quad \sin. 15' &= 2\sin. 8' \cos. 7' - \sin. 1' \end{aligned}$$

And so on to the

$$\begin{aligned} \sin. 30' &= 2\sin. 15' \cos. 15'. \\ \sin. 1^\circ &= \sin. 60' = 2\sin. 30' \cos. 30'. \\ \sin. 2^\circ &= 2\sin. 1^\circ \cos. 1^\circ. \\ \sin. 3^\circ &= 2\sin. 2^\circ \cos. 1^\circ - \sin. 1^\circ, \text{ etc., etc., etc.} \end{aligned}$$

This process may be continued until we have found the sines and cosines of all arcs differing by 1', from 0 to 90°, the values of the cosines being deduced successively from those of the sines by means of the formula,

$$\cos. = \sqrt{1 - \sin.^2}.$$

In this calculation, we began by assuming that, for small arcs, the sines and the arcs were sensibly equal.

It must be remembered that this is but an approximation; and although the error in the early stages of the process is not sufficient to affect any of the decimal figures which enter the tables, it will finally become so, since it is constantly increased in the operations by which the sines and cosines of the larger arcs are deduced from those of the smaller. When the error has been thus increased until it reaches the order of the last decimal unit of the table, which assigns our limit of error, we must have the means of detecting and correcting it.

This consists in calculating the sines and cosines of certain arcs by independent processes, and comparing them with those found by the above method.

We have seen, for example, (Prop. 7, B. V), that the chord of

$$\begin{array}{l} 30^\circ = 517638090; \text{ whence, } \sin. 15^\circ = .258819045. \\ 15^\circ = .2610523842; \quad \text{“} \quad \text{“} \quad 7^\circ 30' = .130526192. \\ 7^\circ 30' = .1308062583; \quad \text{“} \quad \text{“} \quad 3^\circ 45' = .0654031291. \end{array}$$

And so on to

$$\begin{array}{l} \sin. 14' 3'' 45''' = .004090604. \\ \text{etc.} \quad \text{etc.} \quad \text{etc.} \end{array}$$

The following elegant method of deducing, from the sine of an arc, the sine and cosine of one half the arc, is given, assuming that the student is familiar with the simple algebraic principles upon which it depends.

Let us take the natural sine of  $18^\circ$ , which is .3090170, and make  $x = \text{sine}$ , and  $y$  the cosine of  $9^\circ = \frac{18^\circ}{2}$ .

$$\text{Then,} \quad x^2 + y^2 = 1; \quad (1)$$

$$\text{and} \quad 2xy = .3090170 \quad (2); \quad \text{Eq. (30)}$$

Adding, we have

$$x^2 + 2xy + y^2 = 1.3090170;$$

Taking the square root, we have

$$x + y = 1.144123. \quad (3)$$

Subtracting (2) from (1),

$$x^2 - 2xy + y^2 = .690983;$$

taking the square root,

$$x - y = -.831254* \quad (4)$$

Adding (3) and (4),  $2x = .312869$ ,

hence,  $x = \sin.9^\circ = .1564345$

Subtracting (4) from (3),  $2y = 1.975377$

hence,  $y = \cos.9^\circ = .9876885$

Now, by making  $x =$  the sine of  $4^\circ 30'$ , and  $y =$  cosine of  $4^\circ 30'$ , and as before

$$x^2 + y^2 = 1$$

and  $2xy = .1564345$ ,

we obtain the sine and cosine of  $4^\circ 30'$ ; and another operation will give the sine and cosine  $2^\circ 15'$ , etc., etc.

We may in this manner compute the sines and cosines of all arcs resulting from the division of  $18^\circ$  by 2, and we may make their values accurate to any assigned decimal figure.

This has been carried far enough to show how a table of natural sines, etc., could be computed; but in consequence of the tedious numerical operations which the process requires, other methods are resorted to in the actual construction of the table.

The Calculus furnishes formulæ giving the values of the sines and cosines of arcs developed into rapidly converging series, and from these the sines and cosines of all arcs from  $0^\circ$  to  $90^\circ$ , can be determined with great

\* When an arc is less than  $45^\circ$ , the cosine exceeds the sine; and when the arc is between  $45^\circ$  and  $90^\circ$ , the sine exceeds the cosine. Hence, when the arc is  $9^\circ$ ,  $y$ , its cosine, exceeds  $x$ , its sine; and we therefore placed the minus sign before the second member of Eq. (4).

accuracy and with comparatively little labor. In the last two columns on each page of Table II, will be found the values thus computed of the sines and cosines of every degree and minute of a quadrant.

### TRIGONOMETRICAL LINES FOR ARCS EXCEEDING $90^\circ$ .

From the annexed figure, the construction of which needs no explanation, are deduced by simple inspection the results given in the following

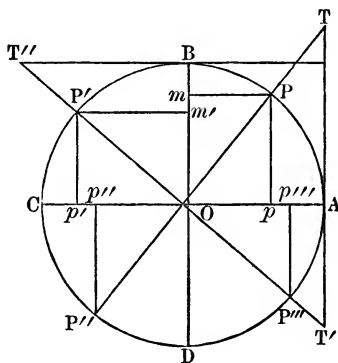


TABLE.

$90^\circ + a^\circ$	$270^\circ - a^\circ$
sin. = cos. $a$ , cos. = -sin. $a$	sin. = -cos. $a$ , cos. = -sin. $a$
tan. = -cot. $a$ , cot. = -tan. $a$	tan. = cot. $a$ , cot. = tan. $a$
sec. = -cosec. $a$ , cosec. = sec. $a$	sec. = -cosec. $a$ , cosec. = -sec. $a$
$180^\circ - a^\circ$	$270^\circ + a^\circ$
sin. = sin. $a$ , cos. = -cos. $a$	sin. = -cos. $a$ , cos. = sin. $a$
tan. = -tan. $a$ , cot. = -cot. $a$	tan. = -cot. $a$ , cot. = -tan. $a$
sec. = -sec. $a$ , cosec. = cosec. $a$	sec. = cosec. $a$ , cosec. = -sec. $a$
$180^\circ + a^\circ$	$360^\circ - a^\circ$
sin. = -sin. $a$ , cos. = -cos. $a$	sin. = -sin. $a$ , cos. = cos. $a$
tan. = tan. $a$ , cot. = cot. $a$	tan. = -tan. $a$ , cot. = -cot. $a$
sec. = -sec. $a$ , cosec. = -cosec. $a$	sec. = sec. $a$ , cosec. = -cosec. $a$

By means of this table, the values of the trigonometrical lines of any arc between  $90^\circ$  and  $360^\circ$ , can be expressed by those of arcs less than  $90^\circ$ .

If, for example, the arc is  $118^\circ$ , we have



$$\sin.118^\circ = \sin.(90^\circ + 28^\circ) = \cos.28^\circ;$$

$$\tan.118^\circ = \tan.(90^\circ + 28^\circ) = -\cot.28^\circ;$$

$$\text{etc.,} \qquad \text{etc.,} \qquad \text{etc.}$$

For the arc  $230^\circ$ , we have

$$\sin.230^\circ = \sin.(270^\circ - 40^\circ) = -\cos.40^\circ;$$

$$\sec.230^\circ = \sec.(270^\circ - 40^\circ) = -\operatorname{cosec}.40^\circ;$$

$$\text{etc.,} \qquad \text{etc.,} \qquad \text{etc.}$$

In many investigations, it becomes necessary to consider the functions of arcs greater than  $360^\circ$ ; but since the addition of  $360^\circ$  any number of times to the arc  $a$ , will give an arc terminating in the extremity of  $a$ , it is obvious that the arc resulting from such addition will have the same functions as the arc  $a$ . And hence it follows that the functions of arcs, however great, may be expressed in terms of the functions of arcs less than  $90^\circ$ .

## SECTION II.

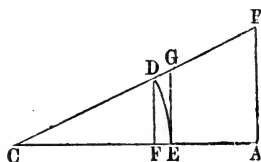
## PLANE TRIGONOMETRY, PRACTICALLY APPLIED.

IN the preceding section, the theory of Trigonometry has been quite fully developed, and the student should now be prepared for its various applications, were he acquainted with logarithms. But logarithms are no part of Trigonometry, and serve only to facilitate the numerical operations. Trigonometrical computations can be made without logarithms, and were so made long before the theory of logarithms was understood.

For this reason, we proceed at once to the solution of the following triangles.

1. The hypotenuse of a right-angled triangle is 21, and the base is 17; required the perpendicular and the acute angles.

Let  $CAB$  be the triangle, in which  $CB = 21$ , and  $CA = 17$ . With  $C$  as a center, and  $CD = 1$  as a radius, describe the arc  $DE$ , of which the sine is  $DF$ , the tangent is  $EG$ , and the cosine is  $CF$ .



By similar triangles we have

$$CB : CA :: CD : CF;$$

that is,

$$21 : 17 :: 1 : \cos. C.$$

Hence,

$$\cos. C = \frac{17}{21} = .80952+.$$

We must now turn to Table II, and find in the last two columns the cosine nearest to .80952, and the corresponding degrees and minutes will be the value of the angle  $C$ .

On page 57, of Tables, near the bottom of the page, and in the column with cosine at the top, we find .80953, which corresponds to  $35^\circ 56'$  for the angle  $C$ . The angle  $B$  is, therefore,  $54^\circ 3'$ .

This Table is so arranged, that the sum of the degrees at the top and bottom of the page, added to the sum of the minutes which are found on the same horizontal line in the two side columns of the page, is  $90^\circ$ .

Thus, in finding the angle  $C$ , the number .80953 was found in the column with cosine at the head. We therefore took the degrees from the head of the page, and the minutes were taken from the left hand column, counting downwards.

For the side  $AB$ , we have the proportion

$$CF : FD :: CA : AB;$$

or,  $\cos. C : \sin. C :: 17 : AB;$

that is,  $.80953 : .58708 :: 17 : AB.$

From which we find  $AB = .58708 \times 17 \div .80953;$

whence,  $AB = 12.323.$

If we had formed a table of natural tangents, as well as of natural sines,  $AB$  could have been found by the following proportion.

$$CE : EG :: CA : AB$$

or,  $1 : \tan. C :: 17 : AB;$

whence,  $AB = 17 \tan. C.$

The perpendicular  $AB$  may also be found by the proportion

$$CD : DF :: CB : AB;$$

or,  $1 : \sin. C :: 21 : AB;$

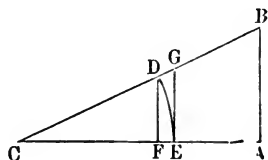
whence,  $AB = 21 \sin. C = 21 \times .58708 = 12.32868.$

2. The two sides of a right-angled triangle are 150 and 125; required the hypotenuse and the acute angles.

We may employ the same figure as in the preceding problem.

Then, from the similar triangles,  $CFD$  and  $CAR$ , we get

$$CF : FD :: CA : AB;$$



that is,  $\cos. C : \sin. C :: 150 : 125 :: 6 : 5$ ,

which gives  $6 \sin. C = 5 \cos. C$ ;

hence,  $36 \sin.^2 C = 25 \cos.^2 C$ .

Adding member to member,  $36 \cos.^2 C = 36 \cos.^2 C$ .

we have  $36 (\sin.^2 C + \cos.^2 C) = 61 \cos.^2 C$ .

But  $\sin.^2 C + \cos.^2 C = 1$ , (Eq. (1) Trigonometry);

whence,  $61 \cos.^2 C = 36$ ;

$$\cos.^2 C = \frac{36}{61} = .5901639344;$$

and  $\cos. C = .76822$ , nearly.

To find the angle of which this is the cosine, we turn to page 60 of tables, and looking in the column having cosine at the head, we see that .76822 falls between .76828, which has 48' opposite to it in the left hand column, and .76810, which has 49' opposite to it in the same column. Now, the cosines of arcs less than 90° decrease when the arcs increase, and the converse; and while the increase of the arc is confined within the limits of 1', the increase of the arc will be sensibly proportional to the decrease of the cosine.

$$\begin{array}{r} \text{Hence,} \quad \begin{array}{r} 0.76828 \\ 0.76810 \\ \hline 18 \end{array} \quad : \quad \begin{array}{r} .76828 \\ .76822 \\ \hline 6 \end{array} :: 60'' : x'' \end{array}$$

which gives  $x'' = 20''$ .

The angle  $C$  is, therefore, equal to  $39^\circ 48' 20''$ , and the angle  $B = 90^\circ - 39^\circ 48' 20'' = 50^\circ 11' 40''$ .

To find  $CB$ , we have

$$CF : CD :: CA : CB;$$

or,  $\cos. C : 1 :: 150 : CB$ ;

that is,  $.76822 : 1 :: 150 : CB$ ;

whence,  $CB = \frac{150}{.76822} = 195.26$ —.

3. The base of a right-angled triangle is 150, and the angle opposite the base is  $50^\circ 11' 40''$ ; required the hypotenuse and the perpendicular.

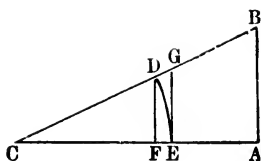
Let  $CAB$  be the triangle.

Then, (Prop. 4, Sec. I),

$$\sin. 50^\circ 11' 40'' : \sin. 90^\circ :: 150 : CB.$$

Whence,

$$CB = \frac{150}{.76822} = 195.26,$$



the same as in the preceding example.

To find  $AB$ , we have

$$CD : DF :: CB : AB;$$

that is,  $1 : \sin. C$  or  $\cos. B :: 195.26 : AB$ ;

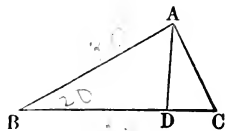
from which we find

$$AB = 195.26 \sin. 39^\circ 48' 40'';$$

or,  $AB = 125.0015.$

4. Two sides, the one 30 and the other 35, and the included angle  $20^\circ$ , of a triangle, are given, to find the other two angles and the third side.

Let  $BAC$  be the triangle, in which  $BC = 35$ ,  $BA = 30$ , and the angle  $B = 20^\circ$ . From  $A$ , the extremity of the shorter side, let fall on  $BC$  the perpendicular  $AD$ , thus dividing the triangle into the two right-angled triangles  $BAD$  and  $CAD$ .



Then, from the triangle  $BAD$ , we have

$$1st, \quad \sin. D : \sin. B :: BA : AD;$$

$$or, \quad 1 : \sin. 20^\circ :: 30 : AD = 30 \sin. 20^\circ$$

$$2d, \quad 1 : \cos. B :: BA : BD;$$

$$or, \quad 1 : \cos. 20^\circ :: 30 : BD = 30 \cos. 20^\circ.$$

In the table of natural sines, we find  $\sin. 20^\circ = .34202$ , and the  $\cos. 20^\circ = .93969$ ; hence,  $AD = 30 \times .34202 = 10.26060$ , and  $BD = 30 \times .93969 = 28.19070$ , and therefore  $DC = BC - BD = 6.8093$ .

From the triangle  $CAD$ , we have

$$1st, \quad AC = \sqrt{AD^2 + DC^2} = \sqrt{(10.26)^2 + (6.8+)^2} = 12.967$$

$$2d, \quad AC : AD :: \sin. 90^\circ : \sin. C;$$

or,  $12.367 : 10.264 :: 1 : \sin. C;$

whence,  $\sin. C = \frac{10.26}{12.367} = .83319.$

and the angle  $C = 56^{\circ} 26'.$

If, now, we add angles  $B$  and  $C$ , and take the sum from  $180^{\circ}$  the remainder will be the angle  $BAC$ .

Hence,  $\sphericalangle BAC = 180^{\circ} - (56^{\circ} 26' + 20^{\circ}) = 103^{\circ} 34'.$

5. Two sides, the one 18 and the other 24, and the angle opposite the side 24 equal to  $76^{\circ}$ , are given, to find the remaining side and the other two angles.

Let  $x$  denote the angle opposite the side 18. Then,

$$24 : 18 :: \sin. 76^{\circ} : \sin. x, \text{ (Prop. 4, Trig.)}$$

or,  $4 : 3 :: \sin. 76^{\circ} : \sin. x.$

$$\sin. x = \frac{3}{4} \sin. 76^{\circ} = \frac{3}{4} \times .97030 = .72772;$$

whence the angle opposite the side 18 is  $46^{\circ} 41' 45''.$

Adding this to the given angle, and taking the sum from  $180^{\circ}$ , we get  $57^{\circ} 18' 15''$  for the third angle.

To find the remaining side, denoted by  $y$ , we have

$$\sin. 76^{\circ} : \sin. 57^{\circ} 18' 15'' :: 24 : y;$$

or,  $.97030 : .84155 :: 24 : y.$

$$y = \frac{24 \times .84155}{.97030} = 20.815 = 3d \text{ side.}$$

6. The three sides of a triangle are 18, 24, and 20.815; required the angles.

This problem may be solved by Prop. 6, or by Prop. 8, Trigonometry.

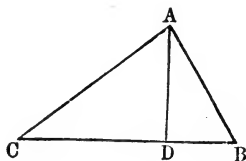
*First. By Prop. 6.*

In the triangle  $ABC$ , make  $CB = 24$ ,  $AC = 20.815$ , and  $AB = 18$ .

Then,

$$24 : 38.815 :: 2.815 : CD - BD.$$

$$CD - BD = \frac{109.264225}{24} = 4.5527.$$



But  $CD + BD = CB = 24$ .

By addition, we get  $2CD = 28.5527$ ;

dividing by 2, and  $CD = 14.2763+$ .

And hence,  $BD = CB - CD = 24 - 14.2763 = 9.7237$ .

In the triangle  $ADB$ , we have

$$BA : BD :: 1 : \cos. B$$

or,  $18 : 9.7237 :: 1 : \cos. B = .54020$

Table II, Page 53,  $\left\{ \begin{array}{l} \cos. 57^\circ 18' = .54024 \\ \cos. 57^\circ 19' = .54000 \end{array} \right\}$

diff. =  $24 : 60'' :: 4 : 10''$

hence,  $\sphericalangle B = 57^\circ 18' 10''$ .

It will be observed that Examples 5 and 6 refer to the same triangle, and that in Example 5 the angle  $B$  was  $57^\circ 18' 15''$ . This slight discrepancy in the results should be expected, on account of the small number of decimal places used in the computations.

*Second. By Prop. 8.*

Sum of the sides, = 62.815,

half sum denoted by  $s$ , = 31.4075

$a$  = 24

$s - a$  = 7.4075

Formula,  $\cos. \frac{1}{2} A = \sqrt{\frac{s(s-a)}{bc}}$ , radius being unity.

$$s(s-a) = 31.4075 \times 7.4075 = 232.65105625$$

$$bc = 20.815 \times 18 = 374.67$$

$$\frac{s(s-a)}{bc} = .62095 \text{ very nearly.}$$

$$\sqrt{.62095} = .78800.$$

Hence,  $\cos. \frac{1}{2} A = .78800$ , and  $\frac{1}{2} A$  (Table II, page 59) =  $38^\circ$  very nearly; the angle  $A$  is therefore equal to  $76^\circ$ , which agrees with Example 5.

7. Given, the three sides, 1425, 1338, and 493, of a triangle; required, the angle opposite the greater side, using the formula for the sine of one half an angle.

Make  $a = 1425$ ,  $b = 1338$ , and  $c = 493$ ; then the  $\sphericalangle A$  is opposite the side  $a$ , and the formula is

$$\sin.^2 \frac{1}{2}A = \frac{(s-b)(s-c)}{bc}$$

in which  $s$  denotes the half sum of the three sides.

Then we have  $s = 1628$ ,  $s - b = 290$ ,  $s - c = 1135$ ,  $(s - b)(s - c) = 329150$ ,  $bc = 659634$ ,  $\frac{(s-b)(s-c)}{bc} = .498988$

Hence,  $\sin. \frac{1}{2}A = \sqrt{.498988} = .70632$ .

In the table we find  $\sin. 44^\circ 56' 28.5'' = .70638$ .

Therefore,  $\frac{1}{2}A = 44^\circ 56' 28.5''$ , and  $A = 89^\circ 52' 57''$ ; — but little less than a right angle.

In these seven examples we have shown that it is possible to solve any plane triangle, in which three parts, one at least being a side, are given, without the aid of logarithms. But, when great accuracy is required, and the number of decimal places employed is large, the necessary multiplications and divisions, the raising to powers, and the extraction of roots, *become very tedious*. All of these operations may be performed without impairing the correctness of results, and with a great saving of labor, by means of logarithms; but, before using them, the student should be made acquainted with their nature and properties.

## LOGARITHMS.

**Logarithms** are the exponents of the powers to which a fixed number, called the *base*, must be raised, to produce other numbers.

The exponent of a number is also a number expressing how many times the first number is taken as a factor.

Thus, let  $a$  denote any number; then  $a^3$  indicates that  $a$  has been used three times as a factor,  $a^4$  that it has been used four times as a factor, and  $a^n$  that it has been thus used  $n$  times.



Now, instead of calling these numbers 3, 4, — —  $n$ , exponents, we call them the logarithms of the powers  $a^3$ ,  $a^4$ , — —  $a^n$ .

To multiply  $a^2$  by  $a^5$ , we have simply to write  $a$ , giving it an exponent equal to  $2 + 5$ ; thus,  $a^2 \times a^5 = a^7$ .

Hence, *the sum of the logarithms of any number of factors is equal to the logarithm of the product.*

To divide  $a^{12}$  by  $a^9$ , we have only to write  $a$ , giving it an exponent equal to  $12 - 9$ ; thus,  $a^{12} \div a^9 = a^3$ ; and, generally, the quotient arising from the division of  $a^m$  by  $a^n$ , is equal to  $a^{m-n}$ .

Hence, *the logarithm of a quotient is the logarithm of the dividend diminished by the logarithm of the divisor.*

If it is required to raise a number denoted by  $a^3$ , to the fifth power, we write  $a$ , giving it an exponent equal to  $3 \times 5$ ; thus,  $(a^3)^5 = a^{15}$ , and, generally,  $(a^n)^m = a^{nm}$ .

Hence, *the logarithm of the power of a number is equal to the logarithm of the number multiplied by the exponent of the power.*

To extract the 5th root of the number  $a^3$ , we write  $a$ , giving it an exponent equal to  $\frac{3}{5}$ ; thus,  $\sqrt[5]{a^3} = a^{\frac{3}{5}}$ , and, generally, to extract any root of a number, we divide the exponent of the number by the index of the root, and the quotient will be the exponent of the required root.

Hence, *the logarithm of a root of a number is equal to the quotient obtained by dividing the logarithm of the number by the index of the root.*

Now, understanding that by means of a table of logarithms we may find the numbers answering to given logarithms, with as much facility as we can find the logarithms of given numbers, we see from what precedes that multiplications, divisions, raising to powers, and the extraction of roots, may be performed by logarithms; and the utility of logarithms, in trigonometrical computations, mainly consists in the simplification and abridgment of these operations by their use.

The common logarithms are those of which 10 is the base; that is, they are the exponents of 10.

Thus, $10^1 = 10$	Hence the logarithm 10	= 1.
$10^2 = 100$	“ “ “	100 = 2.
$10^3 = 1000$	“ “ “	1000 = 3.
$10^4 = 10000$	“ “ “	10000 = 4.
etc. etc.	etc.	etc. etc.

Since  $\frac{10}{10} = 1 = 10^{1-1} = 10^0$ , and generally  $\frac{a^m}{a^m} = a^0 = 1$ , it follows that in this, as in all other systems, the logarithm of  $1 = 0$ .

From what precedes, it is evident that the logarithm of any number between 10 and 100 must be found between 1 and 2; that is, its logarithm is 1 plus a number less than 1; and any number between 100 and 1000, will have for its logarithm 2 plus some number less than 1, and so on. The fractional part of the logarithm of a number is expressed decimally.

The entire number belonging to a logarithm is called its *index*. The index is never put in the tables, (except from 1 to 100), and need not be put there, because we always know what it is. It is always one less than the number of digits in the integer. Thus, the number 3754 has 3 for the index to its logarithm, because the number consists of 4 digits; that is, *the logarithm is 3 and some decimal*.

The number 347.921 has 2 for the index of its logarithm, because the number is between 347 and 348, and 2 is the index for the logarithms of all numbers over 100, and less than 1000.

All numbers consisting of the same figures, whether integral, fractional, or mixed, have logarithms consisting of the same *decimal* part. The logarithms differ only in their indices.

Thus, the number 7956. has	3.900695	for its log.
the number 795.6 has	2.900695	“
the number 79.56 has	1.900695	“
the number 7.956 has	0.900695	“
the number .7956 has	—1.900695	“
the number .07956 has	—2.900695	“

From this we perceive that we must take the logarithm out of the table for a mixed number or a decimal, the same as if the figures expressed an entire number; and then, to *prefix* the index, we must consider the *value* of the number.

The decimal part of a logarithm is always positive; but the index becomes negative when the number is a decimal; and the smaller the decimal, the greater the negative index. Hence,

To prefix the index to a decimal, count the decimal point as 1, and every cipher as 1, up to the first significant figure, and this is the negative index.

For example, find the logarithm of the decimal .0000831.

Num. .0000831; log. —5.919601.

The point is counted one, and each of the ciphers is counted one; therefore the index is *minus five*.

The smaller the decimal, the greater the negative index; and when the number becomes 0, the logarithm is *negatively infinite*.

Hence, the logarithmic sine of  $0^\circ$  is *negatively infinite*, however great the radius.

*A number being given, to find its corresponding logarithm.*

The logarithm of any number consisting of four figures, or less, is taken out of the table directly, and without the least difficulty.

Thus, to find the logarithm of the number 3725, we

find 372 at the side of the table, and in the column marked 5 at the top, and opposite 372, we find .571126, for the decimal part of the logarithm.

Hence, the logarithm of 3725 is 3.571126.  
 the logarithm of 37250 is 4.571126.  
 the logarithm of 37.25 is 1.571126, etc.

Find the logarithm of the number 834785.

This number is so large that we cannot find it in the table, but we can find the numbers 8347 and 8348. The logarithms of these numbers are the same as the logarithms of the numbers 834700 and 834800, except the indices.

	834700	log.	5.921530
	834800	log.	5.921582
	100		52
Difference,			

Now, our proposed number, 834785, is between the two assumed numbers; and, of course, its logarithm lies between the logarithms of the two assumed numbers; and, without further comment, we may find it by proportion thus,

$$\begin{aligned} & 100 : 85 = 52 : 44.2 \\ \text{Or,} & \quad 1. : .85 = 52 : 44.2 \end{aligned}$$

Hence, for finding from the table the logarithm of a number consisting of more than four places of figures, we have the following

#### R U L E.

*Take from the table the log. of the number expressed by the the four superior figures; this, with the proper index, is the approximate logarithm. Multiply the number expressed by the remaining figures of the number, regarded as a decimal, by the tabular difference, and the product will be the correction to be added to the approximate log. to obtain the true log*

## EXAMPLES.

1. What is the log. of 357.32514?

The log. of 357.3 is 2.553033

No. not included, .2514

Tabular diff., 122

Prod., 30.6708; correction, 31

log. sought, 2.553064

The log. of 35732.514 is 4.553064

“ .035732514 “ — 2.553064.

2. What is the log. of 7912532?

Approximate log., 6.898286

.532 × 55 = correction, 29

True log. = 6.898315.

*A logarithm being given, to find its corresponding number.*

For example, what number corresponds to the log. 6.898315?

The index 6 shows that the entire part of the number must contain seven places of figures. With the decimal part, .898315, of the log., we turn to the table, and find the next less decimal part to be .898286, which corresponds to the superior places, 7912.

The difference between the given log. and the one next less is 29. This we divide by the tabular difference, 55, because we are working the converse of the preceding problem. Thus,

$$29 \div 55 = 52727+.$$

Place the quotient to the right of the four figures before found, and we shall have 7912527.27 for the number sought.

This example was taken from the preceding case, and the number found should have been 7912532; and so it would have been, had we used the true difference, 29.26, in place of 29.

When the numbers are large, as in this example, the

result is liable to a small error, to avoid which the logarithms should contain a great number of decimal places; but the logarithms in our table contain a sufficient number of decimal places for most practical purposes.

Hence, for finding the number corresponding to **any** given logarithm, we have the following

R U L E.

*Look in the table for the decimal part of the given logarithm, and if not found, take the decimal next less, and take out the four corresponding figures.*

*Take the difference between the given log. and the next less in the table; divide that difference by the tabular difference, and write the quotient on the right of the four superior figures, and the result is the number sought.*

*Point off the whole number required by the given index.*

EX A M P L E S.

1. Given, the logarithm 3.743210, to find its corresponding number true to three places of decimals.

*Ans.* 5536.177.

2. Given, the logarithm 2.633356, to find its corresponding number true to two places of decimals.

*Ans.* 429.89.

3. Given, the logarithm — 3.291746, to find its corresponding number.

*Ans.* .0019577.

4. What number corresponds to the log. 3.233568?

*Ans.* 1712.25.

5. What is the number of which 1.532708 is the log.?

*Ans.* 34.0963.

6. Find the number whose log. is 1.067889.

*Ans.* 11.692.

EXPLANATION OF TABLE II.

Table I is merely a table of numbers and their corresponding logarithms, and requires no explanation other

than that which has been given in connection with the subject of logarithms.

Table II, with the exception of the last two columns, which contain natural sines and cosines, is a table in which are arranged the logarithms of the numerical values of the several trigonometrical lines corresponding to the different angles in a quadrant. The values of these lines are computed to the radius 10,000,000,000, and their logarithms are nothing more than the logarithms, each increased by 10, of the natural sines, cosines, and tangents, of the same angles; because the values of these lines, for arcs of the same number of degrees taken in different circles, are directly proportional to the radii of the circles.

The natural sines are made to the radius of unity; and, of course, any particular sine is a decimal fraction, expressed by natural numbers. The logarithm of any natural sine, with its index increased by 10, will give the logarithmic sine. Thus, the natural sine of  $3^\circ$  is .052336.

The logarithm of this decimal is	— 2.718800
To which add	10.
	<hr style="width: 100px; margin: 0 auto;"/>
The logarithmic sine of $3^\circ$ is, therefore,	8.718800

In this manner we may find the logarithmic sine of any other arc, when we have the natural sine of the same arc.

If the natural sines and logarithmic sines were on the same radius, the logarithm of the natural sine would be the logarithmic sine, at once, without any increase of the index.

The radius for the logarithmic sines is arbitrarily taken so large that the index of its logarithm is 10. It might have been more or less; but, by common consent, it is settled at this value; so that the sines of the smallest arcs ever used shall not have a negative index.

In our preceding equations,  $\sin. a$ ,  $\cos. a$ , etc., refer to *natural sines*; and by such equations we determine their values in natural numbers; and these numbers are put in Table II, under the heads of *N. sine* and *N. cos.*, as before observed.

When we have the sine and cosine of an arc, the tangent and cotangent are found by Eq. (3) and (6); thus,

$$\tan. = \frac{R \sin.}{\cos.} \quad (6) \quad \cot. = \frac{R \cos.}{\sin.};$$

and the secant is found by equation (4); that is,

$$\sec. = \frac{R^2}{\cos.}.$$

For example, the logarithmic sine of  $6^\circ$  is 9.019235, and its cosine 9.997614. From these it is required to find the logarithmic tangent, cotangent, and secant.

$R \sin.$		19.019235
Cos.	subtract	9.997614
Tan. is		9.021621
$R \cos.$		19.997614
Sin.	subtract	9.019235
Cotan. is		10.978379
$R^2$ is		20.000000
Cos.	subtract	9.997674
Secant is		10.002326

The secants and cosecants of arcs are not given in our table, because they are very little used in practice; and if any particular secant is required, it can be determined by subtracting the cosine from 20; and the cosecant can be found by subtracting the sine from 20.

The sine of every degree and minute of the quadrant is given, directly, in the table, commencing at  $0^\circ$ , and extending to  $45^\circ$ , at the head of the table; and from  $45^\circ$  to  $90^\circ$ , at the bottom of the table, increasing backward.



The column having sine at the top has cosine at the bottom, and the opposite, because angles read from above are complementary to those read from below. The differences of consecutive logarithms corresponding to  $10''$  are given for both sine and cosine, but the tangents and cotangents have the same column of differences for the reason that  $\log. \tan. + \log. \cot. = \log. R^2$  and is therefore constant. Hence, by just as much as  $\log. \tan.$  increases,  $\log. \cot.$  decreases and the converse.

As cosines and cotangents decrease when arcs increase, and increase when arcs decrease, the proportional parts answering to seconds for them must be subtracted.

*Example.* Find the sine of  $19^\circ 17' 22''$ .

The sine of $19^\circ 17'$ , taken directly from the table, is	9.518829
The difference for $10''$ is 60.2; for $1''$ is 6.02; and for $6.02 \times 22 =$	132
Hence, $\log. \text{ sine } 19^\circ 17' 22''$ is	9.518961

From this it will be perceived that there is no difficulty in obtaining the sine or tangent, cosine or cotangent, of any angle greater than  $30'$ .

*Conversely:* Given, the logarithmic sine 9.982412, to find its corresponding arc. The sine next less in the table is 9.982404, which gives the arc  $73^\circ 48'$ . The difference between this and the given sine is 8, and the difference for  $1''$  is .61; therefore, the number of seconds corresponding to 8, must be discovered by dividing 8 by the decimal .61, which gives 13. Hence, the arc sought is  $73^\circ 48' 13''$ .

These operations are too obvious to require a rule. When the arc is very small,—and such arcs are sometimes required in Astronomy,—it is necessary to be very accurate; for this reason we omitted the difference for seconds for all arcs under  $30'$ . Assuming that the sines and tangents of arcs under  $30'$  vary in the same proportion as the arcs themselves, we can find the sine or tangent of any very small arc, with great exactness, as follows:

The sine of 1', as expressed in the table, is	3.463726
Divide this by 60; that is, subtract logarithm	1.778151
	<hr/>
The logarithmic sine of 1'', therefore, is	4.685575
Now, for the sine of 17'', add the logarithm of 17	1.230419
	<hr/>
Logarithmic sine of 17'', is	5.916024

In the same manner we may find the sine of any other small arc.

For example, find the sine of  $14' 21\frac{1}{2}''$ ; that is, 861.5".

The logarithmic sine of 1'' is	4.685575
Add logarithm of 861.5,	2.935254
	<hr/>
Logarithmic sine of $14' 21\frac{1}{2}''$ ,	7.620829

Two lines drawn, the one from the surface and the other from the center of the earth, to the center of the sun, make with each other an angle of  $8.61''$ . What is the logarithmic sine of this angle?

The log. of the sine 1'' is	4.685575
Log. of 8.61,	0.935003
	<hr/>
Log. sine of sun's horizontal parallax	= 5.620578

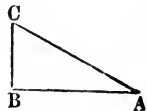
## GENERAL APPLICATIONS WITH THE USE OF LOGARITHMS.

### I. RIGHT-ANGLED TRIGONOMETRY.

One figure will be sufficient to represent the triangle in all of the following examples; the right angle being at  $B$ .

#### PRACTICAL PROBLEMS.

1. In a right-angled triangle,  $ABC$ , given the base  $AB$ , 1214, and the angle  $A$ ,  $51^\circ 40' 30''$ , to find the other parts.



To find  $BC$ .

Radius,	10.000000
: $\tan. A, 51^\circ 40' 30''$ ,	10.102119
:: $AB, 1214$ ,	<u>3.084219</u>
: $BC, 1535.8$ ,	3.186338

**REMARK.**—When the first term of a logarithmic proportion is radius, the required logarithm is found by adding the second and third logarithms, rejecting 10 in the index, which is dividing by the first term.

In all cases we add the second and third logarithms together; which, in logarithms, is multiplying these terms together; and from that sum we subtract the first logarithm, whatever it may be, which is dividing by the first term.

To find  $AC$ .

Sin. $C$ , or cos. $A, 51^\circ 40' 30''$ ,	9.792477
: $AB, 1214$ ,	3.084219
:: Radius,	<u>10.000000</u>
: $AC, 1957.7$ ,	3.291742

To find this resulting logarithm, we subtracted the first logarithm from the second, conceiving its index to be 13.

Let  $ABC$  represent any plane triangle, right-angled at  $B$ .

2. Given,  $AC$  73.26, and the angle  $A, 49^\circ 12' 20''$ ; required the other parts.

*Ans.* The angle  $C, 40^\circ 47' 40''$ ;  $BC, 55.46$ ; and  $AB, 47.86$ .

3. Given,  $AB$  469.34, and the angle  $A, 51^\circ 26' 17''$ , to find the other parts.

*Ans.* The angle  $C, 38^\circ 33' 43''$ ;  $BC, 588.7$ ; and  $AC, 752.9$ .

4. Given,  $AB$  493, and the angle  $C, 20^\circ 14'$ ; required, the remaining parts.

*Ans.* The angle  $A, 69^\circ 46'$ ;  $BC, 1338$ ; and  $AC, 1425.5$ .

5. Let  $AB = 331$ , and the angle  $A = 49^\circ 14'$ ; what are the other parts?

*Ans.*  $AC, 506.9$ ;  $BC, 383.9$ ; and the angle  $C, 40^\circ 46'$ .

6. If  $AC = 45$ , and the angle  $C = 37^\circ 22'$ , what are the remaining parts?

*Ans.*  $AB, 27.31$ ;  $BC, 35.76$ ; and the angle  $A, 52^\circ 38'$

7. Given,  $AC = 4264.3$ , and the angle  $A = 56^\circ 29' 13''$ , to find the remaining parts.

*Ans.*  $AB, 2354.4$ ;  $BC, 3555.4$ ; and the angle  $C, 33^\circ 30' 47''$ .

8. If  $AB = 42.2$ , and the angle  $A = 31^\circ 12' 49''$ , what are the other parts?

*Ans.*  $AC, 49.34$ ;  $BC, 25.57$ ; and the angle  $C, 58^\circ 47' 11''$ .

9. If  $AB = 8372.1$ , and  $BC = 694.73$ , what are the other parts?

*Ans.*  $\left\{ \begin{array}{l} AC, 8400.9; \text{ the angle } C, 85^\circ 15' 23''; \text{ and the} \\ \text{angle } A, 4^\circ 44' 37''. \end{array} \right.$

10. If  $AB$  be  $63.4$ , and  $AC$  be  $85.72$ , what are the other parts?

*Ans.*  $\left\{ \begin{array}{l} BC, 57.69; \text{ the angle } C, 47^\circ 41' 56''; \text{ and the} \\ \text{angle } A, 42^\circ 18' 4''. \end{array} \right.$

11. Given,  $AC = 7269$ , and  $AB = 3162$ , to find the other parts.

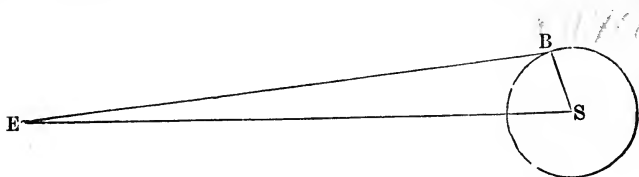
*Ans.*  $\left\{ \begin{array}{l} BC, 6545; \text{ the angle } C, 25^\circ 47' 7''; \text{ and the} \\ \text{angle } A, 64^\circ 12' 53''. \end{array} \right.$

12. Given,  $AC = 4824$ , and  $BC = 2412$ , to find the other parts.

*Ans.*  $\left\{ \begin{array}{l} \text{The angle } A = 30^\circ 00', \text{ the angle } C = 60^\circ 00', \\ \text{and } AB = 4178. \end{array} \right.$

13. The distance between the earth and sun is  $91,500,000$  miles, and at that distance the semi-diameter of the sun subtends an angle of  $16'$ . What is the diameter of the sun in miles?

*Ans.*  $887,674$ .



In this example, let  $E$  be the center of the earth,  $S$  that of the sun, and  $EB$  a tangent to the sun's surface. Then the  $\triangle EBS$  is right-angled at  $B$ , and  $BS$  is the semi-diameter of the sun. The value of  $2BS$  is required.

14. The equatorial diameter of the earth is 7925 miles, and the distance of the sun 91,500,000 miles. What angle will the semi-diameter of the earth subtend, as seen from the sun? *Ans.* 8.94".

This angle is called, in astronomy, the sun's horizontal parallax. The preceding figure applies to this example, by supposing  $E$  to be the center of the sun,  $S$  that of the earth, and  $BS$  equal to 3956 miles.

15. The mean distance of the moon from the earth is 60.3 times 3960 miles, and at this distance the semi-diameter of the moon subtends an angle of 15' 32". What is the diameter of the moon in miles?

*Ans.* 2157.8 miles.

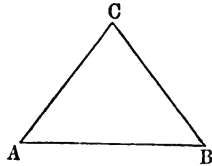
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## II. OBLIQUE-ANGLED TRIGONOMETRY.

### PROBLEM I.

*In a plane triangle, given a side and the two adjacent angles, to find the other parts.*

In the triangle  $ABC$ , let  $AB = 376$ , the angle  $A = 48^\circ 3'$ , and the angle  $B = 40^\circ 14'$ , to find the other parts.



As the sum of the three angles of every triangle is always  $180^\circ$ , the third angle,  $C$ , must be  $180^\circ - 88^\circ 17' = 91^\circ 43'$ .

To find  $AC$ .

Sin. $91^\circ 43'$ ,	9.999805
: $AB$ , 376,	2.575188
:: sin. $B$ $40^\circ 14'$ ,	9.810167
	12.385355
: $AC$ , 243,	2.385550

Observe, that the sine of  $91^\circ 43'$  is the same as the cosine of  $1^\circ 43'$

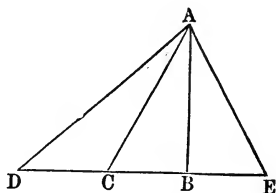
To find  $BC$ .

Sin. $91^\circ 43'$ ,	9.999805
: $AB$ , 376,	2.575188
$\therefore$ sin. $A$ , $48^\circ 3'$ ,	9.871414
	12.446602
: sin. $BC$ , 279.8,	2.446797

PROBLEM 11.

In a plane triangle, given two sides and an angle opposite one of them, to determine the other parts.

Let  $AD = 1751$  feet, one of the given sides; the angle  $D = 31^\circ 17' 19''$ ; and the side opposite, 1257.5. From these data, we are required to find the other side and the other two angles.



In this case we do not know whether  $AC$  or  $AE$  represents 1257.5, because  $AC = AE$ . If we take  $AC$  for the other given side, then  $DC$  is the other required side, and  $DAC$  is the vertical angle. If we take  $AE$  for the other given side, then  $DE$  is the required side, and  $DAE$  is the vertical angle. In such cases we determine both triangles.

To find the angle  $E = C$ .

(Prop. 4.)	$AC = AE = 1257.5$ ,	log. 3.099508
	: $D$ , $31^\circ 17' 19''$ ,	sin. 9.715460
	$\therefore AD$ , 1751,	log. 3.243286
		12.958746
	$E = C$ , $46^\circ 18'$ ,	sin. 9.859238

From  $180^\circ$  take  $46^\circ 18'$ , and the remainder is the angle  $DCA = 133^\circ 42'$ .

The angle  $DAC = ACE - D$ , (Th. 11, B. I);

that is,  $DAC = 46^\circ 18' - 31^\circ 17' 19'' = 15^\circ 0' 41''$ .

The angles  $D$  and  $E$ , taken from  $180^\circ$ , give

$$DAE = 102^\circ 24' 41''.$$

To find  $DC$ .

Sin. $D$ , $31^\circ 17' 19''$ ,	log.	9.715460
: $AC$ , 1257.5,	log.	3.099508
:: sin. $DAC$ $15^\circ 0' 41''$ ,	log.	0.413317
		<hr/>
		12.512825
		<hr/>
· $DC$ , 626.86,		2.797165

To find  $DE$ .

Sin. $D$ , $31^\circ 17' 17''$ ,		9.715460
: $AE$ , 1257.5,		3.099508
:: sin. $DAE$ , $102^\circ 24' 41''$ ,		9.989730
		<hr/>
		13.089238
		<hr/>
: $DE$ , 2364.7,		3.373778

REMARK.—To make the triangle possible,  $AC$  must not be less than  $AB$  the sine of the angle  $D$ , when  $DA$  is made radius.

## PROBLEM III.

In any plane triangle, given two sides and the included angle, to find the other parts.

Let  $AD = 1751$ , (see last figure),  $DE = 2364.5$ , and the included angle  $D = 31^\circ 17' 19''$ . We are required to find  $AE$ , the angle  $DAE$ , and the angle  $E$ .

Observe that the angle  $E$  must be less than the angle  $DAE$ , because it is opposite a less side.

From	$180^\circ$
Take $D$ ,	$31^\circ 17' 19''$ ,
	<hr/>

$$\begin{aligned} \text{Sum of the other two angles,} &= 148^\circ 42' 41'', \text{ (Th. 11, B. I),} \\ \frac{1}{2} \text{ sum} &= 74^\circ 21' 20''. \end{aligned}$$

By Proposition 7,

$$DE + DA : DE - DA = \tan. 74^\circ 21' 20'' : \tan. \frac{1}{2}(DAE - E)$$

That is,

$$4115.5 : 613.5 = \tan. 74^\circ 21' 20'' : \tan. \frac{1}{2}(DAE - E)$$

Tan. $74^{\circ} 21' 20''$ ,	10.552778
613.5,	2.787815
	<hr style="width: 100%;"/>
	13.340593
4115.5 log. (subtracted),	3.614423
	<hr style="width: 100%;"/>
tan. $\frac{1}{2}(DAE - E)$ tan. $28^{\circ} 1' 36''$ ,	9.726170

But the half sum plus the half difference of any two quantities is equal to the greater of the two; and the half sum minus the half difference is equal the less.

Therefore, to	$74^{\circ} 21' 20''$ ,
Add	$28^{\circ} 1' 36''$ ,
	<hr style="width: 100%;"/>
$DAE =$	$102^{\circ} 22' 56''$ ,
$E =$	$46^{\circ} 19' 45''$ ,

To find  $AE$ .

Sin. $E$ , $46^{\circ} 19' 45''$ ,	9.859323
: $DA$ , 1751,	3.243286
:: sin. $D$ , $31^{\circ} 17' 19''$ ,	9.715460
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	12.958746
	<hr style="width: 100%;"/>
: $AE$ , 1257.2,	3.099423

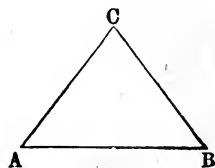
#### PROBLEM IV.

*Given, the three sides of a plane triangle, to find the angles.*

Let  $AC = 1751$ ,  $CB = 1257.5$ ,  $AB = 2364.5$ , to find the angles  $A$ ,  $B$ , and  $C$ .

If we take the formula for cosines, we will compute the greatest angle, which is  $C$ . To correspond with the formula,

$$\cos. \frac{1}{2} C = \sqrt{\frac{R^2 s (s - c)}{ab}},$$



we must take  $a = 1257.5$ ,  $b = 1751$ , and  $c = 2364.5$ .

The half sum of these is,

$$s = 2686.5; \text{ and } s - c = 322.$$



	$R^2$	20.000000
	$s = 2686.5$	3.429187
	$s - c = 322$	2.507856
	Numerator, log.	25.937043
$a$	1257.5	3.099508
$b$	1751.	3.243286
	Denominator, log.	6.342794
		6.342794
		2) 19.594249
$\frac{1}{2}C =$	51° 11' 10"	cos. 9.797124
$C =$	102 22 20	

The remaining angles may now be found by Problem 4.

#### PRACTICAL PROBLEMS.

Let  $ABC$  represent any oblique-angled triangle.

1. Given,  $AB$  697, the angle  $A$   $81^\circ 30' 10''$ , and the angle  $B$   $40^\circ 30' 44''$ , to find the other parts.

*Ans.*  $AC$ , 534;  $BC$ , 813; and  $\angle C$ ,  $57^\circ 59' 6''$ .

2. If  $AC = 720.8$ ,  $\angle A = 70^\circ 5' 22''$ ,  $\angle B = 59^\circ 35' 36''$ , required the other parts.

*Ans.*  $AB$ , 643.2;  $BC$ , 785.8; and  $\angle C$ ,  $50^\circ 19' 2''$ .

3. Given,  $BC$  980.1, the angle  $A$   $7^\circ 6' 26''$ , and the angle  $B$   $106^\circ 2' 23''$ , to find the other parts.

*Ans.*  $AB$ , 7283.8;  $AC$ , 7613.1; and  $\angle C$ ,  $66^\circ 51' 11''$ .

4. Given,  $AB$  896.2,  $BC$  328.4, and the angle  $C$   $113^\circ 15' 20''$ , to find the other parts.

*Ans.*  $\left\{ \begin{array}{l} AC, 712; \angle A, 19^\circ 35' 46''; \\ \text{and } \angle B, 46^\circ 38' 54''. \end{array} \right.$

5. Given,  $AC = 4627$ ,  $BC = 5169$ , and the angle  $A = 70^\circ 25' 12''$ , to find the other parts.

*Ans.*  $\left\{ \begin{array}{l} AB, 4328; \angle B, 57^\circ 29' 56''; \\ \text{and } \angle C, 52^\circ 4' 52''. \end{array} \right.$

6. Given,  $AB$  793.8,  $BC$  481.6, and  $AC$  500.0, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A, 35^\circ 15' 32''; \angle B, 36^\circ 49' 18''; \text{ and } \angle C, \\ 107^\circ 55' 10''. \end{array} \right.$$

7. Given,  $AB$  100.3,  $BC$  100.3, and  $AC$  100.3, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \text{The angle } A, 60^\circ; \text{ the angle } B, 60^\circ; \text{ and the} \\ \text{angle } C, 60^\circ. \end{array} \right.$$

8. Given,  $AB$  92.6,  $BC$  46.3, and  $AC$  71.2, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A, 29^\circ 17' 22''; \angle B, 48^\circ 47' 30''; \text{ and } \angle C, \\ 101^\circ 55' 8''. \end{array} \right.$$

9. Given,  $AB$  4963,  $BC$  5124, and  $AC$  5621, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A, 57^\circ 30' 28''; \angle B, 67^\circ 42' 36''; \text{ and } \angle C, \\ 54^\circ 46' 55''. \end{array} \right.$$

10. Given,  $AB$  728.1,  $BC$  614.7, and  $AC$  583.8, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A = 54^\circ 32' 52'', \angle B = 50^\circ 40' 58'', \text{ and } \angle C \\ = 74^\circ 46' 10''. \end{array} \right.$$

11. Given,  $AB$  96.74,  $BC$  83.29, and  $AC$  111.42, to find the angles.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A = 46^\circ 30' 45'', \angle B = 76^\circ 3' 46'', \text{ and } \angle C \\ = 57^\circ 25' 29''. \end{array} \right.$$

12. Given,  $AB$  363.4,  $BC$  148.4, and the angle  $B$   $102^\circ 18' 27''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} \angle A = 20^\circ 9' 17'', \text{ the side } AC = 420.8, \text{ and } \angle C \\ = 57^\circ 32' 16''. \end{array} \right.$$

13. Given,  $AB$  632,  $BC$  494, and the angle  $A$   $20^\circ 13'$ , to find the other parts, the angle  $C$  being acute.

$$\text{Ans. } \left\{ \begin{array}{l} \angle C = 26^\circ 18' 19'', \angle B = 133^\circ 25' 41'', \text{ and} \\ AC = 1035.7. \end{array} \right.$$

14. Given,  $AB$  53.9,  $AC$  46.21, and the angle  $B$   $58^\circ 16'$ , to find the other parts.

$$\text{Ans. } \angle A = 38^\circ 58', \angle C = 82^\circ 46', \text{ and } BC = 34.16.$$

15. Given,  $AB$  2163,  $BC$  1672, and the angle  $C$   $112^\circ 18' 22''$ , to find the other parts.

*Ans.*  $AC$ , 877.2;  $\sphericalangle B$ ,  $22^\circ 2' 16''$ ; and  $\sphericalangle A$ ,  $45^\circ 39' 22''$ .

16. Given,  $AB$  496,  $BC$  496, and the angle  $B$   $38^\circ 16'$ , to find the other parts.

*Ans.*  $AC$ , 325.1;  $\sphericalangle A$ ,  $70^\circ 52'$ ; and  $\sphericalangle C$ ,  $70^\circ 52'$ .

17. Given,  $AB$  428, the angle  $C$   $49^\circ 16'$ , and  $(AC + BC)$  918, to find the other parts, the angle  $B$  being obtuse.

*Ans.*  $\left\{ \begin{array}{l} \text{The angle } A = 38^\circ 44' 48'', \text{ the angle } B = 91^\circ \\ 59' 12'', AC = 564.5, \text{ and } BC = 353.5. \end{array} \right.$

18. Given,  $AC$  126, the angle  $B$   $29^\circ 46'$ , and  $(AB - BC)$  43, to find the other parts.

*Ans.*  $\left\{ \begin{array}{l} \text{The angle } A = 55^\circ 51' 32'', \text{ the angle } C = 94^\circ \\ 22' 28'', AB = 253.05, \text{ and } BC = 210.05. \end{array} \right.$

19. Given,  $AB$  1269,  $AC$  1837, and the angle  $A$   $53^\circ 16' 20''$ , to find the other parts.

*Ans.*  $\left\{ \begin{array}{l} \sphericalangle B = 83^\circ 23' 47'', \sphericalangle C = 43^\circ 19' 53'', \text{ and } BC \\ = 1482.16. \end{array} \right.$

## SECTION III.

APPLICATION OF TRIGONOMETRY TO MEASURING  
HEIGHTS AND DISTANCES.

IN this useful application of Trigonometry, a base line is always supposed to be measured, or given in length; and by means of a quadrant, sextant, circle, theodolite, or some other instrument for measuring angles, such angles are measured as, connected with the base line and the objects whose heights or distances it is proposed to determine, enable us to compute, from the principles of Trigonometry, what those heights or distances are.

Sometimes, particularly in marine surveying, horizontal angles are determined by the compass; but the varying effect of surrounding bodies on the needle, even in situations little removed from each other, and the general construction of the instrument itself, render it unfit to be employed in the determination of angles where anything like precision is required.

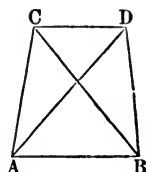
The following problems present sufficient variety, to guide the student in determining what will be the most eligible mode of proceeding, in any case that is likely to occur in practice.

## PROBLEM I.

Being desirous of finding the distance between two distant objects,  $C$  and  $D$ , I measured a base,  $AB$ , of 384 yards, on the same horizontal plane with the objects  $C$

and  $D$ . At  $A$ , I found the angles  $DAB = 48^\circ 12'$ , and  $CAB = 89^\circ 18'$ ; at  $B$ , the angles  $ABC = 46^\circ 14'$ , and  $ABD = 87^\circ 4'$ . It is required, from these data, to compute the distance between  $C$  and  $D$ .

From the angle  $CAB$ , take the angle  $DAB$ ; the remainder,  $41^\circ 6'$ , is the angle  $CAD$ . To the angle  $DBA$ , add the angle  $DAB$ , and  $44^\circ 44'$ , the supplement of the sum, is the angle  $ADB$ . In the same way the angle  $ACB$ , which is the supplement of the sum of  $CAB$  and  $CBA$ , is found to be  $44^\circ 28'$ .



Hence, in the triangles  $ABC$  and  $ABD$ , we have

Sin. $ACB$ , $44^\circ 28'$ ,	9.845405
: $AB$ , 384 yards,	2.584331
:: sin. $ABC$ , $46^\circ 14'$ ,	9.858635
	12.442966
: $AC$ , 395.9 yards,	2.597561
Sin. $ADB$ , $44^\circ 44'$ ,	9.847454
: $AB$ , 384 yards,	2.584331
:: sin. $ABD$ , $87^\circ 4'$ ,	9.999431
	12.583762
: $AD$ , 544.9 yards,	2.736308

Then, in the triangle  $CAD$ , we have given the sides  $CA$  and  $AD$ , and the included angle  $CAD$ , to find  $CD$ ; to compute which we proceed thus:

The supplement of the angle  $CAD$ , is the sum of the angles  $ACD$  and  $ADC$ ;

Hence,  $\frac{ACD + ADC}{2} = 69^\circ 27'$ ; and, by proportion we have,

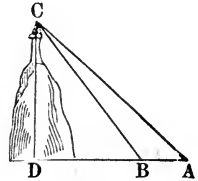
$AD + AC$	(= 940.8)	2.973497
: $AD - AC$	(= 149)	2.173186
:: tan. $\frac{ACD + ADC}{2}$	(= $69^\circ 27'$ )	10.426108
		12.599294

tan. $\frac{ACD - ADC}{2}$ ( $= 22^\circ 54'$ )	9.625797
the angle $ACD$ , sum, $92^\circ 21'$	
the angle $ADC$ , diff., $46^\circ 33'$	
Sin. $ADC$ , $46^\circ 33'$ ,	9.860922
: $AC$ , 395.9 yards,	2.597585
:: sin. $CAD$ , $41^\circ 6'$ ,	9.817813
	12.415398
: $CD$ , 358.5 yards,	2.554476

PROBLEM II.

To determine the altitude of a lighthouse, I observed the elevation of its top above the level sand on the sea-shore, to be  $15^\circ 32' 18''$ ; and measuring directly from it, 638 yards along the sand, I then found its elevation to be  $9^\circ 56' 26''$ . Required the height of the lighthouse

Let  $CD$  represent the height of the lighthouse above the level of the sand, and let  $B$  be the first station, and  $A$  the second; then the angle  $CBD$  is  $15^\circ 32' 18''$ , and the angle  $CAB$  is  $9^\circ 56' 26''$ ; therefore, the angle  $ACB$ , which is the difference of the angles  $CBD$  and  $CAB$ , is  $5^\circ 35' 52''$ .



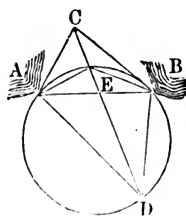
Hence, Sin. $ACB$ , $5^\circ 35' 52''$ ,	8.989201
: $AB$ , 638;	2.804821
:: sin. angle $A$ , $9^\circ 56' 26''$ ,	9.237107
	12.041928
: $BC$ , 1129.09 yards,	3.052727
Radius,	10.000000
· $BC$ , 1129.09,	3.052727
:: sin. $CBD$ , $15^\circ 32' 18''$ ,	9.427945
	12.480672
: $DC$ , 302.46 yards,	2.480672

## PROBLEM III.

Coming from sea, at the point  $D$  I observed two headlands,  $A$  and  $B$ , and inland, at  $C$ , a steeple, which appeared between the headlands. I found, from a map, that the headlands were 5.35 miles apart; that the distance from  $A$  to the steeple was 2.8 miles, and from  $B$  to the steeple 3.47 miles; and I found, with a sextant, that the angle  $ADC$  was  $12^\circ 15'$ , and the angle  $BDC$ ,  $15^\circ 30'$ . Required my distance from each of the headlands, and from the steeple.

## CONSTRUCTION.

The angle between the two headlands is the sum of  $15^\circ 30'$  and  $12^\circ 15'$ , or  $27^\circ 45'$ . Take double this sum,  $55^\circ 30'$ . Conceive  $AB$  to be the chord of a circle, and the arc on one side of it to be  $55^\circ 30'$ ; and, of course, the other will be  $304^\circ 30'$ . The point  $D$  will be somewhere in the circumference of this circle. Consider that point as determined, and draw  $CD$ .



In the triangle  $ABC$ , we have all the sides, and, of course, we can find all the angles; and if the angle  $ACB$  is less than  $180^\circ - 27^\circ 45' = 152^\circ 15'$ , then the circle cuts the line  $CD$  in a point  $E$ , and  $C$  is without the circle.

Draw  $AE$ ,  $BE$ ,  $AD$ , and  $BD$ .  $AEBD$  is a quadrilateral in a circle, and  $\angle AEB + \angle ADB = 180^\circ$ .

The  $\angle ADE =$  the  $\angle ABE$ , because both are measured by one half the arc  $AE$ . Also,  $\angle EDB = \angle EAB$ , for a similar reason.

Now, in the triangle  $AEB$ , its side  $AB$ , and all its angles, are known; and from thence  $AE$  can be computed. Then, having the two sides,  $AC$  and  $AE$ , of the triangle  $AEC$ , and the included angle  $CAE$ , we can find the angle  $AEC$ , and, of course, its supplement,  $AED$ . Then, in the triangle  $AED$ , we have the side  $AE$ , and the two angles  $AED$  and  $ADE$ , from which we can find  $AD$

The computation, at length, is as follows:

To find  $AE$ .

Angle $EAB = 15^\circ 30'$	Sin. $AEB, 152^\circ 15'$ , 9.668027	
Angle $EBA = 12^\circ 15'$	: $AB, 5.35,$	.728354
	<hr style="width: 50%; margin-left: 0;"/>	
27° 45'	:: sin. $ABE 12^\circ 15'$	9.326700
		<hr style="width: 50%; margin-left: 0;"/>
180°		10.055054
		<hr style="width: 50%; margin-left: 0;"/>
Angle $AEB = 152^\circ 15'$	: $AE, 2.438,$	.387027
		<hr style="width: 50%; margin-left: 0;"/>

To find the angle  $BAC$ .

$BC, 3.47$		
$AB, 5.35$	log. .728354	
$AC, 2.80$	log. .447158	
	<hr style="width: 50%; margin-left: 0;"/>	
2 ) 11.62		1.175512
		<hr style="width: 50%; margin-left: 0;"/>
5.81	log. .764176	
$BC, 2.34$	log. .369216	
		20
		<hr style="width: 50%; margin-left: 0;"/>
		21.133392
		<hr style="width: 50%; margin-left: 0;"/>
	2 ) 19.957880	
		<hr style="width: 50%; margin-left: 0;"/>
17° 41' 58"	cos. 9.978940	
2		<hr style="width: 50%; margin-left: 0;"/>
Angle $BAC = 35^\circ 23' 56''$		
Angle $EAB = 15^\circ 30'$		
		<hr style="width: 50%; margin-left: 0;"/>
Angle $EAC = 19^\circ 53' 56''$		
180°		
		<hr style="width: 50%; margin-left: 0;"/>
2 ) 160° 6' 4"		
		<hr style="width: 50%; margin-left: 0;"/>
80° 3' 2"		
		<hr style="width: 50%; margin-left: 0;"/>
	$\frac{AEC + ACE}{2}$	



To find the angles  $AEC$  and  $ACE$ .

$AC + AE$	5.238	.719165
: $AC - AE$	.362	— 1.558709
$\therefore \tan. \frac{AEC + ACE}{2}$	80° 3' 2"	<u>10.755928</u>
		<u>10.314637</u>
: $\tan. \frac{AEC - ACE}{2}$	<u>21° 30' 12"</u>	<u>9.595472</u>

angle  $AEC$ , 101° 33' 14", sum.

angle  $ACE$  or  $ACD$ , 58° 32' 50", diff.

angle  $GDA$ , 12° 15'

70° 47' 50", supplement 109° 12' 10", angle  $CAD$

35° 23' 56", angle  $CAB$

73° 48' 14", angle  $BAD$

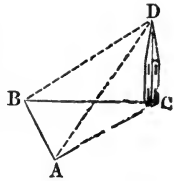
To find  $AD$ .

Sin. $ADC$ , 12° 15',	9.326700	
: $AC$ , 2.8,	.447158	
$\therefore \sin. ACD$ 58° 32' 50",	9.930985	
		<u>10.378143</u>
• $AD$ 11.26 miles.		<u>1.051443</u>

#### PROBLEM IV.

The elevation of a spire at one station was 23° 50' 17', and the horizontal angle at this station, between the spire and another station, was 93° 4' 20". The horizontal angle at the latter station, between the spire and the first station, was 54° 28' 36", and the distance between the two stations was 416 feet. Required the height of the spire.

Let  $CD$  be the spire,  $A$  the first station, and  $B$  the second; then the vertical angle  $CAD$  is  $23^\circ 50' 17''$ ; and as the horizontal angles,  $CAB$  and  $CBA$ , are  $93^\circ 4' 20''$  and  $54^\circ 28' 36''$ , respectively, the angle  $ACB$ , the supplement of their sum, is  $32^\circ 27' 4''$ .



To find  $AC$ .

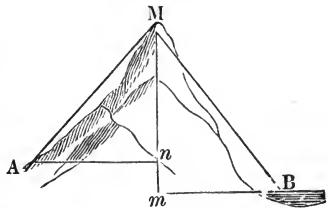
Sin. $BCA$ , $32^\circ 27' 3''$ ,	9.729634
: side $AB$ , 416,	2.619093
:: sin. $ABC$ , $54^\circ 28' 36''$ ,	9.910560
	12.529653
	2.800019
: side $AC$ , 631,	

To find  $DC$ .

Radius,	10.000000
: side $AC$ , 631,	2.800019
:: tan. $DAC$ , $23^\circ 50' 17''$ ,	9.645270
	2.445289
: $DC$ , 278.8,	

By the application of Problem 4, we can compute the distance between two horizontal planes, if the same object is visible from both.

For example, let  $M$  be a prominent tree or rock near the top of a mountain, and by observations taken at  $A$ , we can determine the perpendicular  $Mn$ . By like observations taken at  $B$ , we can determine the perpendicular  $Mm$ . The difference between these two perpendiculars is  $nm$ , or the difference in the elevation between the two points  $A$  and  $B$ . If the distances between  $A$  and  $n$ , or  $B$  and  $m$ , are considerable, or more than two or three miles, corrections must be made for the convexity of the earth; but for less distances such corrections are not necessary.



## PRACTICAL PROBLEMS.

1. Required the height of a wall whose angle of elevation, at the distance of 463 feet, is observed to be  $16^{\circ} 21'$ . *Ans.* 135.8 feet.

2. The angle of elevation of a hill is, near its bottom,  $31^{\circ} 18'$ , and 214 yards further off,  $26^{\circ} 18'$ . Required the perpendicular height of the hill, and the distance of the perpendicular from the first station.

*Ans.* { The height of the hill is 565.2 yards, and the distance of the perpendicular from the first station is 929.6 yards.

3. The wall of a tower which is 149.5 feet in height, makes, with a line drawn from the top of it to a distant object on the horizontal plane, an angle of  $57^{\circ} 21'$ . What is the distance of the object from the bottom of the tower? *Ans.* 233.3 feet.

4. From the top of a tower, which is 138 feet in height, I took the angle of depression of two objects standing in a direct line from the bottom of the tower, and upon the same horizontal plane with it. The depression of the nearer object was found to be  $48^{\circ} 10'$ , and that of the further,  $18^{\circ} 52'$ . What was the distance of each from the bottom of the tower?

*Ans.* { Distance of the nearer, 123.5 feet; and of the further, 403.8 feet.

5. Being on the side of a river, and wishing to know the distance of a house on the opposite side, I measured 312 yards in a right line by the side of the river, and then found that the two angles, one at each end of this line, subtended by the other end and the house, were  $31^{\circ} 15'$  and  $86^{\circ} 27'$ . What was the distance between each end of the line and the house? *Ans.* 351.7, and 182.8 yards.

6. Having measured a base of 260 yards in a straight line, on one bank of a river, I found that the two angles, one at each end of the line, subtended by the

other end and a tree on the opposite bank, were  $40^\circ$  and  $80^\circ$ . What was the width of the river?

*Ans.* 190.1 yards.

7. From an eminence of 268 feet in perpendicular height, the angle of depression of the top of a steeple which stood on the same horizontal plane, was found to be  $40^\circ 3'$ , and of the bottom,  $56^\circ 18'$ . What was the height of the steeple?

*Ans.* 117.76 feet.

8. Wanting to know the distance between two objects which were separated by a morass, I measured the distance from each to a point from whence both could be seen; the distances were 1840 and 1428 yards, and the angle which, at that point, the objects subtended, was  $36^\circ 18' 24''$ . Required their distance. *Ans.* 1090.85 yards.

9. From the top of a mountain, three miles in height, the visible horizon appeared depressed  $2^\circ 13' 27''$ . Required the diameter of the earth, and the distance of the boundary of the visible horizon.

*Ans.*  $\left\{ \begin{array}{l} \text{Diameter of the earth, 7958 miles; distance of} \\ \text{the horizon, 154.54 miles.} \end{array} \right.$

10. From a ship a headland was seen, bearing north  $39^\circ 23'$  east. After sailing 20 miles north,  $47^\circ 49'$  west, the same headland was observed to bear north,  $87^\circ 11'$  east. Required the distance of the headland from the ship at each station.

*Ans.*  $\left\{ \begin{array}{l} \text{At first station, 19.09 miles; at the second,} \\ \text{26.96 miles.} \end{array} \right.$

11. The top of a tower, 100 feet above the level of the sea, was seen as on the surface of the sea, from the mast-head of a ship, 90 feet above the water. The diameter of the earth being 7960 miles, what was the distance between the observer and the object?

*Ans.* 23.92 plus  $\frac{1}{3}$  for refraction = 25.76 miles.

12. From the top of a tower, by the seaside, 143 feet high, it was observed that the angle of depression of a

ship's bottom, then at anchor, measured  $35^\circ$ ; what, then, was the ship's distance from the foot of the tower?

*Ans.* 204.22 feet.

13. Wanting to know the breadth of a river, I measured a base of 500 yards in a straight line on one bank; and at each end of this line I found the angles subtended by the other end and a tree on the opposite bank of the river, to be  $53^\circ$  and  $79^\circ 12'$ . What, then, was the perpendicular breadth of the river? *Ans.* 529.48 yards.

14. What is the perpendicular height of a hill, its angle of elevation, taken at the bottom of it, being  $46^\circ$ , and 200 yards further off, on a level with the bottom,  $31^\circ$ ? *Ans.* 286.28 yards.

15. Wanting to know the height of an inaccessible tower, at the least accessible distance from it, on the same horizontal plane, I found its angle of elevation to be  $58^\circ$ ; then going 300 feet directly from it, I found the angle there to be only  $32^\circ$ ; required the height of the tower, and my distance from it at the first station.

*Ans.*  $\left\{ \begin{array}{l} \text{Height, } 307.54 \text{ feet.} \\ \text{Distance, } 192.18 \text{ "} \end{array} \right.$

16. Two ships of war, intending to cannonade a fort, are, by the shallowness of the water, kept so far from it, that they suspect their guns cannot reach it with effect. In order, therefore, to measure the distance, they separate from each other a quarter of a mile, or 440 yards, and then each ship observes and measures the angle which the other ship and fort subtends; these angles are  $83^\circ 45'$ , and  $85^\circ 15'$ . What, then, is the distance between each ship and the fort?

*Ans.*  $\left\{ \begin{array}{l} 2292.26 \text{ yards.} \\ 2298.05 \text{ "} \end{array} \right.$

17. A point of land was observed by a ship, at sea, to bear east-by-south;\* and after sailing north-east 12 miles,

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\* That is, one point south of east. A point of the compass is  $11^\circ 15'$ .

it was found to bear south-east-by-east. It is required to determine the place of that headland, and the ship's distance from it at the last observation.

*Ans.* Distance, 26.0728 miles.

18. Wishing to know my distance from an inaccessible object,  $O$ , on the opposite side of a river, and having a chain or chord for measuring distances, but no instrument for taking angles; from each of two stations,  $A$  and  $B$ , which were taken at 500 yards asunder, I measured in a direct line from the object,  $O$ , 100 yards, viz.,  $AC$  and  $BD$ , each equal to 100 yards; and I found that the diagonal  $AD$  measured 550 yards, and the diagonal  $BC$  560. What, then, was the distance of the object  $O$  from each station  $A$  and  $B$ ?

*Ans.*  $\begin{cases} AO, 536.27 \text{ yards.} \\ BO, 500.14 \text{ "} \end{cases}$

19. A navigator found, by observation, that the summit of a certain mountain, which he supposed to be 45 minutes of a degree distant, had an altitude above the sea horizon of  $31' 20''$ . Now, on the supposition that the earth's radius is 3956 miles, and the observer's *dip* was  $4' 15''$ , what was the height of the mountain?

*Ans.* 3960 feet.

REMARK.—This should be diminished by about one eleventh part of itself, for the influence of horizontal refraction.

20. From two ships,  $A$  and  $B$ , which are anchored in a bay, two objects,  $C$  and  $D$ , on the shore, can be seen. These objects are known to be 500 yards apart. At the ship  $A$ , the angle subtended by the objects was measured, and found to be  $41^\circ 25'$ ; and that by the object  $D$  and the other ship was found to be  $52^\circ 12'$ . At the other ship, the angle subtended by the objects on shore was found to be  $48^\circ 10'$ ; and that by the object  $C$ , and the ship  $A$ , to be  $47^\circ 40'$ . Required the distance between

the ships, and the distance from each ship to the objects on shore.

$$\text{Ans. } \left\{ \begin{array}{l} \text{Distance between ships, } 395.7 \text{ yards.} \\ \text{From ship } A \text{ to object } D, 743.5 \text{ " } \\ \text{From ship } A \text{ to object } C, 467.7 \text{ " } \\ \text{From ship } B \text{ to object } D, 590.5 \text{ " } \end{array} \right.$$

To solve this problem, suppose the distance between the ships to be 100 yards, and determine the several distances, including the distance between the objects,  $C$  and  $D$ , under this supposition; then multiply the values thus found for the required distances by the quotient obtained by dividing the given value of  $CD$  by the computed value.

PART II.  
SPHERICAL GEOMETRY  
AND  
TRIGONOMETRY.

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SECTION I.  
SPHERICAL GEOMETRY.

DEFINITIONS.

**1.** Spherical Geometry has for its object the investigation of the properties, and of the relations to each other, of the portions of the surface of a sphere which are bounded by the arcs of its great circles.

**2.** A Spherical Polygon is a portion of the surface of a sphere bounded by three or more arcs of great circles, called the *sides* of the polygon.

**3.** The Angles of a spherical polygon are the angles formed by the bounding arcs, and are the same as the angles formed by the planes of these arcs.

**4.** A Spherical Triangle is a spherical polygon having but three sides, each of which is less than a semi-circumference.

**5.** A Lune is a portion of the surface of a sphere included between two great semi-circumferences having a common diameter.

**6.** A Spherical Wedge, or Ungula, is a portion of the solid sphere included between two great semi-circles having a common diameter.



**7.** A **Spherical Pyramid** is a portion of a sphere bounded by the faces of a solid angle having its vertex at the center, and the spherical polygon which these faces intercept on the surface. This spherical polygon is called the *base* of the pyramid.

**8.** The **Axis** of a great circle of a sphere is that diameter of the sphere which is perpendicular to the plane of the circle. This diameter is also the axis of all small circles parallel to the great circle.

**9.** A **Pole** of a circle of a sphere is a point on the surface of the sphere equally distant from every point in the circumference of the circle.

**10.** **Supplemental, or Polar Triangles**, are two triangles on a sphere, so related that the vertices of the angles of either triangle are the poles of the sides of the other

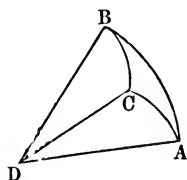
## PROPOSITION I.

*Any two sides of a spherical triangle are together greater than the third side.*

Let  $AB$ ,  $AC$ , and  $BC$ , be the three sides of the triangle, and  $D$  the center of the sphere.

The angles of the planes that form the solid angle at  $D$ , are measured by the arcs  $AB$ ,  $AC$ , and  $BC$ . But any two of these angles are together greater than the third angle, (Th. 18, B. VI). Therefore, any two sides of the triangle are, together, greater than the third side.

Hence the proposition.

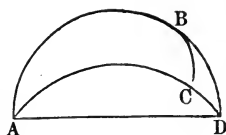


## PROPOSITION II.

*The sum of the three sides of any spherical triangle is less than the circumference of a great circle.*

Let  $ABC$  be a spherical triangle; the two sides,  $AB$  and  $AC$ , produced, will meet at the point which is diametrically opposite to  $A$ , and the arcs,  $ABD$  and  $ACD$  are

together equal to a great circle. But, by the last proposition,  $BC$  is less than the two arcs,  $BD$  and  $DC$ . Therefore,  $AB + BC + AC$ , is less than  $ABD + ACD$ ; that is, less than a great circle.

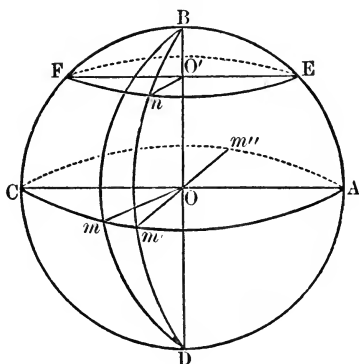


Hence the proposition.

### PROPOSITION III.

*The extremities of the axis of a great circle of a sphere are the poles of the great circle, and these points are also the poles of all small circles parallel to the great circle.*

Let  $O$  be the center of the sphere, and  $BD$  the axis of the great circle,  $Cm Am''$ ; then will  $B$  and  $D$ , the extremities of the axis, be the poles of the circle, and also the poles of any parallel small circle, as  $FnE$ .



For, since  $BD$  is perpendicular to the plane of the circle,  $Cm Am''$ , it is perpendicular to the lines  $OA$ ,  $Om'$ ,  $Om''$ , etc., passing through its foot in the plane, (Def. 2, B. VI); hence, all the arcs,  $Bm$ ,  $Bm'$ , etc., are quadrants, as are also the arcs  $Dm$ ,  $Dm'$ , etc. The points  $B$  and  $D$  are, therefore, each equally distant from all the points in the circumference,  $Cm Am''$ ; hence, (Def. 9), they are its poles.

Again, since the radius,  $OB$ , is perpendicular to the plane of the circle,  $Cm Am''$ , it is also perpendicular to the plane of the parallel small circle,  $FnE$ , and passes through its center,  $O'$ . Now, the chords of the arcs,  $BF$ ,  $Bn$ ,  $BE$ , etc., being oblique lines, meeting the plane of the small circle at equal distances from the foot of the

perpendicular,  $BO'$ , are all equal, (Th. 4, B. VI); hence, the arcs themselves are equal, and  $B$  is one pole of the circle,  $FnE$ . In like manner we prove the arcs,  $DF$ ,  $Dn$ ,  $DE$ , etc., equal, and therefore  $D$  is the other pole of the same circle.

Hence the proposition, etc.

*Cor. 1. A point on the surface of a sphere at the distance of a quadrant from two points in the arc of a great circle, not at the extremities of a diameter, is a pole of that arc.*

For, if the arcs,  $Bm$ ,  $Bm'$ , are each quadrants, the angles,  $BOm$  and  $BOm'$ , are each right angles; and hence,  $BO$  is perpendicular to the plane of the lines,  $Om$  and  $Om'$ , which is the plane of the arc,  $m m'$ ;  $B$  is therefore the pole of this arc.

*Cor. 2. The angle included between the arc of a great circle and the arc of another great circle, connecting any of its points with the pole, is a right angle.*

For, since the radius,  $BO$ , is perpendicular to the plane of the circle,  $Cm Am''$ , every plane passed through this radius is perpendicular to the plane of the circle; hence, the plane of the arc  $Bm$  is perpendicular to that of the arc  $Cm$ ; and the angle of the arcs is that of their planes.

#### PROPOSITION IV.

*The angle formed by two arcs of great circles which intersect each other, is equal to the angle included between the tangents to these arcs at their point of intersection, and is measured by that arc of a great circle whose pole is the vertex of the angle, and which is limited by the sides of the angle or the sides produced.*

Let  $AM$  and  $AN$  be two arcs intersecting at the point  $A$ , and let  $AE$  and  $AF$  be the tangents to these arcs at this point. Take  $AC$  and  $AD$ , each quadrants, and draw the arc  $CD$ , of which  $A$  is the pole, and  $OC$  and  $OD$  are the radii.

Now, since the planes of the arcs intersect in the radius  $OA$ , and  $AE$  is a tangent to one arc, and  $AF$  a tangent to the other, at the common point  $A$ , these tangents form with each other an angle which is the measure of the angle of the planes of the arcs; but the angle of the planes of the arcs is taken as the angle included by the arcs, (Def. 3).

Again, because the arcs,  $AC$  and  $AD$ , are each quadrants, the angles,  $AOC$ ,  $AOD$ , are right angles; hence the radii,  $OC$  and  $OD$ , which lie, one in one face, and the other in the other face, of the diedral angle formed by the planes of the arcs, are perpendicular to the common intersection of these faces at the same point. The angle,  $COD$ , is therefore the angle of the planes, and consequently the angle of the arcs; but the angle  $COD$  is measured by the arc  $CD$ .

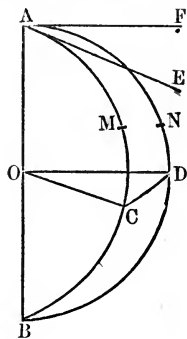
Hence the proposition.

*Cor. 1.* Since the angles included between the arcs of great circles on a sphere, are measured by other arcs of great circles of the same sphere, we may compare such angles with each other, and construct angles equal to other angles, by processes which do not differ in principle from those by which plane angles are compared and constructed.

*Cor. 2.* Two arcs of great circles will form, by their intersection, four angles, the opposite or vertical ones of which will be equal, as in the case of the angles formed by the intersection of straight lines, (Th. 4, B. I).

#### PROPOSITION V.

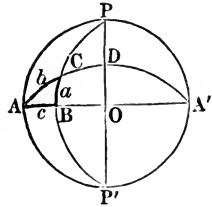
*The surface of a hemisphere may be divided into three right-angled and four quadrantal triangles, and one of these right-angled triangles will be so related to the other two, that two of its sides and one of its angles will be complementary to the*



sides of one of them, and two of its sides supplemental to two of the sides of the other.

Let  $ABC$  be a right-angled spherical triangle, right angled at  $B$ .

Produce the sides,  $AB$  and  $AC$ , and they will meet at  $A'$ , the opposite point on the sphere. Produce  $BC$ , both ways,  $90^\circ$  from the point  $B$ , to  $P$  and  $P'$ , which are, therefore, poles to the arc  $AB$ , (Prop. 3). Through  $A$ ,  $P$ , and the center of the sphere, pass a plane, cutting the sphere into two equal parts, forming a great circle on the sphere, which great circle will be represented by the circle  $PAP'A'$  in the figure. At right angles to this plane, pass another plane, cutting the sphere into two equal parts; this great circle is represented in the figure by the straight line,  $POP'$ .  $A$  and  $A'$  are the poles to the great circle,  $POP'$ ; and  $P$  and  $P'$  are the poles to the great circle,  $ABA'$ .



Now,  $CPD$  is a spherical triangle, right-angled at  $D$ , and its sides  $CP$  and  $CD$  are complementary respectively to the sides  $BC$  and  $AC$  of the  $\triangle ABC$ , and its side  $PD$  is complementary to the arc  $DO$ , which measures the  $\sphericalangle BAC$  of the same triangle. Again, the  $\triangle A'BC$  is right-angled at  $B$ , and its sides  $A'C$ ,  $A'B$ , are supplemental respectively to the sides  $AC$ ,  $AB$ , of the  $\triangle ABC$ . Therefore, the three right-angled  $\triangle$ 's,  $ABC$ ,  $CPD$ , and  $A'BC$ , have the required relations. In the  $\triangle ACP$ , the side  $AP$  is a quadrant, and for this reason the  $\triangle$  is called a quadrantal triangle. So also, are the  $\triangle$ 's  $A'CP$ ,  $ACP'$ , and  $P'CA'$ , quadrantal triangles. Hence the proposition.

**SCHOLIUM.**—In every triangle there are *six* elements, three sides and three angles, called the parts of the triangle.

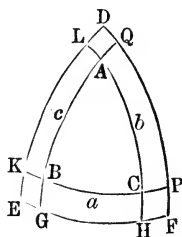
Now, if all the parts of the triangle  $ABC$  are known, the parts of each of the  $\triangle$ 's,  $PCD$  and  $A'BC$ , are as completely known. And when the parts of the  $\triangle PCD$  are known, the parts of the  $\triangle ACP$

and  $A'CP$  are also known; for, the side  $PD$  measures each of the  $\sphericalangle$ 's  $PAC$  and  $PA'C$ , and the angle  $CPD$ , added to the right angle  $A'PD$ , gives the  $\sphericalangle A'PC$ , and the  $\sphericalangle CPA$  is supplemental to this. Hence, the solution of the  $\triangle ABC$  is a solution of the two right-angled and four quadrantal  $\triangle$ 's, which together with it make up the surface of the hemisphere.

### PROPOSITION VI.

*If there be three arcs of great circles whose poles are the angular points of a spherical triangle, such arcs, if produced, will form another triangle, whose sides will be supplemental to the angles of the first triangle, and the sides of the first triangle will be supplemental to the angles of the second.*

Let the arcs of the three great circles be  $GH$ ,  $PQ$ ,  $KL$ , whose poles are respectively  $A$ ,  $B$ , and  $C$ . Produce the three arcs until they meet in  $D$ ,  $E$ , and  $F$ . We are now to prove that  $E$  is the pole of the arc  $AC$ ;  $D$  the pole of the arc  $BC$ ;  $F$  the pole to the arc  $AB$ . Also, that the side  $EF$ , is supplemental to the angle  $A$ ;  $ED$  to the angle  $C$ ; and  $DF$  to the angle  $B$ ; and also, that the side  $AC$  is supplemental to the angle  $E$ , etc.



A pole is  $90^\circ$  from any point in the circumference of its great circle; and, therefore, as  $A$  is the pole of the arc  $GH$ , the point  $A$  is  $90^\circ$  from the point  $E$ . As  $C$  is the pole of the arc  $LK$ ,  $C$  is  $90^\circ$  from any point in that arc; therefore,  $C$  is  $90^\circ$  from the point  $E$ ; and  $E$  being  $90^\circ$  from both  $A$  and  $C$ , it is the pole of the arc  $AC$ . In the same manner, we may prove that  $D$  is the pole of  $BC$ , and  $F$  the pole of  $AB$ .

Because  $A$  is the pole of the arc  $GH$ , the arc  $GH$  measures the angle  $A$ , (Prop. 4); for a similar reason,  $PQ$  measures the angle  $B$ , and  $LK$  measures the angle  $C$ .

Because  $E$  is the pole of the arc  $AC$ ,  $EH = 90^\circ$

Or,  $EG + GH = 90^\circ$

For a like reason,  $FH + GH = 90^\circ$

Adding these two equations, and observing that  $GH = A$ , and afterward transposing one  $A$ , we have,

$$EG + GH + FH = 180^\circ - A.$$

$$\left. \begin{array}{l} \text{Or,} \\ \text{In like manner,} \\ \text{And,} \end{array} \right\} \begin{array}{l} EF = 180^\circ - A \\ FD = 180^\circ - B \\ DE = 180^\circ - C \end{array} \quad (a)$$

But the arc  $(180^\circ - A)$ , is a supplemental arc to  $A$ , by the definition of arcs; therefore, the three sides of the triangle  $DEF$ , are supplements of the angles  $A, B, C$ , of the triangle  $ABC$ .

Again, as  $E$  is the pole of the arc  $AC$ , the whole angle  $E$  is measured by the whole arc  $LH$ .

$$\begin{array}{l} \text{But,} \\ \text{Also,} \end{array} \quad \begin{array}{l} AC + CH = 90^\circ \\ AC + AL = 90^\circ \end{array}$$

$$\text{By addition, } AC + AC + CH + AL = 180^\circ$$

$$\text{By transposition, } AC + CH + AL = 180^\circ - AC$$

$$\left. \begin{array}{l} \text{That is,} \\ \text{In the same manner,} \\ \text{And,} \end{array} \right\} \begin{array}{l} LH, \text{ or } E = 180^\circ - AC \\ F = 180^\circ - AB \\ D = 180^\circ - BC \end{array} \quad (b)$$

That is, the sides of the first triangle are supplemental to the angles of the second triangle.

#### PROPOSITION VII.

*The sum of the three angles of any spherical triangle, is greater than two right angles, and less than six right angles.*

Add equations (a), of the last proposition. The first member of the equation so formed will be the sum of the three sides of a spherical triangle, which sum we may designate by  $S$ . The second member will be 6 right angles (there being 2 right angles in each  $180^\circ$ ) less the three angles  $A, B$ , and  $C$ .

$$\text{That is,} \quad S = 6 \text{ right angles} - (A + B + C)$$

By Prop. 2, the sum  $S$  is less than 4 right angles;

therefore, to it add  $s$ , a sufficient quantity to make 4 right angles. Then,

$$4 \text{ right angles} = 6 \text{ right angles} - (A + B + C) + s$$

Drop or cancel 4 right angles from both members, and transpose  $(A + B + C)$ .

$$\text{Then,} \quad A + B + C = 2 \text{ right angles} + s.$$

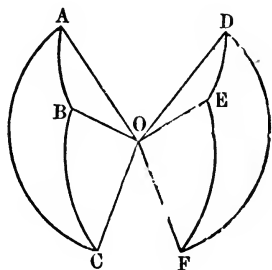
That is, the three angles of a spherical triangle make a greater sum than two right angles by the indefinite quantity  $s$ , which quantity is called the *spherical excess*, and is greater or less according to the size of the triangle.

Again, the sum of the angles is less than 6 right angles. There are but *three* angles in any triangle, and each one of them must be less than  $180^\circ$ , or 2 right angles. For, an angle is the inclination of two lines or two planes; and when two planes incline by  $180^\circ$ , the planes are parallel, or are in one and the same plane; therefore, as neither angle can be equal to 2 right angles, the three can never be equal to 6 right angles.

### PROPOSITION VIII.

*On the same sphere, or on equal spheres, triangles which are mutually equilateral are also mutually equiangular; and, conversely, triangles which are mutually equiangular are also mutually equilateral, equal sides lying opposite equal angles.*

*First.*—Let  $ABC$  and  $DEF$ , in which  $AB = DE$ ,  $AC = DF$ , and  $BC = EF$ , be two triangles on the sphere whose center is  $O$ ; then will the  $\sphericalangle A$ , opposite the side  $BC$ , in the first triangle, be equal the  $\sphericalangle D$ , opposite the equal side  $EF$ , in the second; also  $\sphericalangle B = \sphericalangle E$ , and  $\sphericalangle C = \sphericalangle F$ .





For, drawing the radii to the vertices of the angles of these triangles, we may conceive  $O$  to be the common vertex of two triedral angles, one of which is bounded by the plane angles  $AOB$ ,  $BOC$ , and  $AOC$ , and the other by the plane angles  $DOE$ ,  $EOF$ , and  $DOF$ . But the plane angles bounding the one of these triedral angles, are equal to the plane angles bounding the other, each to each, since they are measured by the equal sides of the two triangles. The planes of the equal arcs in the two triangles are therefore equally inclined to each other, (Th. 20, B. VI); but the angles included between the planes of the arcs are equal to the angles formed by the arcs, (Def. 3).

Hence the  $\sphericalangle A$ , opposite the side  $BC$ , in the  $\triangle AOB$  is equal to the  $\sphericalangle D$ , opposite the equal side  $EF$ , in the other triangle; and for a similar reason, the  $\sphericalangle B = \sphericalangle E$ , and the  $\sphericalangle C = \sphericalangle F$ .

*Second.*—If, in the triangles  $ABC$  and  $DEF$ , being on the same sphere whose center is  $O$ , the  $\sphericalangle A = \sphericalangle D$ , the  $\sphericalangle B = \sphericalangle E$ , and the  $\sphericalangle C = \sphericalangle F$ ; then will the side  $AB$ , opposite the  $\sphericalangle C$ , in the first, be equal to the side  $DE$ , opposite the equal  $\sphericalangle F$ , in the second; and also the side  $AC$  equal to the side  $DF$ , and the side  $BC$  equal to the side  $EF$ .

For, conceive two triangles, denoted by  $A'B'C'$  and  $D'E'F'$ , supplemental to  $ABC$  and  $DEF$ , to be formed; then will these supplemental triangles be mutually equilateral, for their sides are measured by  $180^\circ$  less the opposite and equal angles of the triangles  $ABC$  and  $DEF$ , (Prop. 6); and being mutually equilateral, they are, as proved above, mutually equiangular. But the triangles  $ABC$  and  $DEF$  are supplemental to the triangles  $A'B'C'$  and  $D'E'F'$ ; and their sides are therefore measured severally by  $180^\circ$  less the opposite and equal angles of the triangles  $A'B'C'$  and  $D'E'F'$ , (Prop. 6).

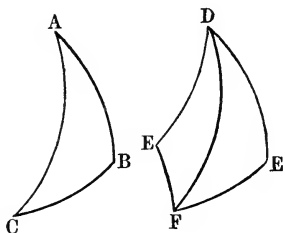
Hence the triangles  $ABC$  and  $DEF$ , which are mutually equiangular, are also mutually equilateral.

SCHOLIUM.—With the three arcs of great circles,  $AB$ ,  $AC$ , and  $BC$  either of the two triangles,  $ABC$ ,  $DEF$ , may be formed; but 't is evident that these two triangles cannot be made to coincide, though they are both mutually equilateral and mutually equiangular. Spherical triangles on the same sphere, or on equal spheres, in which the sides and angles of the one are equal to the sides and angles of the other each to each, but are not themselves capable of superposition, are called *symmetrical triangles*.

### PROPOSITION IX.

*On the same sphere, or on equal spheres, triangles having two sides of the one equal to two sides of the other, each to each, and the included angles equal, have their remaining sides and angles equal.*

Let  $ABC$  and  $DEF$  be two triangles, in which  $AB = DE$ ,  $AC = DF$ , and the angle  $A =$  the angle  $D$ ; then will the side  $BC$  be equal to the side  $FE$ , the  $\sphericalangle B =$  the  $\sphericalangle E$ , and  $\sphericalangle C =$   $\sphericalangle F$ .



For, if  $DE$  lies on the same side of  $DF$  that  $AB$  does of  $AC$ , the two triangles,  $ABC$  and  $DEF$ , may be applied the one to the other, and they may be proved to coincide, as in the case of plane triangles. But, if  $DE$  does not lie on the same side of  $DF$  that  $AB$  does of  $AC$ , we may construct the triangle which is symmetrical with  $DEF$ ; and this symmetrical triangle, when applied to the triangle  $ABC$ , will exactly coincide with it. But the triangle  $DEF$ , and the triangle symmetrical with it, are not only mutually equilateral, but also are mutually equiangular, the equal angles lying opposite the equal sides, (Prop. 8); and as the one or the other will coincide with the triangle  $ABC$ , it follows that

the triangles,  $ABC$  and  $DEF$ , are either absolutely or symmetrically equal.

*Cor.* On the same sphere, or on equal spheres, triangles having two angles of the one equal to two angles of the other, each to each, and the included sides equal, have their remaining sides and angles equal.

For, if  $\sphericalangle A = \sphericalangle D$ ,  $\sphericalangle B = \sphericalangle E$ , and side  $AB =$  side  $DE$ , the triangle  $DEF$ , or the triangle symmetrical with it, will exactly coincide with  $\triangle ABC$ , when applied to it as in the case of plane triangles; hence, the sides and angles of the one will be equal to the sides and angles of the other, each to each.

### PROPOSITION X.

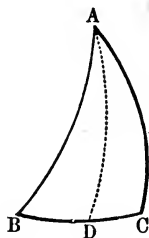
*In an isosceles spherical triangle, the angles opposite the equal sides are equal.*

Let  $ABC$  be an isosceles spherical triangle, in which  $AB$  and  $AC$  are the equal sides; then will  $\sphericalangle B = \sphericalangle C$ .

For, connect the vertex  $A$  with  $D$ , the middle point of the base, by the arc of a great circle, thus forming the two mutually equilateral triangles,  $ADB$  and  $ADC$ .

They are mutually equilateral, because  $AD$  is common,  $BD = DC$  by construction, and  $AB = AC$  by supposition; hence they are mutually equiangular, the equal angles being opposite the equal sides, (Prop. 8). The angles  $B$  and  $C$ , being opposite the common side  $AD$ , are therefore equal.

*Cor.* The arc of a great circle which joins the vertex of an isosceles spherical triangle with the middle point of the base, is perpendicular to the base, and bisects the vertical angle of the triangle; and, conversely, the arc of a



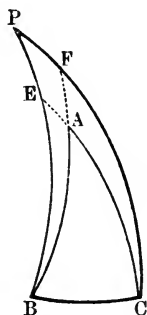
great circle which bisects the vertical angle of an isosceles spherical triangle, is perpendicular to, and bisects the base.

PROPOSITION XI.

*If two angles of a spherical triangle are equal, the opposite sides are also equal, and the triangle is isosceles.*

In the spherical triangle,  $ABC$ , let the  $\sphericalangle B = \sphericalangle C$ ; then will the sides,  $AB$  and  $AC$ , opposite these equal angles, be equal.

For, let  $P$  be the pole of the base,  $BC$ , and draw the arcs of great circles,  $PB$ ,  $PC$ ; these arcs will be quadrants, and at right angles to  $BC$ , (Cor. 2, Prop. 3). Also, produce  $CA$  and  $BA$  to meet  $PB$  and  $PC$ , in the points  $E$  and  $F$ . Now, the angles,  $PBF$  and  $PCE$ , are equal, because the first is equal to  $90^\circ$  less the  $\sphericalangle ABC$ , and the second is equal to  $90^\circ$  less the equal  $\sphericalangle ACB$ ; hence, the  $\triangle$ 's,  $PBF$  and  $PCE$ , are equal in all their parts, since they have the  $\sphericalangle P$  common, the  $\sphericalangle PBF = \sphericalangle PCE$ , and the side  $PB$  equal to the side  $PC$ , (Cor., Prop. 9).  $PE$  is therefore equal to  $PF$ , and  $\sphericalangle PEC = \sphericalangle PFB$ .



Taking the equals  $PF$  and  $PE$ , from the equals  $PC$  and  $PB$ , we have the remainders,  $FC$  and  $EB$ , equal; and, from  $180^\circ$ , taking the  $\sphericalangle$ 's  $PFB$  and  $PEC$ , we have the remaining  $\sphericalangle$ 's,  $AFC$  and  $AEB$ , equal. Hence, the  $\triangle$ 's,  $AFC$  and  $AEB$ , have two angles of the one equal to two angles of the other, each to each, and the included sides equal; the remaining sides and angles are therefore equal, (Cor., Prop. 9). Therefore,  $AC$  is equal to  $BA$ , and the  $\triangle ABC$  is isosceles.

*Cor.* An equiangular spherical triangle is also equilateral, and the converse.

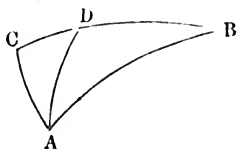
**REMARK.**—In this demonstration, the pole of the base,  $BC$ , is supposed to fall without the triangle,  $ABC$ . The same figure may be used for the case in which the pole falls within the triangle; the modification the demonstration then requires is so slight and obvious, that it would be superfluous to suggest it.

## PROPOSITION XII.

*The greater of two sides of a spherical triangle is opposite the greater angle; and, conversely, the greater of two angles of a spherical triangle is opposite the greater side.*

Let  $ABC$  be a spherical triangle, in which the angle  $A$  is greater than the angle  $B$ ; then is the side  $BC$  greater than the side  $AC$ .

Through  $A$  draw the arc of a great circle,  $AD$ , making, with  $AB$ , the angle  $BAD$  equal to the angle  $ABD$ . The triangle,  $DAB$ , is isosceles, and  $DA = DB$ , (Prop. 11).



In the  $\triangle ACD$ ,  $CD + AD > AC$ , (Prop. 1.); or, substituting for  $AD$  its equal  $DB$ , we have,

$$CD + DB > AC.$$

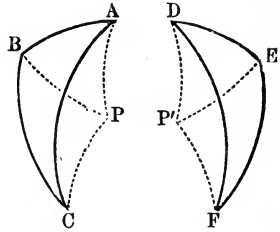
If in the above inequality we now substitute  $CB$  for  $CD + DB$ , it becomes  $CB > CA$ .

Conversely; if the side  $CB$  be greater than the side  $CA$ , then is the  $\sphericalangle A >$  the  $\sphericalangle B$ . For, if the  $\sphericalangle A$  is not greater than the  $\sphericalangle B$ , it is either equal to it, or less than it. The  $\sphericalangle A$  is not equal to the  $\sphericalangle B$ ; for if it were, the triangle would be isosceles, and  $CB$  would be equal to  $CA$ , which is contrary to the hypothesis. The  $\sphericalangle A$  is not less than the  $\sphericalangle B$ ; for if it were, the side  $CB$  would be less than the side  $CA$ , by the first part of the proposition, which is also contrary to the hypothesis; hence, the  $\sphericalangle A$  must be greater than the  $\sphericalangle B$ .

## PROPOSITION XIII.

*Two symmetrical spherical triangles are equal in area.*

Let  $ABC$  and  $DEF$  be two  $\Delta$ 's on the same sphere, having the sides and angles of the one equal to the sides and angles of the other, each to each, the triangles themselves not admitting of superposition. It is to be proved that these  $\Delta$ 's have equal areas.



Let  $P$  be the pole of a small circle passing through the three points,  $A, B,$  and  $C,$  and connect  $P$  with each of the points,  $A, B,$  and  $C,$  by arcs of great circles. Next, through  $E$  draw the arc of a great circle,  $EP',$  making the angle  $DEP'$  equal to the angle  $ABP.$  Take  $EP' = BP,$  and draw the arcs of great circles,  $P'D, P'F.$

The  $\Delta$ 's,  $ABP$  and  $DEP',$  are equal in all their parts, because  $AB = DE, BP = EP',$  and the  $\sphericalangle ABP = \sphericalangle DEP',$  (Prop. 9). Taking from the  $\sphericalangle ABC$  the  $\sphericalangle ABP,$  and from the  $\sphericalangle DEF$  the  $\sphericalangle DEP',$  we have the remaining angles,  $PBC$  and  $P'EF,$  equal; and therefore the  $\Delta$ 's,  $BPC$  and  $EP'F,$  are also equal in all their parts.

Now, since the  $\Delta$ 's,  $ABP$  and  $DEP',$  are isosceles, they will coincide when applied, as will also the  $\Delta$ 's,  $BPC$  and  $EP'F,$  for the same reason. The polygonal areas,  $ABCP$  and  $DEFP',$  are therefore equivalent. If from the first we take the isosceles triangle,  $PAC,$  and from the second the equal isosceles triangle,  $P'DF,$  the remainders, or the triangles  $ABC$  and  $DEF,$  will be equivalent.

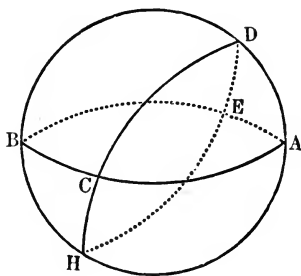
REMARK.—It is assumed in this demonstration that the pole  $P$  falls without the triangle. Were it to fall within, instead of without, no other change in the above process would be required than to add the isosceles triangles,  $PAC, P'DF,$  to the polygonal areas, to get the areas of the triangles,  $ABC, DEF.$

*Cor.* Two spherical triangles on the same sphere, or on equal spheres, will be equivalent — 1st, when they are mutually equilateral; — 2d, when they are mutually equiangular; — 3d, when two sides of the one are equal to two sides of the other, each to each, and the included angles are equal; — 4th, when two angles of the one are equal to two angles of the other, each to each, and the included sides are equal.

## PROPOSITION XIV.

*If two arcs of great circles intersect each other on the surface of a hemisphere, the sum of either two of the opposite triangles thus formed will be equivalent to a lune whose angle is the corresponding angle formed by the arcs.*

Let the great circle,  $AEB C$ , be the base of a hemisphere, on the surface of which the great semi-circumferences,  $BDA$  and  $CDE$ , intersect each other at  $D$ ; then will the sum of the opposite triangles,  $BDC$  and  $DAE$ , be equivalent to the lune whose angle is  $BDC$ ; and the sum of the opposite triangles,  $CDA$  and  $BDE$ , will be equivalent to the lune whose angle is  $CDA$ .



Produce the arcs,  $BDA$  and  $CDE$ , until they intersect on the opposite hemisphere at  $H$ ; then, since  $CDE$  and  $DEH$  are both semi-circumferences of a great circle, they are equal. Taking from each the common part  $DE$ , we have  $CD = HE$ . In the same way we prove  $BD = HA$ , and  $AE = BC$ . The two triangles,  $BDC$  and  $HAE$ , are therefore mutually equilateral, and hence they are equivalent, (Prop. 13). But the two triangles,  $HAE$  and  $ADE$ , together, make up the lune

$DEHAD$ ; hence the sum of the  $\triangle$ 's,  $BDC$  and  $ADE$ , is equivalent to the same lune.

By the same course of reasoning, we prove that the sum of the opposite  $\triangle$ 's,  $DAC$  and  $DBE$ , is equivalent to the lune  $DCHAD$ , whose angle is  $ADC$ .

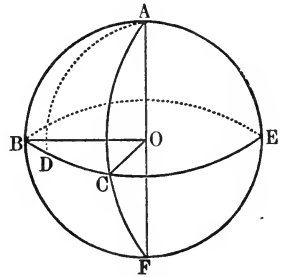
PROPOSITION XV.

*The surface of a lune is to the whole surface of the sphere, as the angle of the lune is to four right angles; or, as the arc which measures that angle is to the circumference of a great circle.*

Let  $ABFCA$  be a lune on the surface of a sphere, and  $BCE$  an arc of a great circle, whose poles are  $A$  and  $F$ , the vertices of the angles of the lune. The arc,  $BC$ , will then measure the angles of the lune. Take any arc, as  $BD$ , that will be contained an exact number of times in  $BC$ , and in the whole circumference,  $BCEB$ , and, beginning at  $B$ , divide the arc and the circumference into parts equal to  $BD$ , and join the points of division and the poles, by arcs of great circles. We shall thus divide the whole surface of the sphere into a number of equal lunes. Now, if the arc  $BC$  contains the arc  $BD$   $m$  times, and the whole circumference contains this arc  $n$  times, the surface of the lune will contain  $m$  of these partial lunes, and the surface of the sphere will contain  $n$  of the same; and we shall have,

$$\text{Surf. lune} : \text{surf. sphere} :: m : n.$$

But,  $m : n :: BC : \text{circumference great circle}$ ;  
 Hence,  $\text{surf. lune} : \text{surf. sphere} :: BC : \text{cir. great circle}$ ;  
 or,  $\text{surf. lune} : \text{surf. sphere} :: \angle BOC : 4 \text{ right angles}$ .





This demonstration assumes that  $BD$  is a common measure of the arc,  $BC$ , and the whole circumference. It may happen that no finite common measure can be found; but our reasoning would remain the same, even though this common measure were to become indefinitely small.

Hence the proposition.

*Cor. 1.* Any two lunes on the same sphere, or on equal spheres, are to each other as their respective angles.

SCHOLIUM.—Spherical triangles, formed by joining the pole of an arc of a great circle with the extremities of this arc by the arcs of great circles, are isosceles, and contain two right angles. For this reason they are called *bi-rectangular*. If the base is also a quadrant, the vertex of either angle becomes the pole of the opposite side, and each angle is measured by its opposite side. The three angles are then right angles, and the triangle is for this reason called *tri-rectangular*. It is evident that the surface of a sphere contains eight of its tri-rectangular triangles.

*Cor. 2.* Taking the right angle as the unit of angles, and denoting the angle of a lune by  $A$ , and the surface of a tri-rectangular triangle by  $T$ , we have,

$$\text{surf. of lune} : 8T :: A : 4;$$

whence,  $\text{surf. of lune} = 2A \times T$ .

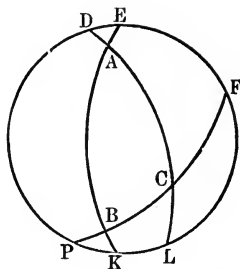
*Cor. 3.* A spherical ungula bears the same relation to the entire sphere, that the lune, which is the base of the ungula, bears to the surface of the sphere; and hence, any two spherical ungulas in the same sphere, or in equal spheres, are to each other as the angles of their respective lunes.

#### PROPOSITION XVI.

*The area of a spherical triangle is measured by the excess of the sum of its angles over two right angles, multiplied by the tri-rectangular triangle.*

Let  $ABC$  be a spherical triangle, and  $DEFLK$  the circumference of the base of the hemisphere on which this triangle is situated.

Produce the sides of the triangle until they meet this circumference in the points,  $D, E, F, L, K,$  and  $P,$  thus forming the sets of opposite triangles,  $DAE, AKL; BEF, BPK; CFL, CDP.$



Now, the triangles of each of these sets are together equal to a lune, whose angle is the corresponding angle of the triangle, (Prop. 14); hence we have,

$$\triangle DAE + \triangle AKL = 2A \times T, \text{ (Prop. 15, Cor. 2).}$$

$$\triangle BEF + \triangle BPK = 2B \times T.$$

$$\triangle CFL + \triangle CDP = 2C \times T.$$

If the first members of these equations be added, it is evident that their sum will exceed the surface of the hemisphere by twice the triangle  $ABC$ ; hence, adding these equations member to member, and substituting for the first member of the result its value,  $4T + 2\triangle ABC,$  we have

$$4T + 2\triangle ABC = 2A.T + 2B.T + 2C.T$$

$$\text{or, } 2T + \triangle ABC = A.T + B.T + C.T$$

$$\text{whence, } \triangle ABC = A.T + B.T + C.T - 2T.$$

$$\text{That is, } \triangle ABC = (A + B + C - 2) T.$$

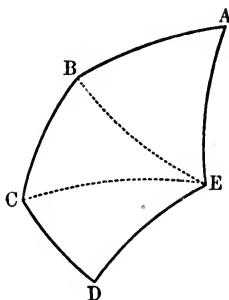
But  $A + B + C - 2$  is the excess of the sum of the angles of the triangle over two right angles, and  $T$  denotes the area of a tri-rectangular triangle.

Hence the proposition; *the area, etc.*

## PROPOSITION XVII.

*The area of any spherical polygon is measured by the excess of the sum of all its angles over two right angles, taken as many times, less two, as the polygon has sides, multiplied by the tri-rectangular triangle.*

Let  $ABCDE$  be a spherical polygon; then will its area be measured by the excess of the sum of the angles,  $A$ ,  $B$ ,  $C$ ,  $D$ , and  $E$ , over two right angles taken a number of times which is two less than the number of sides, multiplied by  $T$ , the tri-rectangular triangle. Through the vertex of any of the angles, as  $E$ , and the vertices of



the opposite angles, pass arcs of great circles, thus dividing the polygon into as many triangles, less two, as the polygon has sides. The sum of the angles of the several triangles will be equal to the sum of the angles of the polygon.

Now, the area of each triangle is measured by the excess of the sum of its angles over two right angles, multiplied by the tri-rectangular triangle. Hence the sum of the areas of all the triangles, or the area of the polygon, is measured by the excess of the sum of all the angles of the triangles over two right angles, taken as many times as there are triangles, multiplied by the tri-rectangular triangle. But there are as many triangles as the polygon has sides, less two.

Hence the proposition; *the area of any spherical polygon, etc.*

*Cor.* If  $S$  denote the sum of the angles of any spherical polygon,  $n$  the number of sides, and  $T$  the tri-rectangular triangle, the right angle being the unit of angles; the area of the polygon will be expressed by

$$[S - 2(n - 2)] \times T = (S - 2n + 4) T.$$

## SECTION II.

## SPHERICAL TRIGONOMETRY.

A Spherical Triangle contains six parts—three sides and three angles—any three of which being given, the other three may be determined.

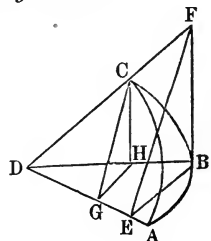
Spherical Trigonometry has for its object to explain the different methods of computing three of the six parts of a spherical triangle, when the other three are given. It may be divided into *Right-angled* Spherical Trigonometry, and *Oblique-angled* Spherical Trigonometry; the first treating of the solution of right-angled, and the second of oblique-angled spherical triangles.

## RIGHT-ANGLED SPHERICAL TRIGONOMETRY.

## PROPOSITION I.

*With the sines of the sides, and the tangent of ONE SIDE of any right-angled spherical triangle, two plane triangles can be formed that will be similar, and similarly situated.*

Let  $ABC$  be a spherical triangle, right-angled at  $B$ ; and let  $D$  be the center of the sphere. Because the angle  $CBA$  is a right angle, the plane  $CBD$  is perpendicular to the plane  $DBA$ . From  $C$  let fall  $CH$ , perpendicular to the plane  $DBA$ ; and as the



plane  $CBD$  is perpendicular to the plane  $DBA$ ,  $CH$  will lie in the plane  $CBD$ , and be perpendicular to the line  $DB$ , and perpendicular to all lines that can be drawn in the plane  $DBA$ , from the point  $H$  (Def. 2, B. VI).

Draw  $HG$  perpendicular to  $DA$ , and draw  $GC$ ;  $GC$  will lie wholly in the plane  $CDA$ , and  $CHG$  is a right-angled triangle, right-angled at  $H$ .

We will now demonstrate that the angle  $DGC$  is a right angle.

The right-angled  $\triangle CHG$ , gives  $CH^2 + HG^2 = CG^2$  (1)

The right-angled  $\triangle DGH$ , gives  $DG^2 + HG^2 = DH^2$  (2)

By subtraction,  $CH^2 - DG^2 = CG^2 - DH^2$  (3)

By transposition,  $CH^2 + DH^2 = CG^2 + DG^2$  (4)

But the first member of equation (4), is equal to  $CD^2$ , because  $CDH$  is a right-angled triangle;

Therefore,  $CD^2 = CG^2 + DG^2$

Hence,  $CD$  is the hypotenuse of the right-angled triangle  $DGC$ , (Th. 39, B. I).

From the point  $B$ , draw  $BE$  at right angles to  $DA$ , and  $BF$  at right angles to  $DB$ , in the plane  $CDB$  extended; the point  $F$  will be in the line  $DC$ . Draw  $EF$ , and as  $F$  is in the plane  $CDA$ , and  $E$  is in the same plane, the line  $EF$  is in the plane  $CDA$ . Now we are to prove that the triangle  $CHG$  is similar to the triangle  $BEF$ , and similarly situated.

As  $HG$  and  $BE$  are both at right angles to  $DA$ , they are parallel; and as  $HC$  and  $BF$  are both at right angles to  $DB$ , they are parallel; and by reason of the parallels, the angles  $GHC$  and  $EBF$  are equal; but  $GHC$  is a right angle; therefore,  $EBF$  is also a right angle.

Now, as  $GH$  and  $BE$  are parallel, and  $CH$  and  $BF$  are also parallel, we have,

$$DH : DB = HG : BE$$

And,  $DH : DB = HC : BF$

Therefore,  $HG : BE = HC : BF$  (Th. 6, B. II),

Or,  $HG : HC = BE : BF$ .

Here, then, are two triangles, having an angle in the one equal to an angle in the other, and the sides about the equal angles proportional; the two triangles are therefore equiangular, (Cor. 2, Th. 17, B. II); and they are similarly situated, for their sides make equal angles at  $H$  and  $B$  with the same line,  $DB$ .

Hence the proposition.

SCHOLIUM.—By the definition of sines, cosines, and tangents, we perceive that  $CH$  is the sine of the arc  $BC$ ,  $DH$  is its cosine, and  $BF$  its tangent;  $CG$  is the sine of the arc  $AC$ , and  $DG$  its cosine. Also,  $BE$  is the sine of the arc  $AB$ , and  $DE$  is the cosine of the same arc. With this figure we are prepared to demonstrate the following propositions.

#### PROPOSITION II.

*In any right-angled spherical triangle, the sine of one side is to the tangent of the other side, as radius is to the tangent of the angle adjacent to the first-mentioned side.*

*Or, the sine of one side is to the tangent of the other side, as the cotangent of the angle adjacent to the first-mentioned side is to the radius.*

For the sake of brevity, we will represent the angles of the triangle by  $A, B, C$ , and the sides or arcs opposite to these angles, by  $a, b, c$ , that is,  $a$  opposite  $A$ , etc.

In the right-angled plane triangle  $EBF$ , we have,

$$EB : BF = R : \tan.BEF$$

That is,  $\sin.c : \tan.a = R : \tan.A$ ,

which agrees with the first part of the enunciation. By reference to equation (5), Section I, Plane Trigonometry, we shall find that,

$$\tan.A \cot.A = R^2;$$

therefore, 
$$\tan.A = \frac{R^2}{\cot.A}$$

Substituting this value for tangent  $A$ , in the preceding proportion, and dividing the last couplet by  $R$ , we shall have,

$$\sin.c : \tan.a = 1 : \frac{R}{\cot.A}.$$

Or,  $\sin.c : \tan.a = \cot.A : R.$

Or,  $R \sin.c = \tan.a \cot.A,$  (1)

which answers to the second part of the enunciation.

*Cor.* By changing the construction, drawing the tangent to  $AB$ , in place of the tangent to  $BC$ , and proceeding in a similar manner, we have,

$$R \sin.a = \tan.c \cot.C. \quad (2)$$

### PROPOSITION III.

*In any right-angled spherical triangle, the sine of the right angle is to the sine of the hypotenuse, as the sine of either of the other angles is to the sine of the side opposite to that angle.*

The sine of  $90^\circ$ , or radius, is designated by  $R$ .

In the plane triangle,  $CHG$ , we have,

$$\sin.CHG : CG = \sin.CGH : CH$$

That is,  $R : \sin.b = \sin.A : \sin.a$

Or,  $R \sin.a = \sin.b \sin.A$  (3)

*Cor.* By a change in the construction of the figure, drawing a tangent to  $AB$ , etc., we shall have,

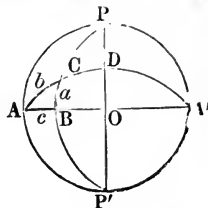
$$R : \sin.b = \sin.C : \sin.c$$

Or,  $R \sin.c = \sin.b \sin.C.$  (4)

**SCHOLIUM.** — Collecting the four equations taken from this and the preceding proposition, we have,

$$\left. \begin{array}{l} (1) \ R \sin.c = \tan.a \cot.A \\ (2) \ R \sin.a = \tan.c \cot.C \\ (3) \ R \sin.a = \sin.b \sin.A \\ (4) \ R \sin.c = \sin.b \sin.C \end{array} \right\}$$

These equations refer to the right-angled triangle,  $ABC$ ; but the principles are true for any right-angled spherical triangle. Let us apply them to the right-angled triangle,  $PDC$ , the complementary triangle to  $ABC$ .



Making this application, equation

$$\begin{aligned} (1) & \text{ becomes } R \sin.CD = \tan.PD \cot.C & (n) \\ (2) & \text{ becomes } R \sin.PD = \tan.CD \cot.P & (m) \\ (3) & \text{ becomes } R \sin.PD = \sin.PC \sin.C & (o) \\ (4) & \text{ becomes } R \sin.CD = \sin.PC \sin.P & (p) \end{aligned}$$

By observing that  $\sin.CD = \cos.AC = \cos.b$ .

And that  $\tan.PD = \cot. \angle C = \cot.A$ , etc.; and by running equations  $(n)$ ,  $(m)$ ,  $(o)$ , and  $(p)$ , back into the triangle,  $ABC$ , we shall have,

$$\left. \begin{aligned} (5) \quad R \cos.b &= \cot.A \cot.C \\ (6) \quad R \cos.A &= \cot.b \tan.c \\ (7) \quad R \cos.A &= \cos.a \sin.C \\ (8) \quad R \cos.b &= \cos.a \cos.c \end{aligned} \right\}$$

By observing equation  $(6)$ , we find that the second member refers to sides adjacent to the angle  $A$ . The same relation holds in respect to the angle  $C$ , and gives,

$$(9) \quad R \cos.C = \cot.b \tan.a.$$

Making the same observations on  $(7)$ , we infer,

$$(10) \quad R \cos.C = \cos.c \sin.A.$$

**OBSERVATION 1.** Several of these equations can be deduced geometrically without the least difficulty. For example, take the figure to Proposition 1. The parallels in the plane,  $DBA$ , give,

$$DB : DH = DE : DG.$$

That is,  $R : \cos.a = \cos.c : \cos.b$ .

A result identical with equation  $(8)$ , and in words it is expressed thus: *Radius is to cosine of one side, as the cosine of the other side is to the cosine of the hypotenuse.*

**OBSERVATION 2.** The equations numbered from  $(1)$  to  $(10)$  cover every possible case that can occur in right-angled spherical trigonometry; but the combinations are



too various to be remembered, and readily applied to practical use.

We can remedy this inconvenience, by taking the *complement* of the hypotenuse, and the *complements* of the two oblique angles, in place of the arcs themselves.

Thus,  $b$  is the hypotenuse, and let  $b'$  be its complement.

Then,  $b + b' = 90^\circ$ ; or,  $b = 90^\circ - b'$ ; and,  $\sin.b = \cos.b'$ ,  $\cos.b = \sin.b'$ ;  $\tan.b = \cot.b'$ . In the same manner, if  $A'$  is the complement to  $A$ ,

Then,  $\sin.A = \cos.A'$ ;  $\cos.A = \sin.A'$ ; and,  $\tan.A = \cot.A'$ ; and similarly,  $\sin.C = \cos.C'$ ;  $\cos.C = \sin.C'$ ; and  $\tan.C = \cot.C'$ .

Substituting these values for  $b$ ,  $A$ , and  $C$ , in the foregoing *ten* equations ( $a$  and  $c$  remaining the same), we have,

#### NAPIER'S CIRCULAR PARTS.

$$(11) R \sin.c = \tan.a \tan.A'$$

$$(12) R \sin.a = \tan.c \tan.C'$$

$$(13) R \sin.a = \cos.b' \cos.A'$$

$$(14) R \sin.c = \cos.b' \cos.C'$$

$$(15) R \sin.b' = \tan.A' \tan.C'$$

$$(16) R \sin.A' = \tan.b' \tan.c$$

$$(17) R \sin.A' = \cos.a \cos.C'$$

$$(18) R \sin.b' = \cos.a \cos.c$$

$$(19) R \sin.C' = \tan.b' \tan.a$$

$$(20) R \sin.C' = \cos.c \cos.A'$$

Omitting the consideration of the right angle, there are five parts. Each part taken as a middle part, is connected to its adjacent parts by one equation, and to its extreme parts by another equation; therefore, ten equations are required for the combinations of all the parts.

These equations are very remarkable, because the first members are all composed of radius into *some sine*, and the second members are all composed of the product of *two tangents*, or *two cosines*.

To condense these equations into words, for the purpose of assisting the memory, we will refer any one of them directly to the right-angled triangle,  $ABC$ , in the last figure.

When the right angle is left out of the question, a right-angled triangle consists of *five* parts — *three* sides, and *two* angles. Let any one of these parts be called a *middle part*; then two other parts will lie adjacent to this part, and two *opposite to it*, that is, separated from it by two other parts.

For instance, take equation (11), and call  $c$  the *middle part*; then  $A'$  and  $a$  will be adjacent parts, and  $C'$  and  $b'$  opposite parts. Again, take  $a$  as a *middle part*; then  $c$  and  $C'$  will be adjacent parts, and  $A'$  and  $b'$  will be opposite parts; and thus we may go round the triangle.

Take any equation from (11) to (20), and consider the middle part in the first member of the equation, and we shall find that it corresponds to one of the following *invariable and comprehensive rules*:

1. *The radius into the sine of the middle part is equal to the product of the tangents of the adjacent parts.*
2. *The radius into the sine of the middle part is equal to the product of the cosines of the opposite parts.*

These rules are known as Napier's Rules, because they were first given by that distinguished mathematician, who was also the inventor of logarithms.

In the application of these equations, the *accent* may be omitted if  $\tan.$  be changed to  $\cotan.$ ,  $\sin.$  to  $\cosin.$ , etc. Thus, if equation (13) were to be employed, it would be written, in the first instance,  $R \sin.a = \cos.b' \cos.A'$ , to insure conformity to the rule; then, we would change it into  $R \sin.a = \sin.b \sin.A$ .

REMARK.—We caution the pupil to be very particular to take the *complements* of the hypotenuse, and the complements of the oblique angles.

## SECTION III.

## OBLIQUE-ANGLED SPHERICAL TRIGONOMETRY.

THE preceding investigations have had reference to right-angled spherical trigonometry only, but the application of these principles covers oblique-angled trigonometry also; for, every oblique-angled spherical triangle may be considered as made up of the sum or difference of two right-angled spherical triangles. With this explanatory remark, we give

## PROPOSITION I.

*In all spherical triangles, the sines of the sides are to each other, as the sines of the angles opposite to them.*

This was proved in relation to right-angled triangles in Prop. 3, Sec. II, and we now apply the principle to oblique-angled triangles.

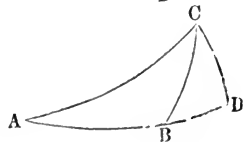
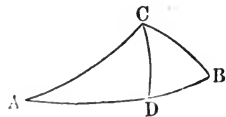
Let  $ABC$  be the triangle, and let  $CD$  be perpendicular to  $AB$ , or to  $AB$  produced.

Then, by Prop. 3, Sec. II, we have,

$$R : \sin. AC = \sin. A : \sin. CD.$$

Also,

$$\sin. CB : R = \sin. CD : \sin. B.$$



By multiplying these two proportions together, term by term, and omitting the common factor  $R$ , in the first couplet, and the common factor,  $\sin.CD$ , in the second, we have

$$\sin.CB : \sin.AC = \sin.A : \sin.B.$$

### PROPOSITION II.

*In any spherical triangle, if an arc of a great circle be let fall from any angle perpendicular to the opposite side as a base, or to the base produced, the cosines of the other two sides will be to each other as the cosines of the segments of the base.*

By the application of equation 8, (Sec. II), to the last figure, we have,

$$R \cos.AC = \cos.AD \cos.DC$$

Similarly,  $R \cos.BC = \cos.DC \cos.BD$

Dividing one of these equations by the other, omitting common factors in numerators and denominators, we have,

$$\frac{\cos.AC}{\cos.BC} = \frac{\cos.AD}{\cos.BD}$$

Or,  $\cos.AC : \cos.BC = \cos.AD : \cos.BD.$

### PROPOSITION III.

*If from any angle of a spherical triangle, a perpendicular be let fall on the base, or on the base produced, the tangents of the segments of the base will be reciprocally proportional to the cotangents of the segments of the angle.*

By the application of Equation 2, (Sec. II), to the last figure, we have,

$$R \sin.CD = \tan.AD \cot.ACD.$$

Similarly,  $R \sin.CD = \tan.BD \cot.BCD$

Therefore, by equality,

$$\tan.AD \cot.ACD = \tan.BD \cot.BCD$$

Or,  $\tan.AD : \tan.BD = \cot.BCD : \cot.ACD.$

## PROPOSITION IV.

*The same construction remaining, the cosines of the angles at the extremities of the segments of the base are to each other as the sines of the segments of the opposite angle.*

Equation 7, (Sec. II), applied to the triangle  $ACD$ , gives

$$R \cos.A = \cos.CD \sin.ACD \quad (s)$$

Also,  $R \cos.B = \cos.CD \sin.BCD \quad (t)$

Dividing equation  $(s)$  by  $(t)$ , gives

$$\frac{\cos.A}{\cos.B} = \frac{\sin.ACD}{\sin.BCD}$$

Or,  $\cos.B : \cos.A = \sin.BCD : \sin.ACD.$

## PROPOSITION V.

*The same construction remaining, the sines of the segments of the base are to each other as the cotangents of the adjacent angles.*

Equation 1, (Sec. II), applied to the triangle  $ACD$ , gives

$$R \sin.AD = \tan.CD \cot.A \quad (s)$$

Similarly,  $R \sin.BD = \tan.CD \cot.B \quad (t)$

Dividing  $(s)$  by  $(t)$ , gives

$$\frac{\sin.AD}{\sin.BD} = \frac{\cot.A}{\cot.B}$$

Or,  $\sin.BD : \sin.AD = \cot.B : \cot.A$

## PROPOSITION VI.

The same construction remaining, the cotangents of the two sides are to each other as the cosines of the segments of the angle.

Equation 9, (Sec. II), applied to the triangle  $ACD$ , gives

$$R \cos.ACD = \cot.AC \tan.CD \quad (s)$$

Similarly,  $R \cos.BCD = \cot.BC \tan.CD \quad (t)$

Dividing  $(s)$  by  $(t)$ , gives

$$\frac{\cos.ACD}{\cos.BCD} = \frac{\cot.AC}{\cot.BC}$$

Or,  $\cot.AC : \cot.BC = \cos.ACD : \cos.BCD.$

## PROPOSITION VII.

The cosine of any side of a spherical triangle, is equal to the product of the cosines of the other two sides, plus the product of the sines of those sides multiplied by the cosine of the included angle.

Let  $ABC$  be a spherical triangle, and  $CD$  a perpendicular from the angle  $C$  to the side  $AB$ , or to the side  $AB$  produced. Then, by Prop. 2,

$$\cos.AC : \cos.CB = \cos.AD : \cos.BD \quad (1)$$

When  $CD$  falls within the triangle,

$$BD = (AB - AD);$$

and when  $CD$  falls without the triangle,

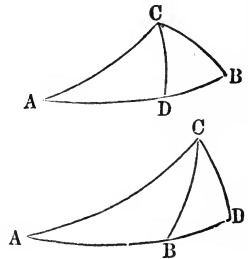
$$BD = (AD - AB).$$

Hence,  $\cos.BD = \cos.(AD - AB)$

Now,  $\cos.(AB - AD) = \cos.(AD - AB),$

because each of them is equal to

$\cos.AB \cos.AD + \sin.AB \sin.AD,$  (Eq. 10, Prop. 2, Sec. I, Plane Trig.).



This value of  $\cos. BD$ , put in proportion (1), gives

$$\cos AC : \cos. CB = \cos. AD : \cos. AB \cos. AD + \sin. AB \sin. AD \quad (2)$$

Dividing the last couplet of proportion (2) by  $\cos. AD$ , observing that

$$\frac{\sin. AD}{\cos. AD} = \tan. AD,$$

and we have

$$\cos. AC : \cos. CB = 1 : \cos. AB + \sin. AB \tan. AD \quad (3)$$

By applying equation 6, (Sec. II), to the triangle  $ACD$ , taking the radius as unity, we have

$$\cos. A = \cot. AC \tan. AD \quad (k)$$

But,  $\tan. AC \cot. AC = 1$ , (Eq. 5, Sec. I, Plane Trig.) (l)

Multiplying equation (k) by  $\tan. AC$ , observing equation (l), and we have

$$\tan. AC \cos. A = \tan. AD$$

Substituting this value of  $\tan. AD$ , in proportion (3), we have

$$\cos. AC : \cos. CB = 1 : \cos. AB + \sin. AB \tan. AC \cos. A \quad (4)$$

Multiplying extremes and means, gives

$$\cos. CB = \cos. AC \cos. AB + \sin. AB (\cos. AC \tan. AC) \cos. A.$$

But,  $\tan. AC = \frac{\sin. AC}{\cos. AC}$ , or,  $\cos. AC \tan. AC = \sin. AC$ .

Therefore,  $\cos. CB = \cos. AC \cos. AB + \sin. AB \sin. AC \cos. A$ .

If the sides opposite the angles,  $A$ ,  $B$ , and  $C$ , be respectively represented by  $a$ ,  $b$ , and  $c$ , this equation becomes,

$$\cos. a = \cos. b \cos. c + \sin. b \sin. c \cos. A.$$

This formula conforms to the enunciation in respect to the side  $a$ . Now, by interchanging  $b$  and  $a$ , and  $B$  and  $A$ , in the last equation, we get the formula for  $\cos. b$ , which is,

$$\cos. b = \cos. a \cos. c + \sin. a \sin. c \cos. B.$$

Interchanging  $c$  and  $a$ , and  $C$  and  $A$ , we get the formula for  $\cos.c$ , which is,

$$\cos.c = \cos.a \cos.b + \sin.a \sin.b \cos.C.$$

Hence, we have the three symmetrical formulæ:

$$\left. \begin{aligned} \cos.a &= \cos.b \cos.c + \sin.b \sin.c \cos.A \\ \cos.b &= \cos.a \cos.c + \sin.a \sin.c \cos.B \\ \cos.c &= \cos.a \cos.b + \sin.a \sin.b \cos.C \end{aligned} \right\} (S)$$

From these, by simple transposition and division, we deduce the following formulæ for the cosines of the angles of any spherical triangle, viz:

$$\left. \begin{aligned} \cos.A &= \frac{\cos.a - \cos.b \cos.c}{\sin.b \sin.c} \\ \cos.B &= \frac{\cos.b - \cos.a \cos.c}{\sin.a \sin.c} \\ \cos.C &= \frac{\cos.c - \cos.a \cos.b}{\sin.a \sin.b} \end{aligned} \right\} (S')$$

By means of these equations we can find the cosine of any of the three angles of a spherical triangle in terms of the functions of the sides; but in their present form they are not suited for the employment of logarithms, and we should be compelled to use a table of natural sines and cosines, and to perform tedious numerical operations, to obtain the value of the angle.

They are, however, by the following process, transformed into others well adapted to the use of logarithms.

In Eq. 34, Sec. I, Plane Trig., we have

$$1 + \cos.A = 2\cos.^2 \frac{1}{2}A.$$

$$\begin{aligned} \text{Therefore, } 2\cos.^2 \frac{1}{2}A &= 1 + \frac{\cos.a - \cos.b \cos.c}{\sin.b \sin.c} \\ &= \frac{(\sin.b \sin.c - \cos.b \cos.c) + \cos.a}{\sin.b \sin.c} \quad (m). \end{aligned}$$

But,  $\cos.(b + c) = \cos.b \cos.c - \sin.c \sin.b$ , (Equation 9. Section I, Plane Trig.). By comparing this equation



with the second member of equation ( $m$ ), we perceive that equation ( $m$ ) is readily reduced to

$$2\cos.^2 \frac{1}{2}A = \frac{\cos.a - \cos.(b+c)}{\sin.b \sin.c}.$$

Considering  $(b+c)$  as one arc, and then making application of equation (18), Plane Trigonometry, we have,

$$2\cos.^2 \frac{1}{2}A = \frac{2\sin.\left(\frac{a+b+c}{2}\right) \sin.\left(\frac{b+c-a}{2}\right)}{\sin.b \sin.c}.$$

But,  $\frac{b+c-a}{2} = \frac{b+c+a}{2} - a$ ; and if we put  $S$  to represent  $\frac{b+c+a}{2}$ , we shall have,

$$\cos.^2 \frac{A}{2} = \frac{\sin.S \sin.(S-a)}{\sin.b \sin.c}.$$

Or, 
$$\cos. \frac{A}{2} = \sqrt{\frac{\sin.S \sin.(S-a)}{\sin.b \sin.c}}.$$

The second member of this equation gives the value of the cosine when the radius is unity. To a greater radius, the cosine would be greater; and in just the same proportion as the radius increases, all the trigonometrical lines increase; therefore, to adapt the above equation to our tables where the radius is  $R$ , we must write  $R$  in the second member, as a factor; and if we put it under the radical sign, we must write  $R^2$ .

For the other angles we shall have precisely similar equations:

$$\left. \begin{aligned} \text{That is, } \cos. \frac{A}{2} &= \sqrt{\frac{R^2 \sin.S \sin.(S-a)}{\sin.b \sin.c}} \\ \cos. \frac{B}{2} &= \sqrt{\frac{R^2 \sin.S \sin.(S-b)}{\sin.a \sin.c}} \\ \cos. \frac{C}{2} &= \sqrt{\frac{R^2 \sin.S \sin.(S-c)}{\sin.a \sin.b}} \end{aligned} \right\} (T)$$

To deduce from formulæ ( $S$ ), formulæ for the sines of the half of each of the angles of a spherical triangle, we proceed as follows:

From Eq. 35, Sec. I, Plane Trig., we have

$$2\sin.^2 \frac{1}{2}A = 1 - \cos.A.$$

Substituting the value of  $\cos.A$ , taken from formulæ ( $S$ ), and we have,

$$\begin{aligned} 2\sin.^2 \frac{1}{2}A &= 1 - \frac{\cos.a - \cos.b \cos.c}{\sin.b \sin.c} \\ &= \frac{(\sin.b \sin.c + \cos.b \cos.c) - \cos^2 a}{\sin.b \sin.c}. \quad (o) \end{aligned}$$

But,  $\cos.(b \oslash c) = \sin.b \sin.c + \cos.b \cos.c$ , (Eq. 10, Sec. I, Plane Trig.).

This equation reduces equation ( $o$ ) to

$$2\sin.^2 \frac{1}{2}A = \frac{\cos.(b \oslash c) - \cos.a}{\sin.b \sin.c}.$$

Considering  $(b \oslash c)$  as a single arc, and applying equation 18, Sec. I, Plane Trig., we have

$$2\sin.^2 \frac{1}{2}A = \frac{2\sin.\left(\frac{a+b-c}{2}\right) \sin.\left(\frac{a+c-b}{2}\right)}{\sin.b \sin.c}. \quad (o')$$

But,  $\frac{a+b-c}{2} = \frac{a+b+c}{2} - c = S - c$ , if we put  $S = \frac{a+b+c}{2}$ .

Also,  $\frac{a+c-b}{2} = \frac{a+b+c}{2} - b = S - b$ .

Dividing equation ( $o'$ ) by 2, and making these substitutions, we have

$$\sin.^2 \frac{1}{2}A = \frac{\sin.(S - c) \sin.(S - b)}{\sin.b \sin.c},$$

when radius is unity.

When radius is  $R$ , we have

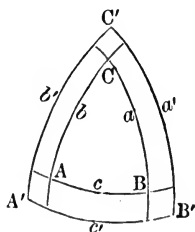
$$\left. \begin{aligned} \sin. \frac{1}{2}A &= \sqrt{\frac{R^2 \sin.(S-c) \sin.(S-b)}{\sin.b \sin.c}} \\ \text{Similarly, } \sin. \frac{1}{2}B &= \sqrt{\frac{R^2 \sin.(S-a) \sin.(S-c)}{\sin.a \sin.c}} \\ \text{And, } \sin. \frac{1}{2}C &= \sqrt{\frac{R^2 \sin.(S-a) \sin.(S-b)}{\sin.a \sin.b}} \end{aligned} \right\} (U)$$

The above equations are now adapted to our tables. We shall show the application of these formulæ, and those in group (T), hereafter.

### PROPOSITION VIII.

*The cosine of any of the angles of a spherical triangle, is equal to the product of the sines of the other two angles multiplied by the cosine of the included side, minus the product of the cosines of these other two angles.*

Let  $ABC$  be a spherical triangle, and  $A'B'C'$  its supplemental or polar triangle, the angles of the first being denoted by  $A, B,$  and  $C$ , and the sides opposite these angles by  $a, b, c$ , respectively;  $A', B', C', a', b', c'$ , denoting the angles and corresponding sides of the second.



By Prop. 6, Sec. I, we have the following relations between the sides and angles of these two triangles.

$$A' = 180^\circ - a, \quad B' = 180^\circ - b, \quad C' = 180^\circ - c;$$

$$a' = 180^\circ - A, \quad b' = 180^\circ - B, \quad c' = 180^\circ - C.$$

The first of formulæ (S), Prop. 7, when applied to the polar triangle, gives

$$\cos a' = \cos b' \cos c' + \sin b' \sin c' \cos A' \quad (1)$$

which, by substituting the values of  $a'$ ,  $b'$ ,  $c'$ , and  $A'$ , becomes

$$\cos.(180^\circ - A) = \cos.(180^\circ - B) \cos.(180^\circ - C) + \sin.(180^\circ - B) \sin.(180^\circ - C) \cos.(180^\circ - a), \quad (2)$$

But,

$\cos.(180^\circ - A) = -\cos.A$ , etc.,  $\sin.(180^\circ - B) = \sin.B$ , etc.; and placing these values for their equals in eq. (2), and changing the signs of both members of the resulting equation, we get

$$\cos.A = \sin.B \sin.C \cos.a - \cos.B \cos.C,$$

which agrees with the enunciation.

By treating the other two of formulæ (S), Prop. 7, in the same manner, we should obtain similar values for the cosines of the other two angles of the triangle  $ABC$ ; or we may get them more easily by a simple permutation of the letters  $A$ ,  $B$ ,  $C$ ,  $a$ , etc.

Hence, we have the three equations

$$\left. \begin{aligned} \cos.A &= \sin.B \sin.C \cos.a - \cos.B \cos.C \\ \cos.B &= \sin.A \sin.C \cos.b - \cos.A \cos.C \\ \cos.C &= \sin.A \sin.B \cos.c - \cos.A \cos.B \end{aligned} \right\} \quad (V)$$

By transposition and division, these equations become

$$\cos.a = \frac{\cos.A + \cos.B \cos.C}{\sin.B \sin.C} \quad (3)$$

$$\cos.b = \frac{\cos.B + \cos.A \cos.C}{\sin.A \sin.C}$$

$$\cos.c = \frac{\cos.C + \cos.A \cos.B}{\sin.A \sin.B}$$

From these we can find formulæ to express the sine or the cosine of one half of the side of a spherical triangle, in terms of the functions of its angles; thus:

Add 1 to each member of eq. (3), and we have

$$1 + \cos.a = \frac{\cos.A + \cos.B \cos.C + \sin.B \sin.C}{\sin.B \sin.C}$$

$$= \frac{\cos.A + \cos.(B - C)}{\sin.B \sin.C}$$

But,  $1 + \cos.a = 2\cos.^2 \frac{1}{2}a$ ; hence,

$$2\cos.^2 \frac{1}{2}a = \frac{\cos.A + \cos.(B - C)}{\sin.B \sin.C}$$

and since  $\cos.A + \cos.(B - C) = 2\cos.\frac{1}{2}(A + B - C)\cos.\frac{1}{2}(A + C - B)$  (Eq. 17, Sec. I, Plane Trig.), we have

$$2\cos.^2 \frac{1}{2}a = \frac{2\cos.\frac{1}{2}(A + B - C)\cos.\frac{1}{2}(A + C - B)}{\sin.B \sin.C}$$

Make  $A + B + C = 2S$ ; then  $A + B - C = 2S - 2C$ ,  $A + C - B = 2S - 2B$ ,  $\frac{1}{2}(A + B - C) = S - C$ , and  $\frac{1}{2}(A + C - B) = S - B$ ; whence

$$2\cos.^2 \frac{1}{2}a = \frac{2\cos.(S - C)\cos.(S - B)}{\sin.B \sin.C}$$

$$\left. \begin{array}{l} \text{or,} \quad \cos.\frac{1}{2}a = \sqrt{\frac{\cos.(S - C)\cos.(S - B)}{\sin.B \sin.C}} \\ \text{Similarly, } \cos.\frac{1}{2}b = \sqrt{\frac{\cos.(S - A)\cos.(S - C)}{\sin.A \sin.C}} \\ \text{and,} \quad \cos.\frac{1}{2}c = \sqrt{\frac{\cos.(S - A)\cos.(S - B)}{\sin.A \sin.B}} \end{array} \right\} (V')$$

To find the  $\sin.\frac{1}{2}a$  in terms of the functions of the angles, we must subtract each member of eq. (3) from 1, by which we get

$$1 - \cos.a = 1 - \frac{\cos.A + \cos.B \cos.C}{\sin.B \sin.C}$$

But,  $1 - \cos.a = 2\sin.^2 \frac{1}{2}a$ ; hence we have,

$$2\sin.^2 \frac{1}{2}a = \frac{(\sin.B \sin.C - \cos.B \cos.C) - \cos.A}{\sin.B \sin.C}$$

Operating upon this in a manner analogous to that by which  $\cos.\frac{1}{2}a$  was found, we get,

$$\left. \begin{aligned} \sin.\frac{1}{2}a &= \left\{ \frac{-\cos.S \cos.(S-A)}{\sin.B \sin.C} \right\}^{\frac{1}{2}} \\ \sin.\frac{1}{2}b &= \left\{ \frac{-\cos.S \cos.(S-B)}{\sin.A \sin.C} \right\}^{\frac{1}{2}} \\ \sin.\frac{1}{2}c &= \left\{ \frac{-\cos.S \cos.(S-C)}{\sin.A \sin.B} \right\}^{\frac{1}{2}} \end{aligned} \right\} (W)$$

If the first equation in (W) be divided by the first in (V'), we shall have,

$$\tan.\frac{1}{2}a = \left\{ \frac{-\cos.S \cos.(S-A)}{\cos.(S-B) \cos.(S-C)} \right\}^{\frac{1}{2}}$$

And corresponding expressions may be obtained for  $\tan.\frac{1}{2}b$  and  $\tan.\frac{1}{2}c$ .

#### NAPIER'S ANALOGIES.

If the value of  $\cos.c$ , expressed in the third equation of group (S), Prop. 7, be substituted for  $\cos.c$ , in the second member of the first equation of the same group, we have,

$$\cos.a = \cos.a \cos.^2b + \sin.a \sin.b \cos.b \cos.C + \sin.b \sin.c \cos.A;$$

which, by writing for  $\cos.^2b$  its equal,  $1 - \sin.^2b$ , becomes,

$$\cos.a = \cos.a - \cos.a \sin.^2b + \sin.a \sin.b \cos.b \cos.C + \sin.b \sin.c \cos.A.$$

$$\text{Or, } 0 = -\cos.a \sin.^2b + \sin.a \sin.b \cos.b \cos.C + \sin.b \sin.c \cos.A.$$

Dividing through by  $\sin.b$ , and transposing, we find,

$$\cos.A \sin.c = \cos.a \sin.b - \sin.a \cos.b \cos.C;$$

$$\text{Hence, } \cos.A = \frac{\cos.a \sin.b - \sin.a \cos.b \cos.C}{\sin.c}. \quad (1)$$

By substituting the value of  $\cos.c$ , in the second of the equations of group (S), Prop. 7; or, merely writing  $B$  for  $A$ , and interchanging  $b$  and  $a$ , in the above value, for  $\cos.A$ , we obtain,

$$\cos.B = \frac{\cos.b \sin.a - \sin.b \cos.a \cos.C}{\sin.c} \quad (2)$$

Adding equations (1) and (2), member to member, we have,

$$\cos.A + \cos.B = \frac{\sin.(a+b) - \sin.(a+b) \cos.C}{\sin.c};$$

by remembering that  $\sin.a \cos.b + \cos.a \sin.b = \sin.(a+b)$ .  
(See Eq. (7), Sec. I, Plane Trig.).

$$\text{Whence, } \cos.A + \cos.B = (1 - \cos.C) \frac{\sin.(a+b)}{\sin.c}. \quad (3)$$

In any spherical triangle we have, (Prop. I),

$$\sin.A : \sin.B :: \sin.a : \sin.b;$$

And therefore,  $\sin.A + \sin.B : \sin.B :: \sin.a + \sin.b : \sin.b$ .

$$\text{Hence, } \sin.A + \sin.B = \frac{(\sin.a + \sin.b) \sin.B}{\sin.b}.$$

But,  $\frac{\sin.B}{\sin.b} = \frac{\sin.C}{\sin.c}$ , which value of  $\frac{\sin.B}{\sin.b}$ , in the above equation, gives

$$\sin.A + \sin.B = \frac{(\sin.a + \sin.b) \sin.C}{\sin.c}. \quad (4)$$

Dividing equation (4) by equation (3), member by member, we obtain,

$$\frac{\sin.A + \sin.B}{\cos.A + \cos.B} = \frac{\sin.C}{1 - \cos.C} \times \frac{\sin.a + \sin.b}{\sin.(a+b)}. \quad (5)$$

Comparing this equation with Equations (20) and (26), Sec. I, Plane Trigonometry, we see that it can be reduced to

$$\tan.\frac{1}{2}(A+B) = \cot.\frac{1}{2}C \times \frac{\sin.a + \sin.b}{\sin.(a+b)} \quad (6)$$

Again, from the proportion,

$$\sin.A : \sin.B :: \sin.a : \sin.b,$$

we likewise have,

$$\sin.A - \sin.B : \sin.B :: \sin.a - \sin.b : \sin.b;$$

hence,  $\sin.A - \sin.B = (\sin.a - \sin.b) \frac{\sin.B}{\sin.b} = (\sin.a - \sin.b) \frac{\sin.C}{\sin.c}$ .

Dividing this equation by equation (3), member by member, we obtain,

$$\frac{\sin.A - \sin.B}{\cos.A + \cos.B} = \frac{\sin.C}{1 - \cos.C} \times \frac{\sin.a - \sin.b}{\sin.(a + b)}.$$

Comparing this with Equations (22) and (26), Sec. I, Plane Trigonometry, we see that it will reduce to

$$\tan.\frac{1}{2}(A - B) = \cot.\frac{1}{2}C \times \frac{\sin.a - \sin.b}{\sin.(a + b)}. \quad (7)$$

Now,  $\sin.a + \sin.b = 2\sin.\left(\frac{a+b}{2}\right) \cos.\left(\frac{a-b}{2}\right)$ ; Eq. (15), Sec. I, Plane Trig.).

and,  $\sin.(a + b) = 2\sin.\left(\frac{a+b}{2}\right) \cos.\left(\frac{a+b}{2}\right)$ ; Eq. (30), Sec. I, Plane Trig.).

Dividing the first of these by the second, we have

$$\frac{\sin.a + \sin.b}{\sin.(a + b)} = \frac{\cos.\left(\frac{a-b}{2}\right)}{\cos.\left(\frac{a+b}{2}\right)}$$

Writing the second member of this equation for its first member in Eq (6), that equation becomes

$$\tan.\frac{1}{2}(A + B) = \cot.\frac{1}{2}C \frac{\cos.\frac{1}{2}(a-b)}{\cos.\frac{1}{2}(a+b)}. \quad (8)$$

By a similar operation, Eq. (7) may be reduced to

$$\tan.\frac{1}{2}(A - B) = \cot.\frac{1}{2}C \frac{\sin.\frac{1}{2}(a-b)}{\sin.\frac{1}{2}(a+b)}. \quad (9)$$

Equations (8) and (9) may be resolved into the proportions

$$\begin{aligned} \cos.\frac{1}{2}(a + b) : \cos.\frac{1}{2}(a - b) &:: \cot.\frac{1}{2}C : \tan.\frac{1}{2}(A + B); \\ \sin.\frac{1}{2}(a + b) : \sin.\frac{1}{2}(a - b) &:: \cot.\frac{1}{2}C : \tan.\frac{1}{2}(A - B). \end{aligned}$$

These proportions are known as Napier's 1st and 2d



Analogies, and may be advantageously used in the solution of spherical triangles, when *two sides and the included angle are given*.

When expressed in language, these proportions furnish the following rules:

1. *The cosine of the half sum of any two sides of a spherical triangle is to the cosine of the half difference of the same sides, as the cotangent of half the included angle is to the tangent of the half sum of the other two angles.*

2. *The sine of the half sum of any two sides of a spherical triangle is to the sine of the half difference of the same sides, as the cotangent of half the included angle is to the tangent of the half difference of the other two angles.*

The half sum, and the half difference of two angles of a spherical triangle, may be found by these rules, when two sides and the included angle are given; and by adding the half sum to the half difference, we get the greater of these two angles, and by subtracting the half difference from the half sum, we get the smaller. The third side may then be found by proportion.

We have analogous proportions applicable to the case in which two angles and the included side of a spherical triangle are given.

To deduce these, let us represent the angles of the triangle by  $A, B,$  and  $C,$  and the opposite sides by  $a, b,$  and  $c;$   $A', B', C', a', b', c',$  denoting the corresponding angles and sides of the polar triangle.

Now, Eq. (9) is applicable to any spherical triangle, and when applied to the polar triangle, it becomes

$$\tan. \frac{1}{2}(A' - B') = \cot. \frac{1}{2}C' \frac{\sin. \frac{1}{2}(a' - b')}{\sin. \frac{1}{2}(a' + b')}. \quad (n)$$

But by Prop. 6, Sec. I, Spherical Geometry, we have

$$A' = 180^\circ - a, \quad B' = 180^\circ - b, \quad C' = 180^\circ - c, \\ a' = 180^\circ - A, \quad b' = 180^\circ - B, \quad c' = 180^\circ - C.$$

Whence,  $\frac{1}{2}(A' - B') = \frac{1}{2}(b - a), \quad \frac{1}{2}(a' + b') = 180^\circ - \frac{A + B}{2},$

$$\frac{1}{2}(a' - b') = \frac{1}{2}(B - A), \quad \frac{1}{2}C' = 90^\circ - \frac{1}{2}c.$$

By the substitution of these values in Eq (n), that equation becomes

$$\tan. \frac{1}{2}(b - a) = \frac{\sin. \frac{1}{2}(B - A)}{\sin. \frac{1}{2}(A + B)} \tan. \frac{1}{2}c,$$

$$\text{or,} \quad \tan. \frac{1}{2}(a - b) = \frac{\sin. \frac{1}{2}(A - B)}{\sin. \frac{1}{2}(A + B)} \tan. \frac{1}{2}c, \quad (p)$$

since  $\tan. \frac{1}{2}(b - a) = -\tan. \frac{1}{2}(a - b)$ , and  $\sin. \frac{1}{2}(B - A) = -\sin. \frac{1}{2}(A - B)$ .

By applying Eq. (8) to the polar triangle, and treating the resulting equation in a manner similar to the above, we find

$$\tan. \frac{1}{2}(a + b) = \frac{\cos. \frac{1}{2}(A - B)}{\cos. \frac{1}{2}(A + B)} \tan. \frac{1}{2}c, \quad (q)$$

Equations (p) and (q) may be resolved into the following proportions.

$$\begin{aligned} \sin. \frac{1}{2}(A + B) : \sin. \frac{1}{2}(A - B) &:: \tan. \frac{1}{2}c : \tan. \frac{1}{2}(a - b); \\ \cos. \frac{1}{2}(A + B) : \cos. \frac{1}{2}(A - B) &:: \tan. \frac{1}{2}c : \tan. \frac{1}{2}(a + b). \end{aligned}$$

These proportions are called Napier's 3d and 4th Analogies, and when expressed in words become the following rules:

1. *The cosine of the half sum of any two angles of a spherical triangle is to the cosine of the half difference of the same angles, as the tangent of half the included side is to the tangent of the half sum of the other two sides.*

2. *The sine of the half sum of any two angles of a spherical triangle is to the sine of the half difference of the same angles, as the tangent of half the included side is to the tangent of the half difference of the other two sides.*

The half sum, and the half difference of two sides of a spherical triangle, may be found by these rules, when two angles and the included side are given; and by adding the half sum to the half difference, we get the greater of these sides, and by subtracting the half difference from the half sum, we get the smaller.

## SECTION IV.

## SPHERICAL TRIGONOMETRY APPLIED.

## SOLUTION OF RIGHT-ANGLED SPHERICAL TRIANGLES.

A GOOD general conception of the sphere is essential to a practical knowledge of spherical trigonometry, and this conception is best obtained by the examination of an artificial globe. By tracing out upon its surface the various forms of right-angled and oblique-angled triangles, and viewing them from different points, we may soon acquire the power of making a natural representation of them on paper, which will be found of much assistance in the solution and interpretation of problems.

For instance, suppose one side of a right-angled spherical triangle to be  $56^\circ$ , and the angle between this side and the hypotenuse to be  $24^\circ$ . What is the hypotenuse, and what the other side and angle?

A person might solve this problem by the application of the proper equations or proportions, without really comprehending it; that is, without being able to form a distinct notion of the shape of the triangle, and of its relation to the surface of the sphere on which it is situated.

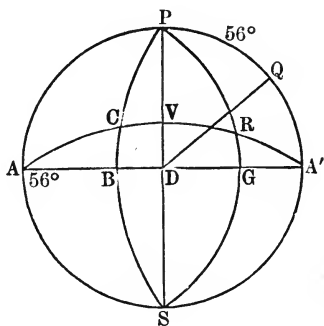
If we refer this triangle to the common geographical globe, the side  $56^\circ$  may be laid off on the equator, or on a meridian. In the first case, the hypotenuse will be the arc of a great circle drawn through one extremity of the side  $56^\circ$ , above or below the equator, and making with

it an angle of  $24^\circ$ ; the other side will be an arc of a meridian. In the second case, the side  $56^\circ$  falling on a meridian, the hypotenuse will be the arc of a great circle drawn through one extremity of this side, on the right or left of the meridian, and making with it an angle of  $24^\circ$ ; the other side will be the arc of a great circle, at right angles to the meridian in which the given side lies.

Generally speaking, the apparent form of a spherical triangle, and consequently the manner of representing it on paper, will differ with the position assumed for the eye in viewing it. From whatever point we look at a sphere, its outline is a perfect circle in the axis of which the eye is situated; and when the eye is, as will be hereafter supposed, at an infinite distance, this circle will be a great circle of the sphere. All great circles of the sphere whose planes pass through the eye, will seem to be diameters of the circle which represents the outline of the sphere.

We will now suppose the eye to be in the plane of the equator, and proceed to construct our triangle on paper.

Let the great circle,  $PASA'$ , represent the outline of the sphere, the diameter  $AA'$  the equator, and the diameter  $PS$  the central meridian, or the meridian in whose plane the eye is situated. Let  $AB = 56^\circ$ , represent the given side, and  $AC$ , making with  $AB$  the angle  $BAC =$



$24^\circ$ , the hypotenuse, then will  $BC$ , the arc of a meridian, be the other side at right angles to  $AB$ , and the triangle,  $ABC$ , corresponds in all respects to the given triangle.

Again measure off  $56^\circ$  from  $P$  to  $Q$ , draw the arc  $DQ$ , make the arc  $A'G$  equal to  $24^\circ$ , and draw the quadrant  $PRG$ . The triangle  $PQR$  will also represent the given triangle in every particular.

We know from the construction, that  $DV, = 24^\circ$ , is greater than  $BC$ , and that  $AC$  is greater than  $AB$ , that is, greater than  $56^\circ$ .

In like manner, we know that  $A', = 24^\circ$ , is greater than  $QR$ , and that  $PR$  is greater than  $PQ$ , because  $PR$  is more nearly equal to  $PG, = 90^\circ$ , than  $PQ$  is to  $PA, = 90^\circ$ .

For illustration and explanation, we also give the following example:

In a right-angled spherical triangle, there are given, the hypotenuse equal to  $150^\circ 33' 20''$ , the angle at the base,  $23^\circ 27' 29''$ , to find the base and the perpendicular. Let  $A'BC$  in the last figure, represent the triangle in which  $A'C = 150^\circ 33' 20''$ , the  $\sphericalangle BA'C = 23^\circ 27' 29''$ , and the sides  $A'B$  and  $BC$  are required.

This problem presents a right-angled spherical triangle, whose base and hypotenuse are each greater than  $90^\circ$ ; and in cases of this kind, let the pupil observe, that the base is greater than the hypotenuse, and the oblique angle opposite the base, is greater than a right angle. In all cases, a spherical triangle and its supplemental triangle make a *lune*. It is  $180^\circ$  from one pole to its opposite, whatever great circle be traversed. It is  $180^\circ$  along the equator  $ABA'$ , and also  $180^\circ$  along the ecliptic  $ACA'$ . The lune always gives two triangles; and when the sides of one of them are greater than  $90^\circ$ , we take the triangle having supplemental sides; hence in this case we operate on the triangle  $ABC$ .

$AC$  is greater than  $AB$ , therefore  $A'B$  is greater than the hypotenuse  $A'C$ .

The  $\sphericalangle ACB$  is less than  $90^\circ$ ; therefore, the adjacent angle  $A'CB$  is greater than  $90^\circ$ , the two together being equal to two right angles.

These facts are technically expressed, by saying, that the sides and opposite angles are of the *same affection*.\*

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\* *Same affection*: that is, both greater or both less than  $90^\circ$ . *Different affection*: the one greater, the other less than  $90^\circ$ .

Now, if the two sides of a right-angled spherical triangle are of the *same affection*, the hypotenuse will be less than  $90^\circ$ ; and if of *different affection*, the hypotenuse will be greater than  $90^\circ$ .

If, in every instance, we make a natural construction of the figure, and use common judgment, it will be impossible to doubt whether an arc must be taken greater or less than  $90^\circ$ .

We will now solve the triangle  $ACB$ .  $AC = 180^\circ - 150^\circ 33' 20'' = 29^\circ 26' 40''$ .

To find  $BC$ , we use Eq. (3) or (13), Prop. 3, Sec. II., thus:

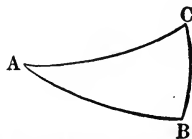
$$\begin{array}{rcl} b, \sin. 29^\circ 26' 40'' & . & 9.691594 \\ A, \sin. \underline{23^\circ 27' 29''} & . & \underline{9.599984} \\ a, \sin. 11^\circ 17' 7'' & . & 9.291578 \end{array}$$

To find  $AB$ , we use equation (1) or (11), thus:

$$\begin{array}{rcl} a, \tan. 11^\circ 17' 7'' & . & 9.300016 \\ A, \cot. \underline{23^\circ 27' 29''} & . & \underline{10.362674} \\ c, \sin. 27^\circ 22' 32'' & . & 9.662690 \\ \hline & & 180 \\ A'B = 152^\circ 37' 28'' \end{array}$$

#### PRACTICAL PROBLEMS IN RIGHT-ANGLED SPHERICAL TRIGONOMETRY.

1. In the right-angled spherical triangle  $ABC$ , given  $AB = 118^\circ 21' 4''$ , and the angle  $A = 23^\circ 40' 12''$ , to find the other parts.



Ans.  $\left\{ \begin{array}{l} AC, 116^\circ 17' 55''; \text{ the angle } C, 100^\circ 59' 26''; \\ \text{and } BC, 21^\circ 5' 42''. \end{array} \right.$

2. In the right-angled spherical triangle  $ABC$ , given  $AB 53^\circ 14' 20''$ , and the angle  $A 91^\circ 25' 53''$ , to find the other parts.

Ans.  $\left\{ \begin{array}{l} AC, 91^\circ 4' 9''; \text{ the angle } C, 53^\circ 15' 8''; \\ \text{and } BC, 91^\circ 47' 10''. \end{array} \right.$

3. In the right-angled spherical triangle  $ABC$ , given  $AB$   $102^{\circ} 50' 25''$ , and the angle  $A$   $113^{\circ} 14' 37''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} AC, 84^{\circ} 51' 36''; \text{ the angle } C, 101^{\circ} 46' 56''; \\ \text{and } BC, 113^{\circ} 46' 27''. \end{array} \right.$$

4. In the right-angled spherical triangle  $ABC$ , given  $AB$   $48^{\circ} 24' 16''$ , and  $BC$   $59^{\circ} 38' 27''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} AC, 70^{\circ} 23' 42''; \text{ the angle } A, 66^{\circ} 20' 40''; \\ \text{and the angle } C, 52^{\circ} 32' 56''. \end{array} \right.$$

5. In the right-angled spherical triangle  $ABC$ , given  $AB$   $151^{\circ} 23' 9''$ , and  $BC$   $16^{\circ} 35' 14''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} AC, 147^{\circ} 16' 51''; \text{ the angle } C, 117^{\circ} 37' 25''; \\ \text{and the angle } A, 31^{\circ} 52' 49''. \end{array} \right.$$

6. In the right-angled spherical triangle  $ABC$ , given  $AB$   $73^{\circ} 4' 31''$ , and  $AC$   $86^{\circ} 12' 15''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} BC, 76^{\circ} 51' 20''; \text{ the angle } A, 77^{\circ} 24' 23''; \\ \text{and the angle } C, 73^{\circ} 29' 40''. \end{array} \right.$$

7. In the right-angled spherical triangle  $ABC$ , given  $AC$   $118^{\circ} 32' 12''$ , and  $AB$   $47^{\circ} 26' 35''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} BC, 134^{\circ} 56' 20''; \text{ the angle } A, 126^{\circ} 19' 2''; \\ \text{and the angle } C, 56^{\circ} 58' 44''. \end{array} \right.$$

8. In the right-angled spherical triangle  $ABC$ , given  $AB$   $40^{\circ} 18' 23''$ , and  $AC$   $100^{\circ} 3' 7''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} \text{The angle } A, 98^{\circ} 38' 53''; \text{ the angle} \\ C, 41^{\circ} 4' 6''; \text{ and } BC, 103^{\circ} 13' 52''. \end{array} \right.$$

9. In the right-angled spherical triangle  $ABC$ , given  $AC$   $61^{\circ} 3' 22''$ , and the angle  $A$   $49^{\circ} 28' 12''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} AB, 49^{\circ} 36' 6''; \text{ the angle } C, 60^{\circ} 29' 20''; \\ \text{and } BC, 41^{\circ} 41' 32''. \end{array} \right.$$

10. In the right-angled spherical triangle  $ABC$ , given

$AB$   $29^\circ 12' 50''$ , and the angle  $C$   $37^\circ 26' 21''$ , to find the other parts.

Ans.  $\left\{ \begin{array}{l} \text{Ambiguous; the angle } A, 65^\circ 27' 57'', \text{ or its} \\ \text{supplement; } AC, 53^\circ 24' 13'', \text{ or its sup-} \\ \text{plement; } BC, 46^\circ 55' 2'', \text{ or its supplement.} \end{array} \right.$

11. In the right-angled spherical triangle  $ABC$ , given  $AB$   $100^\circ 10' 3''$ , and the angle  $C$   $90^\circ 14' 20''$ , to find the other parts.

Ans.  $\left\{ \begin{array}{l} AC, 100^\circ 9' 52'', \text{ or its supplement; } BC, \\ 1^\circ 19' 55'', \text{ or its supplement; and the} \\ \text{angle } A, 1^\circ 21' 12'', \text{ or its supplement.} \end{array} \right.$

12. In the right-angled spherical triangle  $ABC$ , given  $AB$   $54^\circ 21' 35''$ , and the angle  $C$   $61^\circ 2' 15''$ , to find the other parts.

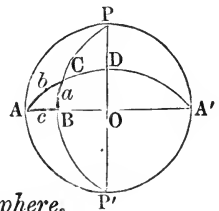
Ans.  $\left\{ \begin{array}{l} BC, 129^\circ 28' 28'', \text{ or its supplement; } AC, \\ 111^\circ 44' 34'', \text{ or its supplement; and the} \\ \text{angle } A, 123^\circ 47' 44'', \text{ or its supplement.} \end{array} \right.$

13. In the right-angled spherical triangle  $ABC$ , given  $AB$   $121^\circ 26' 25''$ , and the angle  $C$   $111^\circ 14' 37''$ , to find the other parts.

Ans.  $\left\{ \begin{array}{l} \text{The angle } A, 136^\circ 0' 5'', \text{ or its supplement;} \\ AC, 66^\circ 15' 38'', \text{ or its supplement; and} \\ BC, 140^\circ 30' 57'', \text{ or its supplement.} \end{array} \right.$

#### QUADRANTAL TRIANGLES.

The solution of right-angled spherical triangles includes, also, the solution of *quadrantal* triangles, as may be seen by inspecting the adjoining figure. *When we have one quadrantal triangle, we have four, which with one right-angled triangle, fill up the whole hemisphere.*



To effect the solution of either of the four quadrantal triangles,  $APC$ ,  $AP'C$ ,  $A'PC$ , or  $A'P'C$ , it is sufficient to solve the small right-angled spherical triangle  $ABC$ .



To the half lune  $AP'B$ , we add the triangle  $ABC$ , and we have the quadrantal triangle  $AP'C$ ; and by subtracting the same from the equal half lune  $APB$ , we have the quadrantal triangle  $PAC$ .

When we have the side,  $AC$ , of the same triangle, we have its supplement,  $A'C$ , which is a side of the triangles  $A'PC$ , and  $A'P'C$ . When we have the side,  $CB$ , of the small triangle, by adding it to  $90^\circ$ , we have  $P'U$ , a side of the triangle  $A'P'C$ ; and subtracting it from  $90^\circ$ , we have  $PC$ , a side of the triangles  $APC$ , and  $A'PC$ .

## PROBLEM I.

*In a quadrantal triangle, there are given the quadrantal side;  $90^\circ$ , a side adjacent,  $42^\circ 21'$ , and the angle opposite this last side, equal to  $36^\circ 31'$ . Required the other parts.*

By this enunciation we cannot decide whether the triangle  $APC$  or  $A'P'C$ , is the one required, for  $AC = 42^\circ 21'$  belongs equally to both triangles. The angle  $APC = A'P'C = 36^\circ 31' = AB$

We operate wholly on the triangle  $ABC$ .

To find the angle  $A$ , call it the *middle part*.

Then,  $R \cos. CAB = R \sin. PAC = \cot. AC \tan. AB$ .

$$\cot. AC = 42^\circ 21' \quad . \quad 10.040231$$

$$\tan. AB = 36^\circ 31' \quad . \quad 9.869473$$

$$\cos. CAB = 35^\circ 40' 51'' \quad 9.909704$$

$$90^\circ$$

---


$$PAC = 54^\circ 19' 9''$$

$$P'AC = 125^\circ 40' 51''$$

To find the angle  $C$ , call it the *middle part*.

$R \cos. ACB = \sin. CAB \cos. AB$ .

$$\sin. CAB = 35^\circ 40' 51'' \quad 9.765869$$

$$\cos. AB = 36^\circ 31' \quad . \quad 9.905085$$

$$\cos. ACB = 62^\circ 2' 45'' \quad 9.670954$$

$$180^\circ$$

---


$$ACP = A'CP' = 117^\circ 57' 15''$$

To find the side  $BC$ , call it the *middle part*.

$$R \sin.BC = \tan.AB \cot.AC B.$$

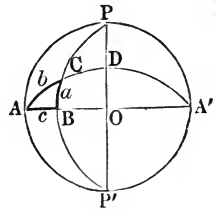
$\tan.AB$	$= 36^\circ 31' 0''$	9.869473
$\cot.AC B$	$= 62^\circ 2' 45''$	9.724835
$\sin.BC$	$= 23^\circ 8' 11''$	9.594308
	$90^\circ$	
<hr/>		
$PC$	$= 66^\circ 51' 49''$	
$P'C$	$= 113^\circ 8' 11''$	

We now have all the sides, and all the angles of the *four* triangles in question.

PROBLEM II.

In a quadrantal spherical triangle, having given the quadrantal side,  $90^\circ$ , an adjacent side,  $115^\circ 09'$ , and the included angle,  $115^\circ 55'$ , to find the other parts.

This enunciation clearly points out the particular triangle  $A'P'C$ .  $A'P' = 90^\circ$ ; and conceive  $A'C = 115^\circ 09'$ . Then the angle  $P'A'C = 115^\circ 55' = P'D$ .



From the angle  $P'A'C$  take  $90^\circ$ , or  $P'A'B$ , and the remainder is the angle  $OA'D = BAC = 25^\circ 55'$ .

We here again operate on the triangle  $ABC$ .  $A'C$ , taken from  $180^\circ$ , gives

$$64^\circ 51' = AC.$$

To find  $BC$ , we call it the *middle part*.

$$R \sin.BC = \sin.AC \sin.BAC.$$

$\sin.AC$	$= 64^\circ 51'$	.	9.956744
$\sin.BAC$	$= 25^\circ 55'$	.	9.640544
$\sin.BC$	$= 23^\circ 18' 19''$	.	9.597288
	$90^\circ$		
<hr/>			
$PC$	$= 113^\circ 18' 19''$		

To find  $AB$ , we call it the *middle part*.

$$R \sin. AB = \tan. BC \cot. BAC.$$

$$\tan. BC = 23^\circ 18' 19'' \quad . \quad 9.634251$$

$$\cot. BAC = 25^\circ 55' \quad . \quad 9.313423$$

$$\sin. AB = 62^\circ 26' 8'' \quad . \quad 8.947674$$

$$180^\circ$$

---


$$A'B = 117^\circ 33' 52'' = \text{the angle } A'P'C.$$

To find the angle  $C$ , we call it the *middle part*.

$$R \cos. C = \cot. AC \tan. BC.$$

$$\cot. AC = 64^\circ 51' \quad . \quad 9.671634$$

$$\tan. BC = 23^\circ 18' 19'' \quad . \quad 9.634251$$

$$\cos. C = 78^\circ \quad . \quad 9.305885$$

$$180^\circ 19' 53'' \quad .$$

---


$$P'CA' = 101^\circ 40' 7''$$

Thus we have found the side  $P'C = 113^\circ 18' 19''$   
 The angle  $A'P'C = 117^\circ 33' 52''$   
 "  $P'CA' = 101^\circ 40' 7''$  } *Ans.*

#### PRACTICAL PROBLEMS.

1. In a quadrantal triangle, given the quadrantal side,  $90^\circ$ , a side adjacent,  $67^\circ 3'$ , and the included angle,  $49^\circ 18'$ , to find the other parts.

*Ans.* { The remaining side is  $53^\circ 5' 44''$ ; the angle  
 opposite the quadrantal side,  $108^\circ 32' 29''$ ;  
 and the remaining angle,  $60^\circ 48' 54''$ .

2. In a quadrantal triangle, given the quadrantal side,  $90^\circ$ , one angle adjacent,  $118^\circ 40' 36''$ , and the side opposite this last-mentioned angle,  $113^\circ 2' 28''$ , to find the other parts.

*Ans.* { The remaining side is  $54^\circ 38' 57''$ ; the angle  
 opposite,  $51^\circ 2' 35''$ ; and the angle opposite  
 the quadrantal side  $72^\circ 26' 21''$ .

3. In a quadrantal triangle, given the quadrantal side,

$90^\circ$ , and the two adjacent angles, one  $69^\circ 13' 16''$ , the other  $72^\circ 12' 4''$ , to find the other parts.

*Ans.* { One of the remaining sides is  $70^\circ 8' 39''$ , the other is  $73^\circ 17' 29''$ , and the angle opposite the quadrantal side is  $96^\circ 13' 23''$ .

4. In a quadrantal triangle, given the quadrantal side,  $90^\circ$ , one adjacent side,  $86^\circ 14' 40''$ , and the angle opposite to that side,  $37^\circ 12' 20''$ , to find the other parts.

*Ans.* { The remaining side is  $4^\circ 43' 2''$ ; the angle opposite,  $2^\circ 51' 23''$ ; and the angle opposite the quadrantal side,  $142^\circ 42' 3''$ .

5. In a quadrantal triangle, given the quadrantal side,  $90^\circ$ , and the other two sides, one  $118^\circ 32' 16''$ , the other  $67^\circ 48' 40''$ , to find the other parts — the three angles.

*Ans.* { The angles are  $64^\circ 32' 21''$ ,  $121^\circ 3' 40''$ , and  $77^\circ 11' 6''$ ; the greater angle opposite the greater side, of course.

6. In a quadrantal triangle, given the quadrantal side,  $90^\circ$ , the angle opposite,  $104^\circ 41' 17''$ , and one adjacent side,  $73^\circ 21' 6''$ , to find the other parts.

*Ans.* { Remaining side,  $49^\circ 42' 16''$ ; remaining angles,  $47^\circ 32' 38''$ , and  $67^\circ 56' 13''$ .

#### SOLUTION OF OBLIQUE-ANGLED SPHERICAL TRIANGLES.

All cases of oblique-angled spherical trigonometry may be solved by right-angled Trigonometry, except two; because every oblique-angled spherical triangle is composed of the sum, or the difference, of two right-angled spherical triangles.

*When a side and two of the angles, or an angle and two of the sides are given, to find the other parts, conform to the following directions:*

Let a perpendicular be drawn from an extremity of a given side, and opposite a given angle or its supplement; this will form two right-angled spherical triangles; and

one of them will have its hypotenuse and one of its adjacent angles given, from which all its other parts can be computed; and some of these parts will become as known parts to the other triangle, from which all its parts can be computed.

To facilitate these computations, we here give a summary of the practical truths demonstrated in the foregoing propositions.

1. *The sines of the sides of spherical triangles are proportional to the sines of their opposite angles.*

2. *The sines of the segments of the base, made by a perpendicular from the opposite angle, are proportional to the cotangents of their adjacent angles.*

3. *The cosines of the segments of the base are proportional to the cosines of the adjacent sides of the triangle.*

4. *The tangents of the segments of the base are reciprocally proportional to the cotangents of the segments of the vertical angle.*

5. *The cosines of the angles at the base are proportional to the sines of the corresponding segments of the vertical angle.*

6. *The cosines of the segments of the vertical angle are proportional to the cotangents of the adjoining sides of the triangle.*

The two cases in which right-angled spherical triangles are not used, are,

1st. When the three sides are given to find the angles; and,

2d. When the three angles are given to find the sides.

The first of these cases is the most important of all, and for that reason great attention has been given to it, and two series of equations, ( $T$  and  $U$ , Prop. 7, Sec. III), have been deduced to facilitate its solution.

As heretofore, let  $ABC$  represent any triangle whose angles are denoted by  $A$ ,  $B$ , and  $C$ , and sides by  $a$ ,  $b$ ,

and  $c$ ; the side  $a$  being opposite  $\sphericalangle A$ , the side  $b$  opposite  $\sphericalangle B$ , etc.

## EXAMPLES.

1. In the triangle  $ABC$ ,  $a = 70^\circ 4' 18''$ ;  $b = 63^\circ 21' 27''$ ; and  $c$ ,  $59^\circ 16' 23''$ ; required the angle  $A$ .

The formula for this is the first equation in group  $T$ , Prop. 7, Sec. III, which is

$$\cos. \frac{A}{2} = \left( \frac{R^2 \sin. S \sin. (S-a)}{\sin. b \sin. c} \right)^{\frac{1}{2}}.$$

We write the second member of this equation thus:

$$\sqrt{\left(\frac{R}{\sin. b}\right) \left(\frac{R}{\sin. c}\right) (\sin. S) \sin. (S-a)},$$

showing four distinct factors under the radical.

The logarithm corresponding to  $\frac{R}{\sin. b}$  is that of  $\sin. b$  subtracted from 10; and of  $\frac{R}{\sin. c}$  is that of  $\sin. c$  subtracted from 10, which we call *sin. complement*.

$BC = a = 70^\circ 4' 18''$	
$AB = c = 59^\circ 16' 23''$	sin. com. .065697
$AC = b = 63^\circ 21' 27''$	sin. com. .048749
	<u>2) 192^\circ 42' 8''</u>
$S = 96^\circ 21' 4''$	sin. 9.997326
$S - a = 26^\circ 16' 46''$	sin. 9.646158
	<u>2) 19.757930</u>
$\frac{1}{2}A = 40^\circ 49' 10''$	cos. 9.878965
	<u>2</u>
$A = 81^\circ 38' 20''$	

When we apply the equation to find the angle  $A$ , we write  $a$  first, at the top of the column; when we apply the equation to find the angle  $B$ , we write  $b$  at the top of the column. Thus,

To find the angle  $B$ .

$$\begin{aligned} \cos. \frac{1}{2} B &= \sqrt{\frac{R^2 \sin. S \sin. (S-b)}{\sin. a \sin. c}} \\ &= \sqrt{\left(\frac{R}{\sin. a}\right) \left(\frac{R}{\sin. c}\right) (\sin. S) \sin. (S-b)} \\ b &= 63^\circ 21' 27'' \\ c &= 59^\circ 16' 23'' \quad \sin. \text{com.} \quad . \quad .065697 \\ a &= 70^\circ 4' 18'' \quad \sin. \text{com.} \quad . \quad .026875 \\ &\quad \underline{2) 192^\circ 42' 8''} \\ S &= 96^\circ 21' 4'' \quad \sin. \quad . \quad .9.997326 \\ S-b &= 32^\circ 59' 37'' \quad \sin. \quad . \quad .9.736034 \\ &\quad \underline{2) 19.825872} \\ \frac{1}{2} B &= 35^\circ 4' 49'' \quad \cos. \quad . \quad .9.912936 \\ &\quad \underline{2} \\ B &= 70^\circ 9' 38'' \end{aligned}$$

By the other equation in formulæ ( $T$ , Prop. 7, Sec. III), we can find the angle  $C$ ; but, for the sake of variety, we will find the angle  $C$  by the application of the third equation in formulæ ( $U$ , Prop. 7, Sec. III).

$$\begin{aligned} \sin. \frac{1}{2} C &= \sqrt{\frac{R^2 \sin. (S-b) \sin. (S-a)}{\sin. b \sin. a}} \\ &= \sqrt{\left(\frac{R}{\sin. b}\right) \left(\frac{R}{\sin. a}\right) \sin. (S-b) \sin. (S-a)} \\ c &= 59^\circ 16' 23'' \\ a &= 70^\circ 4' 18'' \quad \sin. \text{com.} \quad .026817 \\ b &= 63^\circ 21' 27'' \quad \sin. \text{com.} \quad .048479 \\ &\quad \underline{2) 192^\circ 42' 8''} \\ S &= 96^\circ 21' 4'' \\ S-a &= 26^\circ 16' 46'' \quad \sin. \quad . \quad .9.646158 \\ S-b &= 32^\circ 59' 37'' \quad \sin. \quad . \quad .9.736034 \\ &\quad \underline{2) 19.457488} \\ \frac{1}{2} C &= 32^\circ 23' 17'' \quad \sin \quad . \quad .9.778744 \\ &\quad \underline{2} \\ C &= 64^\circ 46' 34'' \\ 85^* \end{aligned}$$

To show the harmony and practical utility of these two sets of equations, we will find the angle  $A$ , from the equation

$$\sin. \frac{1}{2}A = \sqrt{\left(\frac{R}{\sin.b}\right) \left(\frac{R}{\sin.c}\right) \sin.(S-b) \sin.(S-c)}.$$

$$a = 70^\circ 4' 18''$$

$$b = 63^\circ 21' 27'' \quad \sin.com. \quad .048749$$

$$c = 59^\circ 16' 23'' \quad \sin.com. \quad .065697$$

$$2) \underline{192^\circ 42' 8''}$$

$$S = 96^\circ 21' 4''$$

$$S - b = 32^\circ 59' 37'' \quad \sin \quad 9.736034$$

$$S - c = 37^\circ 4' 41'' \quad \sin. \quad \underline{9.780247}$$

$$2) \underline{19.630727}$$

$$\frac{1}{2}A = 40^\circ 49' 10'' \quad \sin. \quad 9.815363$$

2

$$A = 81^\circ 38' 20''$$

2. In a spherical triangle  $ABC$ , given the angle  $A$ ,  $38^\circ 19' 18''$ ; the angle  $B$ ,  $48^\circ 0' 10''$ ; and the angle  $C$ ,  $121^\circ 8' 6''$ ; to find the sides  $a$ ,  $b$ ,  $c$ .

By passing to the triangle polar to this, we have, (Prop. 6, Sec. I, Spherical Geometry),

$$A = 38^\circ 19' 18'' \text{ supplement } 141^\circ 40' 42''$$

$$B = 48^\circ 0' 10'' \text{ supplement } 131^\circ 59' 50''$$

$$C = 121^\circ 8' 6'' \text{ supplement } 58^\circ 51' 54''$$

We now find the angles to the spherical triangle, the sides of which are these supplements.

$$\text{Thus, } \quad 141^\circ 40' 42''$$

$$131^\circ 59' 50'' \quad \sin.com. \quad .128909$$

$$\underline{58^\circ 51' 54''} \quad \sin.com. \quad .067551$$

$$2) \underline{332^\circ 32' 26''}$$

$$166^\circ 16' 13'' \quad \sin. \quad 9.375375$$

$$24^\circ 35' 31'' \quad \sin. \quad \underline{9.619253}$$

$$2) \underline{19.191088}$$

$$66^\circ 47' 37\frac{1}{2}'' \quad \cos. \quad 9.595544$$



$$60^{\circ} 47' 37\frac{1}{2}''$$


---


$$2''$$

$$\text{angle} = 121^{\circ} 35' 15''$$

$$\text{supp.} = 58^{\circ} 24' 45'' = a \text{ of the original triangle.}$$

In the same manner we find  $b = 60^{\circ} 14' 25''$ ;  $c = 89^{\circ} 1' 14''$ .

It is perhaps better to avoid this indirect process of computing the sides of a spherical triangle when the angles are given, by the application of the equations in group *V'* or *W*, Prop. 8, Sec. III. We will illustrate their use by applying the second equation in group (*W*), for computing the side  $b$ . This equation is

$$\sin. \frac{1}{2} b = \left( \frac{-\cos. S \cos. (S - B)}{\sin. A \sin. C} \right)^{\frac{1}{2}}$$

$$A = 38^{\circ} 19' 18''$$

$$B = 48^{\circ} 0' 10''$$

$$C = 121^{\circ} 8' 6''$$

$$2) 207^{\circ} 27' 34''$$

$$S = 103^{\circ} 43' 47'' \quad -\cos. S = +\sin. 13^{\circ} 43' 47'' = 9.375376$$

$$B = 48^{\circ} 0' 10'' \quad \cos. (S - B) = 55^{\circ} 43' 37'' = 9.750612$$

$$(S - B) = 55^{\circ} 43' 37'' \quad 2) 19.125988$$

$$\text{square root} = 9.562994$$

$$\sin. A = 38^{\circ} 19' 18'' = 9.792445$$

$$\sin. C = 121^{\circ} 8' 6'' = 9.932443$$

$$2) 19.724888$$

$$\text{square root} = 9.862444 = 9.862444$$

$$\text{diff.} = 1.700550$$

Add 10, for radius of the table,  $\frac{10}{\quad}$

$$\text{Tabular } \sin. \frac{1}{2} b = 30^{\circ} 7' 14'' = 9.700550$$

$$\frac{2}{\quad}$$

$$b = 60^{\circ} 14' 28'', \text{ nearly.}$$

#### PRACTICAL PROBLEMS.

1. In any triangle,  $ABC$ , whose sides are  $a, b, c$ , given  $b = 118^{\circ} 2' 14''$ ,  $c = 120^{\circ} 18' 33''$ , and the included angle  $A = 27^{\circ} 22' 34''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} a = 23^\circ 57' 13'', \text{ angle } B = 91^\circ 26' 44, \text{ and } C = \\ 102^\circ 5' 52''. \end{array} \right.$$

2. Given,  $A = 81^\circ 38' 17''$ ,  $B = 70^\circ 9' 38''$ , and  $C = 64^\circ 46' 32''$ , to find the sides  $a$ ,  $b$ ,  $c$ .

$$\text{Ans. } \left\{ \begin{array}{l} a = 70^\circ 4' 13'', b = 63^\circ 21' 24'', \text{ and } c = 59^\circ 16' \\ 21''. \end{array} \right.$$

3. Given, the three sides,  $a = 93^\circ 27' 34''$ ,  $b = 100^\circ 4' 26''$ , and  $c = 96^\circ 14' 50''$ , to find the angles  $A$ ,  $B$ , and  $C$ .

$$\text{Ans. } \left\{ \begin{array}{l} A = 94^\circ 39' 4'', B = 100^\circ 32' 19'', \text{ and } C = 96^\circ \\ 58' 35''. \end{array} \right.$$

4. Given, two sides,  $b = 84^\circ 16'$ ,  $c = 81^\circ 12'$ , and the angle  $C = 80^\circ 28'$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} \text{The result is ambiguous, for we may consider} \\ \text{the angle } B \text{ as acute or obtuse. If the angle} \\ B \text{ is acute, then } A = 97^\circ 13' 45'', B = 83^\circ 11' \\ 24'', \text{ and } a = 96^\circ 13' 33''. \text{ If } B \text{ is obtuse, then} \\ A = 21^\circ 16' 43'', B = 96^\circ 48' 36'', \text{ and } a = \\ 21^\circ 19' 29''. \end{array} \right.$$

5. Given, one side,  $c = 64^\circ 26'$ , and the angles adjacent,  $A = 49^\circ$ , and  $B = 52^\circ$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} b = 45^\circ 56' 46'', a = 43^\circ 29' 49'', \text{ and } C = 98^\circ \\ 28' 4''. \end{array} \right.$$

6. Given, the three sides,  $a = 90^\circ$ ,  $b = 90^\circ$ ,  $c = 90^\circ$ , to find the angles  $A$ ,  $B$ , and  $C$ .

$$\text{Ans. } A = 90^\circ, B = 90^\circ, \text{ and } C = 30^\circ.$$

7. Given, the two sides,  $a = 77^\circ 25' 11''$ ,  $c = 128^\circ 13' 47''$ , and the angle  $C = 131^\circ 11' 12''$ , to find the other parts.

$$\text{Ans. } \left\{ \begin{array}{l} b = 84^\circ 29' 20'', A = 69^\circ 13' 59'' \text{ and } B = 72^\circ 28' \\ 42''. \end{array} \right.$$

8. Given, the three sides,  $a = 68^\circ 34' 13''$ ,  $b = 59^\circ 21' 18''$ , and  $c = 112^\circ 16' 32''$ , to find the angles  $A$ ,  $B$ , and  $C$ .

$$\text{Ans. } \left\{ \begin{array}{l} A = 45^\circ 26' 38'', B = 41^\circ 11' 30', C = 134^\circ 53' \\ 55''. \end{array} \right.$$

9. Given,  $a = 89^\circ 21' 37''$ ,  $b = 97^\circ 18' 39''$ ,  $c = 86^\circ 53' 46''$ , to find  $A$ ,  $B$ , and  $C$ .

$$\text{Ans. } \begin{cases} A = 88^\circ 57' 20'' \\ \quad 17'' \\ B = 97^\circ 21' 26'' \\ C = 86^\circ 47' \end{cases}$$

10. Given,  $a = 31^\circ 26' 41''$ ,  $c = 43^\circ 22' 13''$ , and the angle  $A = 12^\circ 16'$ , to find the other parts.

$$\text{Ans. } \begin{cases} \text{Ambiguous; } b = 73^\circ 7' 34'', \text{ or } 12^\circ 17' 40''; \\ \text{angle } B = 157^\circ 3' 44'', \text{ or } 4^\circ 58' 30''; C = 16^\circ \\ \quad 14' 27'', \text{ or } 163^\circ 45' 33''. \end{cases}$$

11. In a triangle,  $ABC$ , we have the angle  $A = 56^\circ 18' 40''$ ,  $B = 39^\circ 10' 38''$ ;  $AD$ , one of the segments of the base, is  $32^\circ 54' 16''$ . The point  $D$  falls upon the base  $AB$ , and the angle  $C$  is obtuse. Required the sides of the triangle and the angle  $C$ .

$$\text{Ans. } \begin{cases} \text{Ambiguous; } C = 135^\circ 25', \text{ or} \\ \quad 135^\circ 57'; c = 122^\circ 29', \text{ or} \\ \quad 123^\circ 19'; a = 89^\circ 40', \text{ or} \\ \quad 90^\circ 20'; b = 49^\circ 23' 41''. \end{cases}$$

12. Given,  $A = 80^\circ 10' 10''$ ,  $B = 58^\circ 48' 36''$ ,  $C = 91^\circ 52' 42''$ , to find  $a$ ,  $b$ , and  $c$ .

$$\text{Ans. } a = 79^\circ 38' 22'', b = 58^\circ 39' 16'', c = 86^\circ 12' 50''.$$

SECTION V.

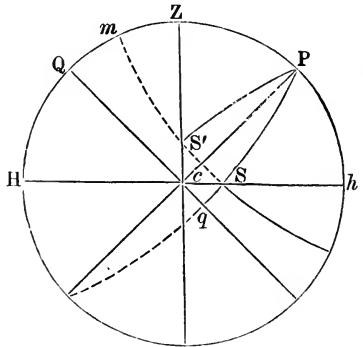
APPLICATIONS OF SPHERICAL TRIGONOMETRY TO ASTRONOMY AND GEOGRAPHY.

SPHERICAL TRIGONOMETRY APPLIED TO ASTRONOMY.

SPHERICAL TRIGONOMETRY becomes a science of incalculable importance in its connection with geography, navigation, and astronomy; for neither of these subjects can be understood without it; and to stimulate the student to a study of the science, we here attempt to give him a glimpse at some of its points of application.

Let the lines in the annexed figure represent circles in the heavens above and around us.

Let  $Z$  be the zenith, or the point just overhead,  $Hch$  the horizon,  $PZH$  the meridian in the heavens, and  $P$  the pole of the celestial equator;  $Ph$  is the latitude of the observer, and  $PZ$  is the co. latitude.



$Qeq$  is a portion of the equator, and the dotted, curved line,  $mS''S$ , parallel to the equator, is the parallel of the sun's declination at some particular time; and in this figure the sun's declination is supposed to be north. By the revolution of the earth on its axis, the

sun is apparently brought from the horizon, at  $S$ , to the meridian, at  $m$ ; and from thence it is carried down on the same curve, on the other side of the meridian; and this apparent motion of the sun (or of any other celestial body,) makes angles at the pole  $P$ , which are in direct proportion to their times of description.

The apparent straight line,  $Zc$ , is what is denominated, in astronomy, the *prime vertical*; that is, the east and west line through the zenith, passing through the *east* and *west* points in the horizon.

When the latitude of the place is north, and the declination is also north, as is represented in this figure, the sun rises and sets on the horizon to the north of the east and west points, and the distance is measured by the arc,  $cS$ , on the horizon.

This arc can be found by means of the right-angled spherical triangle  $eqS$ , right-angled at  $q$ .  $Sq$  is the sun's declination, and the angle  $Scq$  is equal to the *co. latitude* of the place; for the angle  $Pch$  is the latitude, and the angle  $Scq$  is its complement.

The side  $eq$ , a portion of the equator, measures the angle  $cPq$ , the time of the sun's rising or setting before or after *six o'clock*, apparent time. Thus we perceive that this little triangle,  $cSq$ , is a very important one.

When the sun is exactly *east* or *west*, it can be determined by the triangle  $ZPS'$ ; the side  $PZ$  is known, being the *co. latitude*; the angle  $PZS'$  is a right angle, and the side  $PS'$  is the sun's polar distance. Here, then, are the hypotenuse and side of a right-angled spherical triangle given, from which the other parts can be computed. The angle  $ZPS'$  is the time from noon, and the side  $ZS'$  is the sun's zenith distance at that time.

The following problems are given, to illustrate the important applications that can be made of the right-angled triangle  $eqS$ .

## PRACTICAL PROBLEMS.

1. At what time will the sun rise and set in Lat.  $48^{\circ}$  N., when its declination is  $21^{\circ}$  N.?

In this problem, we must make  $qS=21^{\circ}$ ,  $Ph=48^{\circ}$  = the angle  $Pch$ . Then the angle  $Scq=42^{\circ}$ . It is required to find the arc  $cq$ , and convert it into time at the rate of four minutes to a degree. This will give the apparent time after six o'clock that the sun sets, and the apparent time before six o'clock that the sun rises, (no allowance being made for refraction).

Making  $cq$  the middle part, we have

$$R \sin.cq = \tan.21^{\circ} \tan.48^{\circ}$$

$$\tan.21^{\circ} = 9.584177$$

$$\tan.48^{\circ} = 10.045563$$

$$cq = 25^{\circ} 14' 5'' = 25.2346^{\circ} \quad 9.629740, \text{ rejecting } 10.$$

4

$$\hline 1^h 40^m 56'$$

Adding to

$$6^h$$

Sun sets P. M.,

$$\hline 7^h 40^m 56', \text{ apparent time,}$$

From

$$6^h$$

Taking

$$\hline 1^h 40^m 56'$$

Sun rises A. M.,  $4^h 19^m 4'$ , apparent time.

From this we derive the following rule for finding the apparent time of sunrise and sunset, assuming that the declination undergoes no change in the interval between these instants, which we may do without much error.

## R U L E.

*To the logarithmic tangent of the sun's declination, add the logarithmic tangent of the latitude of the observer; and, after rejecting ten from the result, find from the tables the arc of which this is the logarithmic sine, and convert it into time at the rate of 4 minutes to a degree.*

*This time, added to 6 o'clock, will give the time of sunset, and, subtracted from 6 o'clock, will give the time of sunrise,*

when the latitude and declination are both north or both south, but when one is north, and the other south, the addition gives the time of sunrise, and the subtraction the time of sunset.

2. At what time will the sun set when its declination is  $23^{\circ} 12' N.$ , and the latitude of the place is  $42^{\circ} 40' N.$ ?

*Ans.*  $7^h 33^m 4^s$ , apparent time.

3. What will be the time of sunset for places whose latitude is  $42^{\circ} 40' N.$ , when the sun's declination is  $15^{\circ} 21'$  south?

*Ans.*  $5^h 1^m 23^s$ , apparent time.

4. What will be the time of sunrise and sunset for places whose latitude is  $52^{\circ} 30' N.$ , when the sun's declination is  $18^{\circ} 42'$  south?

*Ans.*  $\left\{ \begin{array}{l} \text{Rises } 7^h 44^m 42^s, \\ \text{Sets } 4^h 15^m 18^s, \end{array} \right\}$  apparent time.

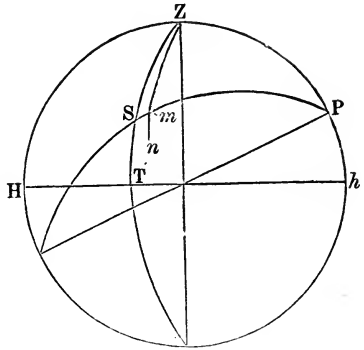
5. What will be the time of sunset and of sunrise at St. Petersburg, in lat.  $59^{\circ} 56'$ , north, when the sun's declination is  $23^{\circ} 24'$ , north? What will be its amplitude at these instants? Also, at what hours will it be due east and west, and what will be its altitude at such times?

*Ans.*  $\left\{ \begin{array}{l} \text{Sun sets at } 9^h 13^m 30' \text{ P.M.} \\ \text{Sun rises at } 2^h 46^m 30' \text{ A.M.} \\ \text{Sun rises N. of east} \\ \text{Sun sets N. of west} \\ \text{Sun is east at } 6^h 58^m 2^s \text{ A.M.} \\ \text{Sun is west at } 5^h 1^m 58^s \text{ P.M.} \\ \text{Alt. when east and west is } 27^{\circ} 18' 57''. \end{array} \right\}$  apparent time.

#### ON THE APPLICATION OF OBLIQUE-ANGLED SPHERICAL TRIANGLES.

One of the most important problems in navigation and astronomy, is the determination of the formula for

time. This problem will be understood by the triangle  $PZS$ . When the sun is on the meridian, it is then apparent noon. When not on the meridian, we can determine the interval from noon, by means of the triangle  $PZS$ ; for we can know all its sides; and the angle at  $P$ , changed into



time at the rate of  $15^\circ$  to one hour, will give the time from apparent noon, when any particular altitude, as  $TS$ , may have been observed.  $PS$  is known, by the sun's declination at about the time; and  $PZ$  is known, if the observer knows his latitude.

Having these three sides, we can always find the sought angle at the pole, by the equations already given in formulæ ( $T$ , or  $U$ , Prop. 7, Sec. III); but these formulæ require the use of the *co.latitude* and the *co.altitude*, and the practical navigator is very averse to taking the trouble of finding the complements of arcs, when he is quite certain that formulæ can be made, comprising but the arcs themselves.

The practical man, also, *very properly* demands the most concise practical results. No matter how much labor is spent in theorizing, provided we arrive at practical brevity; and for the especial accommodation of seamen, the following formula for finding time has been deduced.

From the symmetrical formulæ ( $S'$ ) Prop. 7, Sec. III, we have,

$$\cos P = \frac{\cos.ZS - \cos.PZ \cos.PS}{\sin.PZ \sin.PS}$$

Now, in place of  $\cos.ZS$ . we take  $\sin.ST$ , which is, in



fact, the same thing; and in place of  $\cos.PZ$ , we take  $\sin.\text{lat.}$ , which is also the same.

In short, let  $A$  = the altitude of the sun,  $L$  = the latitude of the observer, and  $D$  = the sun's polar distance.

$$\text{Then, } \cos.P = \frac{\sin.A - \sin.L \cos.D}{\cos.L \sin.D}$$

But,  $2\sin.^2 \frac{1}{2}P = 1 - \cos.P$ . (See Eq. 32, Prop. 2, Sec. I, Plane Trig.)

Therefore,

$$\begin{aligned} 2\sin.^2 \frac{1}{2}P &= 1 - \frac{\sin.A - \sin.L \cos.D}{\cos.L \sin.D} \\ &= \frac{(\cos.L \sin.D + \sin.L \cos.D) - \sin.A}{\cos.L \sin.D} \\ &= \frac{\sin.(L + D) - \sin.A}{\cos.L \sin.D} \end{aligned}$$

Considering  $(L + D)$  as a single arc, and (applying Equation 16, Sec. I, Plane Trig.), we have, after dividing by 2,

$$\sin.^2 \frac{1}{2}P = \frac{\cos.\left(\frac{L + D + A}{2}\right) \sin.\left(\frac{L + D - A}{2}\right)}{\cos.L \sin.D}$$

$$\text{But, } \frac{L + D - A}{2} = \frac{L + D + A}{2} - A,$$

$$\text{and if we assume } S = \frac{L + D + A}{2},$$

$$\text{we shall have, } \sin.^2 \frac{1}{2}P = \frac{\cos.S \sin.(S - A)}{\cos.L \sin.D}$$

$$\text{Or, } \sin.\frac{1}{2}P = \sqrt{\frac{\cos.S \sin.(S - A)}{\cos.L \sin.D}}$$

This is the final result, when the radius is unity; when the radius is  $R$  times greater, then the  $\sin.\frac{1}{2}P$  will be  $R$  times greater; and, therefore, the value of this sine, corresponding to our tables, is,

$$\sin.\frac{1}{2}P = \sqrt{\left(\frac{R}{\cos.L}\right) \left(\frac{R}{\sin.D}\right) \cos.S \sin.(S - A)}$$

## PRACTICAL PROBLEMS.

1. In lat.  $39^{\circ} 6' 20''$  North, when the sun's declination was  $12^{\circ} 3' 10''$  North, the true altitude\* of the sun's center was observed to be  $30^{\circ} 10' 40''$ , *rising*. What was the apparent time?

$$\begin{array}{rcl}
 \text{Alt.} & 30^{\circ} 10' 30'' & \\
 \text{Lat.} & 39^{\circ} 6' 20'' & \text{cos.com.} \quad .110146 \\
 \text{P.D.} & 77^{\circ} 56' 50'' & \text{sin.com.} \quad .009680 \\
 & \hline
 & 2) 147^{\circ} 13' 40'' & \\
 & \hline
 S & = 73^{\circ} 36' 50'' & \text{cos.} \quad 9.450416 \\
 (S - A) & = 43^{\circ} 26' 20'' & \text{sin.} \quad 9.837299 \\
 & & \hline
 & & 2) 19.407541 \\
 & & \hline
 & 30^{\circ} 22' 5'' & \text{sin.} \quad 9.703770 \\
 & \quad \quad \quad 2 & \\
 & \hline
 P & = 60^{\circ} 44' 10'' &
 \end{array}$$

This angle, converted into time at the rate of  $15^{\circ}$  to one hour, or 4 minutes to  $1^{\circ}$ , gives  $4^{\text{h}} 2^{\text{m}} 56'$  from apparent noon; and as the sun was rising, it was before noon or

$$7^{\text{h}} 57^{\text{m}} 4' \text{ A. M.}$$

If to this the equation of time were applied, we should have the mean time; and if such time were compared with that of a clock or watch, we could determine its error. A good observer, with a good instrument, can, in this manner, determine the local time within 4 or 5 seconds.

2. In lat.  $40^{\circ} 21'$  North, the true altitude of the sun, in the forenoon, was found to be  $36^{\circ} 12'$ , when the declina-

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\* The instrument used, the manner of taking the altitude, its correction for refraction, semi-diameter, and other practical or circumstantial details, do not belong to a work of this kind, but to a work of Practical Astronomy or Navigation.

tion of the sun was  $3^{\circ} 20'$  South. What was the apparent time?  
*Ans.*  $9^h 42^m 40^s$  A. M.

3. In latitude  $21^{\circ} 2'$  South, when the sun's declination was  $18^{\circ} 32'$  North, the true altitude, in the afternoon, was found to be  $40^{\circ} 8'$ . What was the apparent time of day?  
*Ans.*  $2^h 3^m 57^s$  P. M.

### SPHERICAL TRIGONOMETRY APPLIED TO GEOGRAPHY.

If we wish to find the shortest distance between two places over the surface of the earth, when the distance is considerable, we must employ Spherical Trigonometry.

Suppose the least distance between Rome and New Orleans is required; we would first find the distance in degrees and parts of a degree, and then multiply that distance by the number of miles in one degree.

In the solution of this problem, it is supposed that we have the latitude and longitude of both places. Then the distances, in degrees, from the north pole of the earth to Rome and to New Orleans are the two sides of a spherical triangle, the difference of longitude of the two places is the angle at the pole included between these sides, and the problem is, to determine the third side of a spherical triangle, when we have two sides and the included angle given.

Let  $P$  be the north pole,  $R$  the position of Rome, and  $N$  that of New Orleans.

	Lat.	Long.	
New Orleans,	$29^{\circ} 57' 30''$ N.	$90^{\circ}$	W.
Rome,	$41^{\circ} 53' 54''$ N.	$12^{\circ} 28' 40''$ E.	

Whence,  $PR = 48^{\circ} 6' 6''$ ,  
 $PN = 60^{\circ} 2' 30''$ .

Angle  $NPR = 102^{\circ} 28' 40''$ .

We now employ Napier's 1st and 2d Analogies, and find the distance, in degrees, to be  $78^{\circ} 48' 15''$ . This reduced to miles, at the rate of 69.16 miles to the degree, will make the distance 5450.1 miles.

The angle at  $N$  is  $47^{\circ} 48' 13''$  and at  $R$ ,  $59^{\circ} 34' 47''$ .

The third side of a spherical triangle can be found by a single formula, as we shall see by inspecting formulæ ( $S'$ ) Prop. 7, Sec. III.

Let  $C$  be the included angle, and  $c$  the unknown side opposite; then,

$$\cos.C = \frac{\cos.c - \cos.a \cos.b}{\sin.a \sin.b}.$$

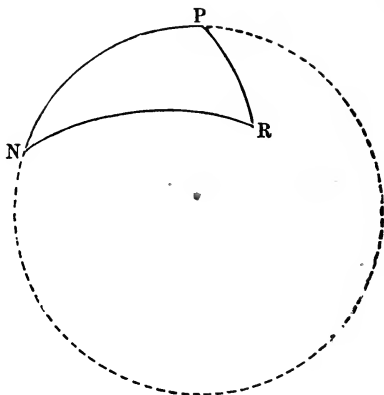
Adding 1 to each member, and reducing, observing at the same time that  $1 + \cos.C = 2\cos.^2 \frac{1}{2}C$ , we have,

$$2\cos.^2 \frac{1}{2}C = \frac{\sin.a \sin.b - \cos.a \cos.b + \cos.c}{\sin.a \sin.b}.$$

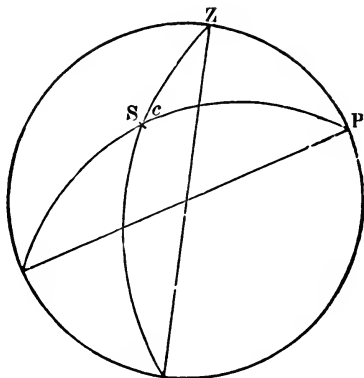
Whence,  $2\cos.^2 \frac{1}{2}C \sin.a \sin.b = \cos.c - \cos.(a + b)$ ;  
or,  $\cos.c = \cos.(a + b) + 2\cos.^2 \frac{1}{2}C \sin.a \sin.b$ .

The second member of this equation is the algebraic sum of two decimal fractions, and expresses the value of the natural cosine of the side sought.

This case of Spherical Trigonometry, namely, that in which two sides and the included angle are given, to find the third side, is very extensively used in practical astronomy, in finding the angular distance of the moon from the sun, stars, and planets. For this purpose, the right ascension and declination of each body must be



found for the same moment of absolute time. Their difference in right ascension gives the included angle,  $P$ , at the celestial pole. The declination subtracted from  $90^\circ$ , if it be north, and added to  $90^\circ$ , if it be south, will give the sides,  $PZ$  and  $PS$ .



In the following examples, we give the right ascension and declination of the bodies, and from these the student is required to compute the distance between them.

The right ascensions are given in time. Their difference must be changed to degrees for the included angle.

## MEAN TIME GREENWICH.

June 24, 1860.

MOON'S			JUPITER'S			Distance.
R. A.	Dec.		R. A.	Dec.		
h. m. s.	° ' "		h. m. s.	° ' "		° ' "
At noon, 10 51 36.5	3 35 24 N.		8 4 27.6	20 51 36.8 N.		44 8 12
" 3 h., 10 58 1	2 47 43		8 4 34.2	20 51 17.8		45 53 47
" 6 h., 11 4 24.6	1 59 56.2		8 4 40.8	20 50 58.7		47 39 18
" 9 h., 11 10 47.6	1 12 6.1		8 4 47.4	20 50 39.6		49 24 43

October 6, 1860.

☾ R. A.			☉ R. A.			Distance.
R. A.	Dec.		R. A.	Dec.		
h. m. s.	° ' "		h. m. s.	° ' "		° ' "
At noon, 5 41 20.8	26 8 0 N.		12 49 29.3	5 18 42.6 S.		107 37 2
" 3 h., 5 48 30.1	26 3 20		12 49 56.7	5 21 35.4		106 8 19
" 6 h., 5 55 40	25 57 19.4		12 50 24.1	5 24 28.2		104 39 19
" 9 h., 6 2 50.5	25 49 58.1		12 50 51.4	5 27 20.9		103 10 0
" 12 h., 6 10 1.3	25 41 15.8		12 51 19.0	5 30 13.5		101 40 27

## SECTION VI.

## REGULAR POLYEDRONS

A **Regular Polyedron** is a polyedron having all its faces equal and regular polygons, and all its polyedral angles equal.

The sum of all the plane angles bounding any polyedral angle is less than four right angles; and as the angle of the equilateral triangle is  $\frac{2}{3}$  of a right angle, we have  $\frac{2}{3} \times 3 < 4$ ,  $\frac{2}{3} \times 4 < 4$ , and  $\frac{2}{3} \times 5 < 4$ ; but  $\frac{2}{3} \times 6 = 4$ ,  $\frac{2}{3} \times 7 > 4$ , and so on. Hence, it follows that three, and only three, polyedral angles may be formed, having the equilateral triangle for faces; namely, a triedral angle and polyedral angles of four and of five faces.

There are, therefore, three distinct regular polyedrons bounded by the equilateral triangle.

1. The **Tetraedron**, having four faces and four solid angles.
2. The **Octaedron**, having eight faces and six solid angles.
3. The **Icosaedron**, having twenty faces and twenty solid angles.

With right plane angles we can form only a triedral angle; hence, with equal squares we may bound a solid having six faces and eight equal triedral angles. This solid is called the **Hexaedron**.

The angle of the regular pentagon being  $\frac{6}{5}$  of a right angle, we have  $\frac{6}{5} \times 3 < 4$ ; but  $\frac{6}{5} \times 4 > 4$ ; hence, with plane angles equal to those of the regular pentagon, we can form only a triedral angle. The solid bounded by twelve regular pentagons, and having twenty solid angles, is called the **Dodecaedron**.

There are, then, but five regular polyedrons, viz.: The *tetraedron*, the *octaedron*, and the *icosaedron*, each of which has the equilateral triangle for faces; the *hexaedron*, whose faces are equal squares, and the *dodecaedron*, whose faces are equal regular pentagons.

It is obvious that a sphere may be circumscribed about, or inscribed within, any of these regular solids, and conversely: and

that these spheres will have a common center, which may also be taken as the *center* of the polyedron.

Any regular polyedron may be regarded as made up of a number of regular pyramids, whose bases are severally the faces of the polyedron, and whose common vertex is its center. Each of these pyramids will have, for its altitude, the radius of the inscribed sphere; and since the volume of the pyramid is measured by one third of the product of its base and altitude, it follows that the volume of any regular polyedron is measured by its surface multiplied by one third of the radius of the inscribed sphere.

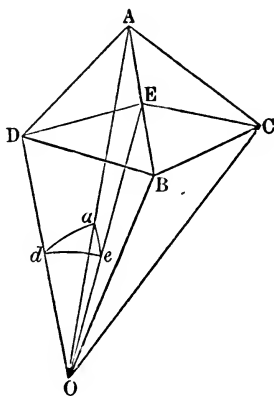
### PROBLEM.

*Given, the name of a regular polyedron, and the side of the bounding polygon, to find the inclination of its faces; the radii of the inscribed and circumscribed spheres; the area of its surface; and its volume.*

Let  $AB$  be the intersection of two adjacent faces of the polyedron, and  $C$  and  $D$  the centers of these faces,  $O$  being the center of the polyedron. Draw the radii,  $OC$  and  $OD$ , of the inscribed, and the radii  $OA$  and  $OB$ , of the circumscribed sphere; also from  $C$  and  $D$  let fall the perpendiculars  $CE$  and  $DE$ , on the edge  $AB$ , and draw  $OE$ ; then will the angle  $DEC$  measure the inclination of the faces of the polyedron, and the angle  $DEO$  is one half of this inclination.

Let  $I$  denote the inclination of the faces,  $m$  the number of faces which meet to form a polyedral angle,  $n$  the number of sides in each face, and suppose the edge of the polyedron to be unity.

The surface of the sphere of which  $O$  is the center, and radius unity, will form, by its intersections with the planes,  $AOE$ ,  $AOD$ ,  $DOE$ , the right-angled spherical triangle  $dae$ , right-angled at  $e$ . In the right-angled triangle  $DEO$ , the angle  $DOE$  is equal to



$$90^\circ - DEO = 90^\circ - \frac{1}{2}I,$$

and is measured by the arc  $de$ . The angle  $dae$ , of the spherical triangle, is equal to  $\frac{360^\circ}{2m}$ , and the angle  $ade = \frac{360^\circ}{2n}$ .

Now, by Napier's Rules we have

$$\cos.dae = \sin.ade \cos.de.$$

$$\text{or,} \quad \cos.de = \frac{\cos.dae}{\sin.ade}; \quad (1)$$

$$\text{and,} \quad \cos.ad = \cot.dae \cot.ade \quad (2)$$

Substituting in eq. (1), for the angles  $dae$  and  $ade$ , their values, we find

$$\sin.\frac{1}{2}I = \frac{\frac{\cos.360^\circ}{2m}}{\frac{\sin.360^\circ}{2n}} \quad (3)$$

Equation (3) gives the value of the sine of one half of the inclination of the planes; and by means of this equation we may readily find the radii of the inscribed and circumscribed spheres.

In the triangle  $BED$ , we have

$$DE = BE \cot.BDE = \frac{1}{2} \cot. \frac{360^\circ}{2n},$$

since  $AB = 1$ , and  $BE = \frac{1}{2}AB$ .

In the triangle  $DOE$ , we have

$$OD = DE \tan. \frac{1}{2}I = \frac{1}{2} \cot. \frac{360^\circ}{2n} \tan.\frac{1}{2}I \quad (4)$$

From the triangle  $AOD$ , we find

$$\cos.DOA : 1 :: OD : OA$$

$$\text{whence} \quad OA = \frac{OD}{\cos.DOA}$$

But the angle  $DOA$  is measured by the arc  $ad$ ; hence, substituting in this last equation the values of  $\cos.DOA$  and  $OD$ , taken from eqs. (2) and (4), we have

$$\begin{aligned} OA &= \frac{1}{2} \tan.\frac{1}{2}I \cot. \frac{360^\circ}{2n} \times \frac{1}{\frac{\cot.360^\circ}{2m}} \times \frac{1}{\frac{\cot.360^\circ}{2n}} \\ &= \frac{1}{2} \tan.\frac{1}{2}I \tan. \frac{360^\circ}{2m}, \end{aligned} \quad (5)$$

by writing  $\tan.$  for  $\frac{1}{\cot.}$ , and reducing.



Equation (4) gives the value of  $OD$ , the radius of the inscribed sphere, and equation (5) gives that of  $OA$ , the radius of the circumscribed sphere. The area of one of the faces of the polyedron is equal to one half of the apothegm multiplied by the perimeter.

The apothegm, as found above, is equal to  $\frac{1}{2} \cot. \frac{360^\circ}{2n}$ ; hence, we

have  $\frac{1}{2}n \times \frac{1}{2} \cot. \frac{360^\circ}{2n}$ , for the area of one of the faces; and multi-

plying this by the number of faces of the polyedron, we shall have the expression for its entire area. The expression for the surface multiplied by one third of the radius of the inscribed sphere, gives the measure of the volume of the polyedron.

In what precedes, we have supposed the edge of the polyedron to be unity. Having found the radii of the inscribed and circumscribed spheres, the surfaces, and the volumes of such polyedrons, to determine the radii, surfaces, and volumes of regular polyedrons having any edge whatever, we have merely to remember that the homologous dimensions of similar bodies are proportional; their surfaces are as the squares of these dimensions; and their volumes as the cubes of the same.

Formula (3) gives, for the inclination of the adjacent faces of

The Tetraedron,	70° 31' 44''
“ Hexaedron,	90° 00' 00''
“ Octaedron,	109° 28' 18''
“ Dodecaedron,	116° 33' 54''
“ Icosaedron,	138° 11' 23''

The subjoined table gives the surfaces and volumes of the regular polyedrons, when the edge is unity.

	Surfaces.	Volumes.
Tetraedron,	1.7320508	0.1178513
Hexaedron,	6.0000000	1.0000000
Octaedron,	3.4641016	0.4714045
Dodecaedron,	20.6457288	7.6631189
Icosaedron,	8.6602540	2.1816950

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LOGARITHMIC TABLES;

ALSO A TABLE OF

NATURAL AND LOGARITHMIC

SINES, COSINES, AND TANGENTS

TO EVERY MINUTE OF THE QUADRANT.

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# LOGARITHMS OF NUMBERS

FROM

1 TO 10000.

N.	Log.	N.	Log.	N.	Log.	N.	Log.
1	0 000000	26	1 414973	51	1 707570	76	1 880814
2	0 301030	27	1 431364	52	1 716003	77	1 886491
3	0 477121	28	1 447158	53	1 724276	78	1 892095
4	0 602060	29	1 462398	54	1 732394	79	1 897627
5	0 698970	30	1 477121	55	1 740363	80	1 903090
6	0 778151	31	1 491362	56	1 748188	81	1 908485
7	0 845098	32	1 505150	57	1 755875	82	1 913814
8	0 903090	33	1 518514	58	1 763428	83	1 919078
9	0 954243	34	1 531479	59	1 770852	84	1 924279
10	1 000000	35	1 544068	60	1 778151	85	1 929419
11	1 041393	36	1 556303	61	1 785330	86	1 934498
12	1 079181	37	1 568202	62	1 792392	87	1 939519
13	1 113943	38	1 579,84	63	1 799341	88	1 944483
14	1 146128	39	1 591065	64	1 806180	89	1 949390
15	1 176091	40	1 602060	65	1 812913	90	1 954243
16	1 204120	41	1 612784	66	1 819544	91	1 959041
17	1 230449	42	1 623249	67	1 826075	92	1 963788
18	1 255273	43	1 633468	68	1 832509	93	1 968483
19	1 278754	44	1 643453	69	1 838849	94	1 973128
20	1 301030	45	1 653213	70	1 845098	95	1 977724
21	1 322219	46	1 662758	71	1 851258	96	1 982271
22	1 342423	47	1 672098	72	1 857333	97	1 9867,2
23	1 361728	48	1 681241	73	1 863323	98	1 991226
24	1 380211	49	1 690196	74	1 869232	99	1 995635
25	1 397940	50	1 698970	75	1 875031	100	2 000000

N. B. In the following table, in the last nine columns of each page, where the first or leading figures change from 9's to 0's, points or dots are now introduced instead of the 0's through the rest of the line, to catch the eye, and to indicate that from thence the corresponding natural number in the first column stands in the *next lower line*, and its annexed first two figures of the Logarithms in the *second column*.

LOGARITHMS OF NUMBERS.

3

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104	7033	7451	7868	8284	8700	9116	9532	9947	.361	.775
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107	9384	9789	.195	.600	1001	1408	1812	2216	2619	3021
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114	6905	7286	7666	8046	8426	8805	9185	9563	9942	.320
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116	4458	4832	5205	5580	5953	6326	6699	7071	7443	7815
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125	6910	7257	7604	7951	8298	8644	8990	9335	9681	1026
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142	152288	2594	2900	3205	3510	3815	4120	4424	4728	5032
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155	190332	0612	0892	1171	1451	1730	2010	2289	2567	2846
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158	8657	8932	9206	9481	9755	.29	.303	.577	.850	1124
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163	212188	2454	2.20	2986	3252	3518	3783	4049	4314	4579
164	4844	5109	5373	5638	5902	6166	6430	6694	6957	7221
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165	7484	7747	8010	8273	8536	8798	9060	9323	9585	9846
166	220108	0370	0631	0892	1153	1414	1675	1936	2196	2456
167	2716	2976	3236	3496	3755	4015	4274	4533	4792	5051
168	5309	5568	5.26	6084	6342	6600	6858	7115	7372	7630
169	7887	8144	8400	8657	8913	9170	9426	9682	9938	.193
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171	2996	3250	3504	3757	4011	4264	4517	4770	5023	5276
172	5528	5781	6033	6285	6537	6789	7041	7292	7544	7795
173	8046	8297	8548	8799	9049	9299	9550	9800	.50	.300
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175	3038	3283	3534	3782	4030	4277	4525	4772	5019	5266
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177	7973	8219	8464	8709	8954	9198	9443	9687	9932	.176
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179	2853	3096	3338	3580	3822	4064	4306	4548	4790	5031
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180	5273	5514	5755	5996	6237	6477	6718	6958	7198	7439
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182	230071	0310	0548	0787	1025	1263	1501	1739	1976	2214
183	2451	2688	2925	3162	3399	3636	3873	4109	4346	4582
184	4818	5054	5290	5525	5761	5996	6232	6467	6702	6937
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194	7802	8026	8249	8473	8696	8920	9143	9366	9589	9812
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197	4466	4687	4907	5127	5347	5567	5787	6007	6226	6446
198	6665	6884	7104	7323	7542	7761	7979	8198	8416	8635
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203	7496	7710	7924	8137	8351	8564	8778	8991	9204	9417
204	9530	9843	10156	10468	10781	11093	11406	11718	12030	12342
205	311754	1966	2177	2389	2600	2812	3023	3234	3445	3656
206	3867	4078	4289	4499	4710	4920	5130	5340	5551	5760
207	5970	6180	6390	6599	6809	7018	7227	7436	7646	7854
208	8063	8272	8481	8689	8898	9106	9314	9522	9730	9938
209	320146	0354	0562	0769	0977	1184	1391	1598	1805	2012
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221	4392	4589	4785	4981	5178	5374	5570	5766	5962	6157
222	6353	6549	6744	6939	7135	7330	7525	7720	7915	8110
223	8305	8500	8694	8889	9083	9278	9472	9666	9860	10054
224	350248	0442	0636	0829	1023	1216	1410	1603	1796	1989
225	2183	2375	2568	2761	2954	3147	3339	3532	3724	3916
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233	7356	7542	7729	7915	8101	8287	8473	8659	8845	9030
234	9216	9401	9587	9772	9958	10143	10328	10513	10698	10883
235	371068	1253	1437	1622	1806	1991	2175	2359	2544	2728
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238	6577	6759	6942	7124	7306	7488	7670	7852	8034	8216
239	8398	8580	8761	8943	9124	9306	9487	9668	9849	10030
240	38211	0392	0573	0754	0934	1115	1296	1476	1656	1837
241	2017	2197	2377	2557	2737	2917	3097	3277	3456	3636
242	3815	3995	4174	4353	4533	4712	4891	5070	5249	5428
243	5606	5785	5964	6142	6321	6499	6677	6856	7034	7212
244	7390	7568	7746	7923	8101	8279	8456	8634	8811	8989
245	9166	9343	9520	9698	9875	10051	10228	10405	10582	10759
246	390935	1112	1288	1464	1641	1817	1993	2169	2345	2521
247	2697	2873	3048	3224	3400	3575	3751	3926	4101	4277
248	4452	4627	4802	4977	5152	5326	5501	5676	5850	6025
249	6199	6374	6548	6722	6896	7071	7245	7419	7592	7766

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251	9674	9847	.20	.192	.365	.538	.711	.883	1056	1228
252	401491	15.3	1745	1917	2089	2261	2433	2605	2777	2949
253	3121	3292	3464	3635	3807	3978	4149	4320	4492	4663
254	4834	5005	5176	5346	5517	5688	5858	6029	6199	6370
					171					
255	6540	6710	6881	7051	7221	7391	7561	7731	7901	8070
256	8240	8410	8579	8749	8918	9087	9257	9426	9595	9764
257	9933	102	.271	.440	.609	.777	.946	1114	1283	1451
258	411620	1788	1956	2124	2293	2461	2629	2796	2964	3132
259	3300	3467	3635	3803	3970	4137	4305	4472	4639	4806
260	4973	5140	5307	5474	5641	5808	5974	6141	6308	6474
261	6641	6807	6973	7139	.305	.472	7638	7804	7970	8135
262	8301	.467	8633	8798	8964	.129	9295	9460	9625	9791
263	9956	.121	.286	.451	.616	.781	.945	1110	1275	1439
264	421604	1788	1933	2097	2261	2426	2590	2754	2918	3082
265	3246	3410	3574	3737	3901	4065	4228	4392	4555	4718
266	4882	5045	5208	5371	.534	.697	5860	6023	6186	6349
267	6511	6674	6836	6999	.161	7324	7486	7648	7811	7973
268	8135	8297	8459	8621	8783	8944	9106	9268	9429	9591
269	9752	9914	.175	.236	.398	.559	.720	.881	1042	1203
270	431364	1525	1685	1846	2007	2167	2328	2488	2649	2809
271	2969	3130	3290	3450	3610	3770	3930	4090	4249	4409
272	4569	4729	4888	5048	5207	5367	5526	5685	5844	6004
273	6163	6322	6481	6640	6800	6957	7116	7275	7433	7592
274	7751	7909	8067	8226	8384	8542	8701	8859	9017	9175
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275	9333	9491	9648	9806	9964	.122	.279	.437	.594	.752
276	440909	1066	1224	1381	1538	1695	1852	2009	2166	2323
277	2486	2637	2793	2950	3106	3263	3419	3576	3732	3889
278	4045	4201	4357	4513	4669	4825	4981	5137	5293	5449
279	5604	5760	5915	6071	6226	6382	6537	6692	6848	7003
280	7158	7313	7468	7623	7778	7933	8088	8242	8397	8552
281	8706	8861	9015	9170	9324	9478	9633	9787	9941	.95
282	450249	0403	0557	0711	0865	1018	1172	1326	1479	1633
283	1786	1940	2093	2247	2400	2553	2706	2859	3012	3165
284	3318	3471	3624	3777	3930	4082	4235	4387	4540	4692
285	4845	4997	5150	5302	5454	5606	5758	5910	6062	6214
286	6366	6518	6670	6821	6973	7125	7276	7428	7579	7731
287	7882	8033	8184	8335	8487	8638	8789	8940	9091	9242
288	9392	9543	9694	9845	9995	.146	.296	.447	.597	.748
289	460898	1048	1198	1348	1499	1649	1799	1948	2098	2248
290	2398	2548	2697	2847	2997	3146	3296	3445	3594	3744
291	3893	4042	4191	4340	4490	4639	4788	4936	5085	5234
292	5383	5532	5680	5829	5977	6126	6274	6423	6571	6719
293	6868	7016	7164	7312	7460	7608	7756	7904	8052	8200
294	8347	8495	8643	8790	8938	9085	9233	9380	9527	9675
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295	9822	9969	.116	.263	.410	.557	.704	.851	.998	1145
296	471292	1438	1585	1732	1878	2025	2171	2318	2464	2610
297	2756	2903	3049	3195	3341	3487	3633	3779	3925	4071
298	4216	4362	4508	4653	4799	4944	5090	5235	5381	5526
299	5671	5816	5962	6107	6252	6397	6542	6687	6832	6976



OF NUMBERS.

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300	477121	7266	7411	7555	7700	7844	7989	8133	8278	8422
301	8566	8711	8855	8999	9143	9287	9481	9575	9719	9863
302	480007	0151	0294	0138	0582	0725	0869	1012	1156	1299
303	1443	1585	1729	1872	2016	2159	2302	2445	2588	2731
304	2874	3016	3159	3302	3445	3587	3730	3872	4015	4157
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305	4300	4442	4585	4727	4869	5011	5153	5295	5437	5579
306	5721	5863	6005	6147	6289	6430	6572	6714	6855	6997
307	7138	7280	7421	7563	7704	7845	7986	8127	8269	8410
308	8551	8692	8833	8974	9114	9255	9396	9537	9677	9818
309	9959	.99	.239	.380	.520	.661	.801	.941	1081	1222
310	491362	1592	1642	1782	1922	2062	2201	2341	2481	2621
311	2769	2900	3040	3179	3319	3458	3597	3737	3876	4015
312	4155	4294	4433	4572	4711	4850	4989	5128	5267	5406
313	5544	5683	5822	5960	6099	6238	6376	6515	6653	6791
314	6930	7068	7206	7344	7483	7621	7759	7897	8035	8173
315	8311	8448	8586	8724	8862	8999	9137	9275	9412	9550
316	9687	9824	9962	.99	.236	.374	.511	.648	.785	.922
317	501059	1196	1333	1470	1607	1744	1880	2017	2154	2291
318	2427	2564	2700	2837	2973	3109	3246	3382	3518	3655
319	3791	3927	4063	4199	4335	4471	4607	4743	4878	5014
320	5150	5283	5421	5557	5693	5828	5964	6099	6234	6370
321	6505	6640	6775	6911	7045	7181	7316	7451	7585	7721
322	7856	7991	8125	8260	8395	8530	8664	8799	8934	9068
323	9203	9337	9471	9606	9740	9874	.99	.143	.277	.411
324	510545	0679	0813	0947	1081	1215	1349	1482	1616	1750
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325	1883	2017	2151	2284	2418	2551	2684	2818	2951	3084
326	3218	3351	3484	3617	3750	3883	4015	4149	4282	4414
327	4548	4681	4813	4946	5079	5211	5344	5476	5609	5741
328	5874	6005	6139	6271	6403	6535	6668	6800	6932	7064
329	7196	7328	7460	7592	7724	7855	7987	8119	8251	8382
330	8514	8646	8777	8909	9040	9171	9303	9434	9566	9697
331	9828	9959	.99	.221	.353	.484	.615	.745	.876	1007
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333	2444	2575	2705	2835	2966	3095	3226	3356	3486	3616
334	3746	3876	4006	4136	4266	4396	4526	4656	4785	4915
335	5045	5174	5304	5434	5563	5693	5822	5951	6081	6210
336	6339	6469	6598	6727	6856	6985	7114	7243	7372	7501
337	7630	7759	7888	8016	8145	8274	8402	8531	8660	8788
338	8917	9045	9174	9302	9430	9559	9687	9815	9943	.72
339	530200	0328	0456	0584	0712	0840	0968	1096	1223	1351
340	1479	1607	1734	1862	1960	2117	2245	2372	2500	2627
341	2754	2882	3009	3136	3264	3391	3518	3645	3772	3899
342	4026	4153	4280	4407	4534	4661	4787	4914	5041	5167
343	5294	5421	5547	5674	5800	5927	6053	6180	6306	6432
344	6558	6685	6811	6937	7063	7189	7315	7441	7567	7693
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345	7819	7945	8071	8197	8322	8448	8574	8699	8825	8951
346	9076	9202	9327	9452	9578	9703	9829	9954	.79	.204
347	540329	0455	0580	0705	0830	0955	1080	1205	1330	1454
348	1579	1704	1829	1953	2078	2203	2327	2452	2576	2701
349	2825	2950	3074	3199	3323	3447	3571	3696	3820	3944

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351	5307	5431	5555	5678	5805	5925	6049	6172	6296	6419
352	6543	6666	6789	6913	7036	7159	7282	7405	7529	7652
353	7775	7898	8021	8144	8267	8389	8512	8635	8758	8881
354	9003	9126	9249	9371	9494	9616	9739	9861	9984	.196
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355	550228	0351	0473	0595	0717	0840	0962	1084	1206	1328
356	1450	1572	1694	1816	1938	2060	2181	2303	2425	2547
357	2668	2790	2911	3033	3155	3276	3393	3519	3640	3762
358	3883	4004	4126	4247	4368	4489	4610	4731	4852	4973
359	5094	5215	5346	5457	5578	5699	5820	5940	6061	6182
360	6303	6423	6544	6664	6785	6905	7026	7146	7267	7387
361	7507	7627	7748	7868	7988	8108	8228	8349	8469	8589
362	8709	8829	8948	9068	9188	9308	9428	9548	9667	9787
363	9907	.26	.146	.265	.385	.504	.624	.743	.863	.982
364	561101	1:21	1340	1459	1578	1698	1817	1936	2055	2173
365	2293	2412	2531	2650	2769	2887	3006	3125	3244	3362
366	3481	3600	3718	3837	3955	4074	4192	4311	4429	4548
367	4666	4784	4903	5021	5139	5257	5376	5494	5612	5730
368	5848	5966	6084	6202	6320	6437	6555	6673	6791	6909
369	7026	7144	7262	7379	7497	7614	7732	7849	7967	8084
370	8202	8319	8436	8554	8671	8788	8905	9023	9140	9257
371	9374	9491	9608	9725	9842	9959	.76	.193	.309	.426
372	570543	0660	0776	0893	1010	1126	1243	1359	1476	1592
373	1709	1825	1942	2058	2174	2291	2407	2522	2639	2755
374	2872	2988	3104	3220	3336	3452	3568	3684	3800	3915
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375	4031	4147	4263	4379	4494	4610	4726	4841	4957	5072
376	5188	5303	5419	5534	5650	5765	5880	5996	6111	6226
377	6311	6457	6572	6687	6802	6917	7032	7147	7262	7377
378	7492	7607	7722	7836	7951	8066	8181	8295	8410	8525
379	8639	8754	8868	8983	9097	9212	9326	9441	9555	9669
380	9784	9898	.12	.126	.241	.355	.469	.583	.697	.811
381	580925	1039	1153	1267	1381	1495	1608	1722	1836	1950
382	2063	2177	2291	2404	2518	2631	2745	2858	2972	3085
383	3199	3312	3426	3539	3652	3765	3879	3992	4105	4218
384	4331	4444	4557	4670	4783	4896	5009	5122	5235	5348
385	5431	5574	5686	5799	5912	6024	6137	6250	6362	6475
386	6587	6700	6812	6925	7037	7149	7262	7374	7486	7599
387	7711	7823	7935	8047	8160	8272	8384	8496	8608	8720
388	8832	8944	9056	9167	9279	9391	9503	9615	9726	9834
389	9950	.61	.173	.284	.396	.507	.619	.730	.842	.953
390	591065	1176	1287	1399	1510	1621	1732	1843	1955	2066
391	2177	2288	2399	2510	2621	2732	2843	2954	3064	3175
392	3286	3397	3508	3618	3729	3840	3950	4061	4171	4282
393	4393	4503	4614	4724	4834	4945	5055	5165	5276	5386
394	5496	5606	5717	5827	5937	6047	6157	6267	6377	6487
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395	6597	6707	6817	6927	7037	7146	7256	7366	7476	7586
396	7695	7805	7914	8024	8134	8243	8353	8462	8572	8681
397	8791	8900	9009	9119	9228	9337	9446	9556	9666	9774
398	9883	9992	.101	.210	.319	.428	.537	.646	.755	.864
399	600973	1082	1191	1299	1408	1517	1625	1734	1843	1951

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402	4226	4334	4442	4550	4658	4766	4874	4982	5089	5197
403	5305	5413	5521	5628	5736	5844	5951	6059	6166	6274
404	6381	6489	6596	6704	6811	6919	7026	7133	7241	7348
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405	7455	7562	7669	7777	7884	7991	8098	8205	8312	8419
406	8526	8633	8740	8847	8954	9061	9167	9274	9381	9488
407	9594	9701	9808	9914	. 21	. 128	. 234	. 341	. 447	. 554
408	610360	0767	0873	0979	1086	1192	1298	1405	1511	1617
409	1723	1829	1936	2042	2148	2254	2360	2466	2572	2678
410	2784	2890	2996	3102	3207	3313	3419	3525	3630	3736
411	3842	3947	4053	4159	4264	4370	4475	4581	4686	4792
412	4897	5003	5108	5213	5319	5424	5529	5634	5740	5845
413	5950	6055	6160	6265	6370	6476	6581	6686	6790	6895
414	7000	7105	7210	7315	7420	7525	7629	7734	7839	7943
415	8048	8153	8257	8362	8466	8571	8676	8780	8884	8989
416	9293	9198	9302	9406	9511	9615	9719	9824	9928	. 32
417	620136	0240	0344	0448	0552	0656	0760	0864	0968	1072
418	1176	1280	1384	1488	1592	1695	1799	1903	2007	2110
419	2214	2318	2421	2525	2628	2732	2835	2939	3042	3145
420	3249	3353	3456	3559	3663	3766	3869	3973	4076	4179
421	4282	4385	4488	4591	4695	4798	4901	5004	5107	5210
422	5312	5415	5518	5621	5724	5827	5929	6032	6135	6238
423	6340	6443	6546	6648	6751	6853	6956	7058	7161	7263
424	7366	7468	7571	7673	7775	7878	7980	8082	8185	8287
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426	9410	9512	9613	9715	9817	9919	. 21	. 123	. 224	. 326
427	630428	0530	0631	0733	0835	0936	1038	1139	1241	1342
428	1444	1545	1647	1748	1849	1951	2052	2153	2255	2356
429	2457	2559	2660	2761	2862	2963	3064	3165	3266	3367
430	3468	3569	3670	3771	3872	3973	4074	4175	4276	4376
431	4477	4578	4679	4779	4880	4981	5081	5182	5283	5383
432	5484	5584	5685	5785	5886	5986	6087	6187	6287	6388
433	6488	6588	6688	6789	6889	6989	7089	7189	7290	7390
434	7490	7590	7690	7790	7890	7990	8090	8190	8290	8389
435	8489	8589	8689	8789	8888	8988	9088	9188	9287	9387
436	9486	9586	9686	9785	9885	9984	. 84	. 183	. 283	. 382
437	640481	0581	0680	0779	0879	0978	1077	1177	1276	1375
438	1474	1573	1672	1771	1871	1970	2069	2168	2267	2366
439	2465	2563	2662	2761	2860	2959	3058	3156	3255	3354
440	3453	3551	3650	3749	3847	3946	4044	4143	4242	4340
441	4439	4537	4636	4734	4832	4931	5029	5127	5226	5324
442	5422	5521	5619	5717	5815	5913	6011	6110	6208	6306
443	6404	6502	6600	6698	6796	6894	6992	7089	7187	7285
444	7383	7481	7579	7676	7774	7872	7969	8067	8165	8262
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445	8360	8458	8555	8653	8750	8848	8945	9043	9140	9237
446	9335	9432	9530	9627	9724	9821	9919	. 16	. 113	. 210
447	650308	0405	0502	0599	0696	0793	0890	0987	1084	1181
448	1278	1375	1472	1569	1666	1762	1859	1955	2053	2150
449	2246	2343	2440	2537	2633	2730	2826	2923	3019	3116

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452	5138	5235	5331	5427	5526	5619	5715	5810	5906	6002
453	6098	6194	6290	6386	6482	6577	6673	6769	6864	6960
454	7055	7152	7247	7343	7438	7534	7629	7725	7820	7916
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455	8011	8107	8202	8298	8393	8488	8584	8679	8774	8870
456	8965	9060	9155	9250	9346	9441	9536	9631	9726	9821
457	9916	.11	.106	.201	.296	.391	.486	.581	.676	.771
458	660865	0960	1055	1150	1245	1339	1434	1529	1623	1718
459	1813	1907	2002	2096	2191	2286	2380	2475	2569	2663
460	2758	2852	2947	3041	3135	3230	3324	3418	3512	3607
461	3701	3795	3889	3983	4078	4172	4266	4360	4454	4548
462	4642	4736	4830	4924	5018	5112	5206	5299	5393	5487
463	5581	5675	5769	5862	5956	6050	6143	6237	6331	6424
464	6518	6612	6705	6799	6892	6986	7079	7173	7266	7360
465	7453	7546	7640	7733	7826	7920	8013	8106	8199	8293
466	8386	8479	8572	8665	8759	8852	8945	9038	9131	9224
467	9317	9410	9503	9596	9689	9782	9875	9967	.60	.153
468	6.0241	0339	0431	0524	0617	0710	0802	0895	0988	1080
469	1173	1265	1358	1451	1543	1636	1728	1821	1913	2005
470	2098	2190	2283	2375	2467	2560	2652	2744	2836	2929
471	3021	3113	3205	3297	3390	3482	3574	3666	3758	3850
472	3942	4034	4126	4218	4310	4402	4494	4586	4677	4769
473	4861	4953	5045	5137	5228	5320	5412	5503	5595	5687
474	5778	5870	5962	6053	6145	6236	6328	6419	6511	6602
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475	6694	6785	6876	6968	7059	7151	7242	7333	7424	7516
476	7607	7698	7789	7881	7972	8063	8154	8245	8336	8427
477	8518	8609	8700	8791	8882	8972	9064	9155	9246	9337
478	9428	9519	9610	9700	9791	9882	9973	.63	.154	.245
479	680336	0426	0517	0607	0698	0789	0879	0970	1060	1151
480	1241	1332	1422	1513	1603	1693	1784	1874	1964	2055
481	2145	2235	2326	2416	2506	2596	2686	2777	2867	2957
482	3047	3137	3227	3317	3407	3497	3587	3677	3767	3857
483	3947	4037	4127	4217	4307	4396	4486	4576	4666	4756
484	4854	4935	5025	5114	5204	5294	5383	5473	5563	5652
485	5742	5831	5921	6010	6100	6189	6279	6368	6458	6547
486	6636	6726	6815	6904	6994	7083	7172	7261	7351	7440
487	7529	7618	7707	7796	7886	7975	8064	8153	8242	8331
488	8420	8509	8598	8687	8776	8865	8953	9042	9131	9220
489	9309	9398	9486	9575	9664	9753	9841	9930	.19	.107
490	690196	0285	0373	0462	0550	0639	0728	0816	0905	0993
491	1081	1170	1258	1347	1435	1524	1612	1700	1789	1877
492	1.65	2053	2142	2230	2318	2406	2494	2583	2671	2759
493	2847	2935	3023	3111	3199	3287	3375	3463	3551	3639
494	3727	3815	3903	3991	4078	4166	4254	4342	4430	4517
					88					
495	4605	4693	4781	4868	4956	5044	5131	5219	5307	5394
496	5482	5569	5657	5744	5832	5919	6007	6094	6182	6269
497	6356	6444	6531	6618	6706	6793	6880	6968	7055	7142
498	7229	7317	7404	7491	7578	7665	7752	7839	7926	8014
499	8104	8188	8275	8362	8449	8535	8622	8709	8796	8883

OF NUMBERS.

11

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502	707704	0790	0877	0963	1050	1136	1222	1309	1395	1482
503	1568	1654	1741	1827	1913	1999	2086	2172	2258	2344
504	2431	2517	2603	2689	2775	2861	2947	3033	3119	3205
					86					
505	3291	3377	3463	3549	3635	3721	3807	3895	3979	4065
506	4151	4236	4322	4408	4494	4579	4665	4751	4837	4922
507	5008	5094	5179	5265	5350	5436	5522	5607	5693	5778
508	5864	5949	6035	6120	6206	6291	6376	6462	6547	6632
509	6718	6803	6888	6974	7059	7144	7229	7315	7400	7485
510	7570	7655	7740	7826	7910	7996	8081	8166	8251	8336
511	8421	8506	8591	8676	8761	8846	8931	9015	9100	9185
512	9270	9355	9440	9524	9609	9694	9779	9863	9948	. 33
513	710117	0202	0287	0371	0456	0540	0625	0710	0794	0879
514	0963	1048	1132	1217	1301	1385	1470	1554	1639	1723
515	1807	1892	1976	2060	2144	2229	2313	2397	2481	2566
516	2650	2734	2818	2902	2986	3070	3154	3238	3322	3407
517	3491	3575	3659	3742	3826	3910	3994	4078	4162	4246
518	4330	4414	4497	4581	4665	4749	4833	4916	5000	5084
519	5167	5251	5335	5418	5502	5586	5669	5753	5836	5920
520	6003	6087	6170	6254	6337	6421	6504	6588	6671	6754
521	6838	6921	7004	7088	7171	7254	7338	7421	7504	7587
522	7671	7754	7837	7920	8003	8086	8169	8253	8336	8419
523	8502	8585	8668	8751	8834	8917	9000	9083	9165	9248
524	9331	9414	9497	9580	9663	9745	9828	9911	9994	. .77
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525	720159	0242	0325	0407	0490	0573	0655	0738	0821	0903
526	0986	1068	1151	1233	1316	1398	1481	1563	1646	1728
527	1811	1893	.975	2058	2140	2222	2305	2387	2469	2552
528	2634	2716	2798	2881	2963	3045	3127	3209	3291	3374
529	3456	3538	3620	3702	3784	3866	3948	4030	4112	4194
530	4276	4358	4440	4522	4604	4685	4767	4849	4931	5013
531	5095	5176	5258	5340	5422	5503	5585	5667	5748	5830
532	5912	5993	6075	6156	6238	6320	6401	6483	6564	6646
533	6727	6809	6890	6972	7053	7134	7216	7297	7379	7460
534	7541	7623	7704	7785	7866	7948	8029	8110	8191	8273
535	8354	8435	8516	8597	8678	8759	8841	8922	9003	9084
536	9165	9246	9327	9408	9489	9570	9651	9732	9813	9895
537	9974	. .55	.136	.217	.298	.378	.459	.540	.621	.702
538	730782	0863	0944	1024	1105	1186	1266	1347	1428	1508
539	1589	1669	1750	1830	1911	1991	2072	2152	2233	2313
540	2394	2474	2555	2635	2715	2796	2876	2956	3037	3117
541	3197	3278	3358	3438	3518	3598	3679	3759	3839	3919
542	3999	4079	4160	4240	4320	4400	4480	4560	4640	4720
543	4800	4880	4960	5040	5120	5200	5279	5359	5439	5519
544	5599	5679	5759	5838	5918	5998	6078	6157	6237	6317
					80					
545	6397	6476	6556	6636	6715	6795	6874	6954	7034	7113
546	7193	7272	7352	7431	7511	7590	7670	7749	7829	7908
547	7987	8067	8146	8225	8305	8384	8463	8543	8622	8701
548	8781	8860	8939	9018	9097	9177	9256	9335	9414	9492
549	9572	9651	9731	9810	9889	9968	. .47	.126	.205	.284

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550	740363	0442	0521	0560	0678	0757	0836	0915	0994	1073
551	1152	1230	1309	1388	1467	1546	1624	1703	1782	1860
552	1939	2018	2096	2175	2254	2332	2411	2489	2568	2646
553	2725	2804	2882	2961	3039	3118	3196	3275	3353	3431
554	3510	3558	3667	3745	3823	3902	3980	4058	4136	4215
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555	4293	4371	4449	4528	4606	4684	4762	4840	4919	4997
556	5075	5153	5231	5309	5387	5465	5543	5621	5699	5777
557	5855	5933	6011	6089	6167	6245	6323	6401	6479	6556
558	6634	6712	6790	6868	6945	7023	7101	7179	7256	7334
559	7412	7489	7567	7645	7722	7800	7878	7955	8033	8110
560	8188	8266	8343	8421	8498	8576	8653	8731	8808	8885
561	8563	9040	9118	9195	9272	9350	9427	9504	9582	9659
562	9736	9814	9891	9968	.45	.123	.200	.277	.354	.431
563	750608	0586	0663	0740	0817	0894	0971	1048	1125	1202
564	1279	1356	1433	1510	1587	1664	1741	1818	1895	1972
565	2048	2125	2202	2279	2356	2433	2509	2586	2663	2740
566	2816	2893	2970	3047	3123	3200	3277	3353	3430	3506
567	3582	3660	3736	3813	3889	3966	4042	4119	4195	4272
568	4348	4425	4501	4578	4654	4730	4807	4883	4960	5036
569	5112	5189	5265	5341	5417	5494	5570	5646	5722	5799
570	5875	5951	6027	6103	6180	6256	6332	6408	6484	6560
571	6636	6712	6788	6864	6940	7016	7092	7168	7244	7320
572	7396	7472	7548	7624	7700	7775	7851	7927	8003	8079
573	8155	8230	8306	8382	8458	8533	8609	8685	8761	8836
574	8912	8988	9068	9139	9214	9290	9366	9441	9517	9592
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575	9658	9743	9819	9894	9970	.45	.121	.196	.272	.347
576	760422	0498	0573	0649	0724	0799	0875	0950	1025	1101
577	1176	1251	1326	1402	1477	1552	1627	1702	1778	1853
578	1928	2003	2078	2153	2228	2303	2378	2453	2529	2604
579	2679	2754	2829	2904	2978	3053	3128	3203	3278	3353
580	3428	3503	3578	3653	3727	3802	3877	3952	4027	4101
581	4176	4251	4326	4400	4475	4550	4624	4699	4774	4848
582	4923	4998	5072	5147	5221	5296	5370	5445	5520	5594
583	5669	5743	5818	5892	5966	6041	6115	6190	6264	6338
584	6413	6487	6562	6636	6710	6785	6859	6933	7007	7082
585	7156	7230	7304	7379	7453	7527	7601	7675	7749	7823
586	7898	7972	8046	8120	8194	8268	8342	8416	8490	8564
587	8638	8712	8786	8860	8934	9008	9082	9156	9230	9303
588	9377	9451	9525	9599	9673	9746	9820	9894	9968	.42
589	770115	0189	0263	0336	0410	0484	0557	0631	0705	0778
590	0852	0926	0999	1073	1146	1220	1293	1367	1440	1514
591	1587	1661	1734	1808	1881	1955	2028	2102	2175	2248
592	2322	2395	2468	2542	2615	2688	2762	2835	2908	2981
593	3055	3128	3201	3274	3348	3421	3494	3567	3640	3713
594	3786	3860	3933	4006	4079	4152	4225	4298	4371	4444
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595	4517	4590	4663	4736	4809	4882	4955	5028	5100	5173
596	5246	5319	5392	5465	5538	5610	5683	5756	5829	5902
597	5974	6047	6120	6193	6265	6338	6411	6483	6556	6629
598	6701	6774	6846	6919	6992	7064	7137	7209	7282	7354
599	7427	7499	7572	7644	7717	7789	7862	7934	8006	8079

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600	778151	8224	8296	8368	8441	8513	8585	8658	8730	8802
601	8874	8947	9019	9091	9163	9236	9308	9380	9452	9524
602	9536	6669	9741	9813	9885	9957	.29	.101	.173	.245
603	780317	0389	0461	0533	0505	0677	0749	0821	0893	0965
604	1037	1109	1181	1253	1324	1396	1468	1540	1612	1684
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605	1755	1827	1899	1971	2042	2114	2186	2258	2329	2401
606	2473	2544	2616	2688	2759	2831	2902	2974	3046	3117
607	3189	3260	3332	3403	3475	3546	3618	3689	3761	3832
608	3904	3975	4046	4118	4189	4261	4332	4403	4475	4546
609	4617	4689	4760	4831	4902	4974	5045	5116	5187	5259
610	5330	5401	5472	5543	5615	5686	5757	5828	5899	5970
611	6041	6112	6183	6254	6325	6396	6467	6538	6609	6680
612	6751	6822	6893	6964	7035	7106	7177	7248	7319	7390
613	7460	7531	7602	7673	7744	7815	7885	7956	8027	8098
614	8168	8239	8310	8381	8451	8522	8593	8663	8734	8804
615	8275	8946	9016	9087	9157	9228	9299	9369	9440	9510
616	9581	9651	9722	9792	9863	9933	.4	.74	.144	.215
617	790285	0356	0426	0496	0567	0637	0707	0778	0848	0918
618	0988	1059	1129	1199	1269	1340	1410	1480	1550	1620
619	1691	1761	1831	1901	1971	2041	2111	2181	2252	2322
620	2392	2462	2532	2602	2672	2742	2812	2882	2952	3022
621	3092	3162	3231	3301	3371	3441	3511	3581	3651	3721
622	3790	3860	3930	4000	4070	4139	4209	4279	4349	4418
623	4488	4558	4627	4697	4767	4836	4906	4976	5045	5115
624	5185	5254	5324	5393	5463	5532	5602	5672	5741	5811
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625	5880	5949	6019	6088	6158	6227	6297	6366	6436	6505
626	6574	6644	6713	6782	6852	6921	6990	7060	7129	7198
627	7268	7337	7406	7475	7545	7614	7683	7752	7821	7890
628	7960	8029	8098	8167	8236	8305	8374	8443	8513	8582
629	8651	8720	8789	8858	8927	8996	9065	6134	9203	9272
630	9341	9409	9478	9547	9610	9685	9754	9823	9892	9961
631	800026	0098	0167	0236	0305	0373	0442	0511	0580	0648
632	0717	0786	0854	0923	0992	1061	1129	1198	1266	1335
633	1404	1472	1541	1609	1678	1747	1815	1884	1952	2021
634	2089	2158	2226	2295	2363	2432	2500	2568	2637	2705
635	2774	2842	2910	2979	3047	3116	3184	3252	3321	3389
636	3457	3525	3594	3662	3730	3798	3867	3935	4003	4071
637	4139	4208	4276	4344	4412	4480	4548	4616	4685	4753
638	4821	4889	4957	5025	5093	5161	5229	5297	5365	5433
639	5501	5569	5637	5705	5773	5841	5908	5976	6044	6112
640	6180	6248	6316	6384	6451	6519	6587	6655	6723	6790
641	6858	6926	6994	7061	7129	7197	7264	7332	7400	7467
642	7535	7603	7670	7738	7805	7873	7941	8008	8076	8143
643	8211	8279	8346	8414	8481	8549	8616	8684	8751	8818
644	8886	8953	9021	9088	9156	9223	9290	9358	9425	9492
645	9560	9627	9694	9762	9829	9896	9964	.31	.98	.165
646	810233	0300	0367	0434	0501	0569	0636	0703	0770	0837
647	0904	0971	1039	1106	1173	1240	1307	1374	1441	1508
648	1575	1642	1709	1776	1843	1910	1977	2044	2111	2178
649	2245	2312	2379	2445	2512	2579	2646	2713	2780	2847

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650	812913	2980	3047	3114	3181	3247	3314	3381	3448	3514
651	3581	3648	3714	3781	3848	3914	3981	4048	4114	4181
652	4248	4314	4381	4447	4514	4581	4647	4714	4780	4847
653	4913	4980	5046	5113	5179	5246	5312	5378	5445	5511
654	5578	5644	5711	5777	5843	5910	5976	6042	6109	6175
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655	6241	6308	6374	6440	6506	6573	6639	6705	6771	6838
656	6904	6970	7036	7102	7169	7233	7301	7367	7433	7499
657	7565	7631	7698	7764	7830	7896	7962	8028	8094	8160
658	8226	8292	8358	8424	8490	8556	8622	8688	8754	8820
659	8885	8951	9017	9083	9149	9215	9281	9346	9412	9478
660	9544	9610	9676	9741	9807	9873	9939	...4	..70	.136
661	820201	0267	0333	0399	0464	0530	0595	0661	0727	0792
662	0858	0924	0989	1055	1120	1186	1251	1317	1382	1448
663	1514	1579	1645	1710	1775	1841	1906	1972	2037	2103
664	2168	2233	2299	2364	2430	2495	2560	2626	2691	2756
665	2822	2887	2952	3018	3083	3148	3213	3279	3344	3409
666	3474	3539	3605	3670	3735	3800	3865	3930	3996	4061
667	4126	4191	4256	4321	4386	4451	4516	4581	4646	4711
668	4776	4841	4906	4971	5036	5101	5166	5231	5296	5361
669	5426	5491	5556	5621	5686	5751	5815	5880	5945	6010
670	6075	6140	6204	6269	6334	6399	6464	6528	6593	6658
671	6723	6787	6852	6917	6981	7046	7111	7175	7240	7305
672	7369	7434	7499	7563	7628	7692	7757	7821	7886	7951
673	8015	8080	8144	8209	8273	8338	8402	8467	8531	8595
674	8660	8724	8789	8853	8918	8982	9046	9111	9175	9239
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675	9304	9368	9432	9497	9561	9625	9690	9754	9818	9882
676	9947	..11	..75	.139	.204	.268	.332	.396	.460	.525
677	830589	0653	0717	0781	0845	0909	0973	1037	1102	1166
678	1230	1294	1358	1422	1486	1550	1614	1678	1742	1806
679	1870	1934	1998	2062	2126	2189	2253	2317	2381	2445
680	2509	2573	2637	2700	2764	2828	2892	2956	3020	3083
681	3147	3211	3275	3338	3402	3466	3530	3593	3657	3721
682	3784	3848	3912	3975	4039	4103	4166	4230	4294	4357
683	4421	4484	4548	4611	4675	4739	4802	4866	4929	4993
684	5056	5120	5183	5247	5310	5373	5437	5500	5564	5627
685	5691	5754	5817	5881	5944	6007	6071	6134	6197	6261
686	6324	6387	6451	6514	6577	6641	6704	6767	6830	6894
687	6957	7020	7083	7146	7210	7273	7336	7399	7462	7525
688	7588	7652	7715	7778	7841	7904	7967	8030	8093	8156
689	8219	8282	8345	8408	8471	8534	8597	8660	8723	8786
690	8849	8912	8975	9038	9101	9164	9227	9289	9352	9415
691	9478	9541	9604	9667	9729	9792	9855	9918	9981	..43
692	840105	0169	0232	0294	0357	0420	0482	0545	0608	0671
693	0733	0796	0859	0921	0984	1046	1109	1172	1234	1297
694	1359	1422	1485	1547	1610	1672	1735	1797	1860	1922
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695	1985	2047	2110	2172	2235	2297	2360	2422	2484	2547
696	2609	2672	2734	2796	2859	2921	2983	3046	3108	3170
697	3233	3295	3357	3420	3482	3544	3606	3669	3731	3793
698	3855	3918	3980	4042	4104	4166	4229	4291	4353	4415
699	4477	4539	4601	4664	4726	4788	4850	4912	4974	5036



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702	6337	6399	6461	6523	6585	6646	6708	6770	6832	6894
703	6955	7017	7079	7141	7202	7264	7326	7388	7449	7511
704	7573	7634	7676	7758	7819	7831	7943	8004	8066	8128
					62					
705	8189	8251	8312	8374	8435	8497	8559	8620	8682	8743
706	8805	8866	8928	8989	9051	9112	9174	9235	9297	9358
707	9419	9481	9542	9604	9665	9726	9788	9849	9911	9972
708	850033	0035	0156	0217	0279	0340	0401	0462	0524	0585
709	0646	0707	0769	0830	0891	0952	1014	1075	1136	1197
710	1258	1320	1381	1442	1503	1564	1625	1686	1747	1809
711	1870	1931	1992	2053	2114	2175	2236	2297	2358	2419
712	2480	2541	2602	2663	2724	2785	2846	2907	2968	3029
713	3090	3150	3211	3272	3333	3394	3455	3516	3577	3637
714	3698	3759	3820	3881	3941	4002	4063	4124	4185	4245
715	4306	4367	4428	4488	4549	4610	4670	4731	4792	4852
716	4913	4974	5034	5095	5156	5216	5277	5337	5398	5459
717	5519	5580	5640	5701	5761	5822	5882	5943	6003	6064
718	6124	6185	6245	6306	6366	6427	6487	6548	6608	6668
719	6729	6789	6850	6910	6970	7031	7091	7152	7212	7272
720	7332	7393	7453	7513	7574	7634	7694	7755	7815	7875
721	7935	7995	8056	8116	8176	8236	8297	8357	8417	8477
722	8537	8597	8657	8718	8778	8838	8898	8958	9018	9078
723	9138	9198	9258	9318	9379	9439	9499	9559	9619	9679
724	9739	9799	9859	9918	9978	.38	.98	.158	.218	.278
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725	860338	0398	0458	0518	0578	0637	0697	0757	0817	0877
726	0937	0996	1056	1116	1176	1236	1295	1355	1415	1475
727	1534	1594	1654	1714	1773	1833	1893	1952	2012	2072
728	2131	2191	2251	2310	2370	2430	2489	2549	2608	2668
729	2728	2787	2847	2906	2966	3025	3085	3144	3204	3263
730	3323	3382	3442	3501	3561	3620	3680	3739	3799	3858
731	3917	3977	4036	4096	4155	4214	4274	4333	4392	4452
732	4511	4570	4630	4689	4748	4808	4867	4926	4985	5045
733	5104	5163	5222	5282	5341	5400	5459	5519	5578	5637
734	5696	5755	5814	5874	5933	5992	6051	6110	6169	6228
735	6287	6346	6405	6465	6524	6583	6642	6701	6760	6819
736	6878	6937	6996	7055	7114	7173	7232	7291	7350	7409
737	7467	7526	7585	7644	7703	7762	7821	7880	7939	7998
738	8056	8115	8174	8233	8292	8350	8409	8468	8527	8586
739	8644	8703	8762	8821	8879	8938	8997	9056	9114	9173
740	9232	9290	9349	9408	9466	9525	9584	9642	9701	9760
741	9818	9877	9935	9994	.53	.111	.170	.228	.287	.345
742	870404	0462	0521	0579	0638	0696	0755	0813	0872	0930
743	0989	1047	1106	1164	1223	1281	1339	1398	1456	1515
744	1573	1631	1690	1748	1806	1865	1923	1981	2040	2098
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745	2156	2215	2273	2331	2389	2448	2506	2564	2622	2681
746	2739	2797	2855	2913	2972	3030	3088	3146	3204	3262
747	3321	3379	3437	3495	3553	3611	3669	3727	3785	3844
748	3902	3960	4018	4076	4134	4192	4250	4308	4366	4424
749	4482	4540	4598	4656	4714	4772	4830	4888	4945	5003

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750	875031	5119	5177	5235	5293	5351	5409	5466	5524	5582
751	5640	5598	5756	5813	5871	5929	5987	6045	6102	6160
752	6218	6276	6333	6391	6449	6507	6564	6622	6680	6737
753	6795	6853	6910	6968	7026	7083	7141	7199	7256	7314
754	7371	7429	7487	7544	7602	7659	7717	7774	7832	7889
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755	7947	8004	8062	8119	8177	8234	8292	8349	8407	8464
756	8522	8579	8637	8694	8752	8809	8866	8924	8981	9039
757	9096	9153	9211	9268	9325	9383	9440	9497	9555	9612
758	9369	9726	9784	9841	9898	9956	.13	.70	.127	.185
759	850242	0299	0356	0413	0471	0528	0580	0642	0699	0756
760	0814	0871	0928	0985	1042	1099	1156	1213	1271	1328
761	1385	1442	1499	1556	1613	1670	1727	1784	1841	1898
762	1955	2012	2069	2126	2183	2240	2297	2354	2411	2468
763	2525	2581	2638	2695	2752	2809	2866	2923	2980	3037
764	3093	3150	3207	3264	3321	3377	3434	3491	3548	3605
765	3661	3718	3775	3832	3888	3945	4002	4059	4115	4172
766	4229	4285	4342	4399	4455	4512	4569	4625	4682	4739
767	4795	4852	4909	4965	5022	5078	5135	5192	5248	5305
768	5361	5418	5474	5531	5587	5644	5700	5757	5813	5870
769	5926	5983	6039	6096	6152	6209	6265	6321	6378	6434
770	6491	6547	6604	6660	6716	6773	6829	6885	6942	6998
771	7054	7111	7167	7223	7280	7336	7392	7449	7505	7561
772	7617	7674	7730	7786	7842	7898	7955	8011	8067	8123
773	8179	8236	8292	8348	8404	8460	8516	8573	8629	8685
774	8741	8797	8853	8909	8965	9021	9077	9134	9190	9246
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775	9302	9358	9414	9470	9526	9582	9638	9694	9750	9806
776	9862	9918	0974	.30	.86	.141	.197	.253	.309	.365
777	890421	0477	0533	0589	0645	0700	0756	0812	0868	0924
778	0980	1035	1091	1147	1203	1259	1314	1370	1426	1482
779	1537	1593	1649	1705	1760	1816	1872	1928	1983	2039
780	2095	2150	2206	2262	2317	2373	2429	2484	2540	2595
781	2651	2707	2762	2818	2873	2929	2985	3040	3096	3151
782	3207	3262	3318	3373	3429	3484	3540	3595	3651	3706
783	3762	3817	3873	3928	3984	4039	4094	4150	4205	4261
784	4316	4371	4427	4482	4538	4593	4648	4704	4759	4814
785	4870	4925	4980	5036	5091	5146	5201	5257	5312	5367
786	5423	5478	5533	5588	5644	5699	5754	5809	5864	5920
787	5975	6030	6085	6140	6195	6251	6306	6361	6416	6471
788	6526	6581	6636	6692	6747	6802	6857	6912	6967	7022
789	7077	7132	7187	7242	7297	7352	7407	7462	7517	7572
790	7627	7683	7737	7792	7847	7902	7957	8012	8067	8122
791	8176	8231	8286	8341	8396	8451	8506	8561	8615	8670
792	8725	8780	8835	8890	8944	8999	9054	9109	9164	9218
793	9273	9328	9383	9437	9492	9547	9602	9656	9711	9766
794	9821	9875	9930	9985	.39	.94	.149	.203	.258	.312
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795	900367	0422	0476	0531	0586	0640	0695	0749	0804	0859
796	0913	0968	1022	1077	1131	1186	1240	1295	1349	1404
797	1458	1513	1567	1622	1676	1731	1785	1840	1894	1948
798	2003	2057	2112	2166	2221	2275	2329	2384	2438	2492
799	2547	2601	2655	2710	2764	2818	2873	2927	2981	3036

OF NUMBERS.

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800	90390	3144	3199	3253	3307	3361	3416	3470	3524	3578
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802	4174	4229	4283	4337	4391	4445	4499	4553	4607	4661
803	4716	4770	4824	4878	4932	4986	5040	5094	5148	5202
804	5256	5310	5364	5418	5472	5526	5580	5634	5688	5742
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805	5796	5850	5904	5958	6012	6066	6119	6173	6227	6281
806	6335	6389	6443	6497	6551	6604	6658	6712	6766	6820
807	6874	6927	6981	7035	7089	7143	7196	7250	7304	7358
808	7411	7465	7519	7573	7626	7680	7734	7787	7841	7895
809	7949	8002	8056	8110	8163	8217	8270	8324	8378	8431
810	8485	8539	8592	8646	8699	8753	8807	8860	8914	8967
811	9021	9074	9128	9181	9235	9289	9342	9396	9449	9503
812	9556	9610	9663	9716	9770	9823	9877	9930	9984	.37
813	910091	0144	0197	0251	0304	0358	0411	0464	0518	0571
814	0624	0678	0731	0784	0838	0891	0944	0998	1051	1104
815	1158	1211	1264	1317	1371	1424	1477	1530	1584	1637
816	1690	1743	1797	1850	1903	1956	2009	2063	2115	2169
817	2222	2275	2328	2381	2435	2488	2541	2594	2645	2700
818	2753	2805	2859	2913	2966	3019	3072	3125	3178	3231
819	3284	3337	3390	3443	3496	3549	3602	3655	3708	3761
820	3814	3867	3920	3973	4026	4079	4132	4184	4237	4290
821	4343	4396	4449	4502	4555	4608	4660	4713	4766	4819
822	4872	4925	4977	5030	5083	5136	5189	5241	5294	5347
823	5400	5453	5505	5558	5611	5664	5716	5769	5822	5875
824	5927	5980	6033	6085	6138	6191	6243	6296	6349	6401
825	6454	6507	6559	6612	6664	6717	6770	6822	6875	6927
826	6980	7033	7085	7138	7190	7243	7295	7348	7400	7453
827	7506	7558	7611	7663	7716	7768	7820	7873	7925	7978
828	8030	8083	8135	8188	8240	8293	8345	8397	8450	8502
829	8555	8607	8659	8712	8764	8816	8869	8921	8973	9026
830	9078	9130	9183	9235	9287	9340	9392	9444	9496	9549
831	9601	9653	9706	9758	9810	9862	9914	9967	.19	.71
832	920123	0176	0228	0280	0332	0384	0436	0489	0541	0593
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834	1166	1218	1270	1322	1374	1426	1478	1530	1582	1634
835	1686	1738	1790	1842	1894	1946	1998	2050	2102	2154
836	2206	2258	2310	2362	2414	2466	2518	2570	2622	2674
837	2725	2777	2829	2881	2933	2985	3037	3089	3141	3193
838	3244	3296	3348	3399	3451	3503	3555	3607	3658	3710
839	3762	3814	3865	3917	3969	4021	4072	4124	4175	4228
840	4279	4331	4383	4434	4486	4538	4589	4641	4693	4744
841	4796	4848	4899	4951	5003	5054	5106	5157	5209	5261
842	5312	5364	5415	5467	5518	5570	5621	5673	5725	5776
843	5828	5879	5931	5982	6034	6085	6137	6188	6240	6291
844	6342	6394	6445	6497	6548	6600	6651	6702	6754	6805
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845	6857	6908	6959	7011	7062	7114	7165	7216	7268	7319
846	7370	7422	7473	7524	7576	7627	7678	7730	7781	7832
847	7883	7935	7986	8037	8088	8140	8191	8242	8293	8345
848	8395	8447	8498	8549	8601	8652	8703	8754	8805	8857
849	8908	8959	9010	9061	9112	9163	9214	9266	9317	9368

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851	9930	9981	.32	.83	.134	.185	.236	.287	.338	.389
852	930440	0491	0542	0592	0543	0694	0745	0796	0847	0898
853	0949	1000	1051	1102	1153	1204	1254	1305	1356	1407
854	1458	1509	1560	1610	1661	1712	1763	1814	1865	1915
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855	1966	2017	2068	2118	2169	2220	2271	2322	2372	2423
856	2474	2524	2575	2626	2677	2727	2778	2829	2879	2930
857	2981	3031	3082	3133	3183	3234	3285	3335	3386	3437
858	3487	3538	3589	3639	3690	3740	3791	3841	3892	3943
859	3993	4044	4094	4145	4195	4246	4296	4347	4397	4448
860	4498	4549	4599	4650	4700	4751	4801	4852	4902	4953
861	5003	5054	5104	5154	5205	5255	5306	5356	5406	5457
862	5507	5558	5608	5658	5709	5759	5809	5860	5910	5960
863	6011	6061	6111	6162	6212	6262	6313	6363	6413	6463
864	6514	6564	6614	6665	6715	6765	6815	6865	6916	6966
865	7016	7066	7117	7167	7217	7267	7317	7367	7418	7468
866	7518	7568	7618	7668	7718	7769	7819	7869	7919	7969
867	8019	8069	8119	8169	8219	8269	8320	8370	8420	8470
868	8520	8570	8620	8670	8720	8770	8820	8870	8919	8970
869	9020	9070	9120	9170	9220	9270	9320	9369	9419	9469
870	9519	9569	9616	9669	9719	9769	9819	9869	9918	9968
871	940018	0088	0118	0168	0218	0267	0317	0367	0417	0467
872	0516	0566	0616	0666	0716	0765	0815	0865	0915	0964
873	1014	1064	1114	1163	1213	1263	1313	1362	1412	1462
874	1511	1561	1611	1660	1710	1760	1809	1859	1909	1958
875	2008	2058	2107	2157	2207	2256	2306	2355	2405	2455
876	2504	2554	2603	2653	2702	2752	2801	2851	2901	2950
877	3000	3049	3099	3148	3198	3247	3297	3346	3396	3445
878	3495	3544	3593	3643	3692	3742	3791	3841	3890	3939
879	3989	4038	4088	4137	4186	4236	4285	4335	4384	4433
880	4483	4532	4581	4631	4680	4729	4779	4828	4877	4927
881	4976	5025	5074	5124	5173	5222	5272	5321	5370	5419
882	5469	5518	5567	5616	5665	5715	5764	5813	5862	5912
883	5961	6010	6059	6108	6157	6207	6256	6305	6354	6403
884	6452	6501	6551	6600	6649	6698	6747	6796	6845	6894
885	6943	6992	7041	7090	7140	7189	7238	7287	7336	7385
886	7434	7483	7532	7581	7630	7679	7728	7777	7826	7875
887	7924	7973	8022	8070	8119	8168	8217	8266	8315	8365
888	8413	8462	8511	8560	8609	8657	8706	8755	8804	8853
889	8902	8951	8999	9048	9097	9146	9195	9244	9292	9341
890	9390	9439	9488	9536	9585	9634	9683	9731	9780	9829
891	9878	9926	9975	.24	.73	.121	.170	.219	.267	.316
892	950365	0414	0462	0511	0560	0608	0657	0705	0754	0803
893	0851	0900	0949	0997	1046	1095	1143	1192	1240	1289
894	1338	1386	1435	1483	1532	1580	1629	1677	1726	1775
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895	1823	1872	1920	1969	2017	2066	2114	2163	2211	2260
896	2308	2356	2405	2453	2502	2550	2599	2647	2696	2744
897	2792	2841	2889	2938	2986	3034	3083	3131	3180	3228
898	3276	3325	3373	3421	3470	3518	3566	3615	3663	3711
899	3760	3808	3856	3905	3953	4001	4049	4098	4146	4194

O F N U M B E R S .

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900	954243	4291	4339	4387	4435	4484	4532	4580	4628	4677
901	4725	4773	4821	4869	4918	4966	5014	5062	5110	5158
902	5207	5255	5303	5351	5399	5447	5495	5543	5592	5640
903	5688	5736	5784	5832	5880	5928	5976	6024	6072	6120
904	6168	6216	6265	6313	63.31	6409	6457	6505	6553	6601
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995	6649	6697	6745	6793	6840	6888	6936	6984	7032	7080
906	7128	7176	7224	7272	7320	7368	7416	7464	7512	7559
907	7607	7655	7703	7751	7799	7847	7894	7942	7990	8038
908	8086	8134	8181	8229	8277	8325	8373	8421	8468	8516
909	8564	8612	8659	8707	8755	8803	8850	8898	8946	8994
910	9011	9089	9137	9185	9232	9280	9328	9375	9423	9471
911	9518	9566	9614	9661	9709	9757	9804	9852	9900	9947
912	9905	.42	.90	.138	.185	.233	.280	.328	.376	.423
913	960471	0518	0566	0613	0661	0709	0756	0804	0851	0899
914	0946	0994	1041	1089	1136	1184	1231	1279	1326	1374
915	1421	1469	1516	1563	1611	1658	1706	1753	1801	1848
916	1895	1943	1990	2038	2085	2132	2180	2227	2275	2322
917	2369	2417	2464	2511	2559	2605	2653	2701	2748	2795
918	2843	2890	2937	2985	3032	3079	3126	3174	3221	3268
919	3316	3363	3410	3457	3504	3552	3599	3646	3693	3741
920	3788	3835	3882	3929	3977	4024	4071	4118	4165	4212
921	4260	4307	4354	4401	4448	4495	4542	4590	4637	4684
922	4731	4778	4825	4872	4919	4966	5013	5061	5108	5155
923	5202	5249	5296	5343	5390	5437	5484	5531	5578	5625
924	5672	5719	5766	5813	5860	5907	5954	6001	6048	6095
925	6142	6189	6236	6283	6329	6376	6423	6470	6517	6564
926	6611	6658	6705	6752	6799	6845	6892	6939	6986	7033
927	7080	7127	7173	7220	7267	7314	7361	7408	7454	7501
928	7548	7595	7642	7688	7735	7782	7829	7875	7922	7969
929	8016	8062	8109	8156	8203	8249	8296	8343	8390	8436
930	8483	8530	8576	8623	8670	8716	8763	8810	8856	8903
931	8950	8996	9043	9090	9136	9183	9229	9276	9323	9369
932	9416	9463	9509	9556	9602	9649	9695	9742	9789	9835
933	9882	9928	9975	.21	.68	.114	.161	.207	.254	.300
934	970347	0393	0440	0486	0533	0579	0626	0672	0719	0765
935	0812	0858	0904	0951	0997	1044	1090	1137	1183	1229
936	1276	1322	1369	1415	1461	1508	1554	1601	1647	1693
937	1740	1786	1832	1879	1925	1971	2018	2064	2110	2157
938	2203	2249	2295	2342	2388	2434	2481	2527	2573	2619
939	2666	2712	2758	2804	2851	2897	2943	2989	3035	3082
940	3128	3174	3220	3266	3313	3359	3405	3451	3497	3543
941	3590	3636	3682	3728	3774	3820	3866	3913	3959	4005
942	4051	4097	4143	4189	4235	4281	4327	4374	4420	4466
943	4512	4558	4604	4650	4696	4742	4788	4834	4880	4926
944	4972	5018	5064	5110	5156	5202	5248	5294	5340	5386
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945	5432	5478	5524	5570	5616	5662	5707	5753	5799	5845
946	5891	5937	5983	6029	6075	6121	6167	6212	6258	6304
947	6350	6396	6442	6488	6533	6579	6625	6671	6717	6763
948	6808	6854	6900	6946	6992	7037	7083	7129	7175	7220
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952	8637	8683	8728	8774	8819	8865	8911	8956	9002	9047
953	9093	9138	9184	9230	9275	9321	9366	9412	9457	9503
954	9548	9594	9639	9685	9730	9776	9821	9867	9912	9958
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955	980003	0049	0094	0140	0185	0231	0276	0322	0367	0412
956	0458	0503	0549	0594	0640	0685	0730	0776	0821	0867
957	0912	0957	1003	1048	1093	1139	1184	1229	1275	1320
958	1366	1411	1456	1501	1547	1592	1637	1683	1728	1773
959	1819	1864	1909	1954	2000	2045	2090	2135	2181	2226
960	2271	2316	2362	2407	2452	2497	2543	2588	2633	2678
961	2723	2769	2814	2859	2904	2949	2994	3040	3085	3130
962	3175	3220	3265	3310	3356	3401	3446	3491	3536	3581
963	3626	3671	3716	3762	3807	3852	3897	3942	3987	4032
964	4077	4122	4167	4212	4257	4302	4347	4392	4437	4482
965	4527	4572	4617	4662	4707	4752	4797	4842	4887	4932
966	4977	5022	5067	5112	5157	5202	5247	5292	5337	5382
967	5426	5471	5516	5561	5606	5651	5699	5741	5786	5830
968	5875	5920	5965	6010	6055	6100	6144	6189	6234	6279
969	6324	6369	6413	6458	6503	6548	6593	6637	6682	6727
970	6772	6817	6861	6906	6951	6996	7040	7085	7130	7175
971	7219	7264	7309	7353	7398	7443	7488	7532	7577	7622
972	7666	7711	7756	7800	7845	7890	7934	7979	8024	8068
973	8113	8157	8202	8247	8291	8336	8381	8425	8470	8514
974	8559	8604	8648	8693	8737	8782	8826	8871	8916	8960
975	9005	9049	9093	9138	9183	9227	9272	9316	9361	9405
976	9450	9494	9539	9583	9628	9672	9717	9761	9806	9850
977	9895	9939	9983	. .28	. .72	.117	.161	.205	.250	.294
978	990339	0383	0428	0472	0516	0561	0605	0650	0694	0738
979	0783	0827	0871	0916	0960	1004	1049	1093	1137	1182
980	1226	1270	1315	1359	1403	1448	1492	1536	1580	1625
981	1669	1713	1758	1802	1846	1890	1935	1979	2023	2067
982	2111	2156	2200	2244	2288	2333	2377	2421	2465	2509
983	2554	2598	2642	2686	2730	2774	2819	2863	2907	2951
984	2995	3039	3083	3127	3172	3216	3260	3304	3348	3392
985	3436	3480	3524	3568	3613	3657	3701	3745	3789	3833
986	3877	3921	3965	4009	4053	4097	4141	4185	4229	4273
987	4317	4361	4405	4449	4493	4537	4581	4625	4669	4713
988	4757	4801	4845	4889	4933	4977	5021	5065	5108	5152
989	5196	5240	5284	5328	5372	5416	5460	5504	5547	5591
990	5635	5679	5723	5767	5811	5854	5898	5942	5986	6030
991	6074	6117	6161	6205	6249	6293	6337	6380	6424	6468
992	6512	6555	6599	6643	6687	6731	6774	6818	6862	6906
993	6949	6993	7037	7080	7124	7168	7212	7255	7299	7343
994	7386	7430	7474	7517	7561	7605	7648	7692	7736	7779
					44					
995	7823	7867	7910	7954	7998	8041	8085	8129	8172	8216
996	8259	8303	8347	8390	8434	8477	8521	8564	8608	8652
997	8695	8739	8792	8826	8869	8913	8956	9000	9043	9087
998	9131	9174	9218	9261	9305	9348	9392	9435	9479	9522
999	9565	9609	9652	9696	9739	9783	9826	9870	9913	9957

TABLE II. Log. Sines and Tangents. (0°) Natural Sines.

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.
0	Neg. Infinite		10.000000		0.000000		Infinite.	00000	100000
1	0.463726		003000		6.463726		13.536274	00029	100000
2	764756		000000		764756		235244	00058	100000
3	940547		000000		940847		059153	00087	100000
4	7.035786		000000		7.065786		12.934214	00116	100000
5	162696		000000		162696		837304	00145	100000
6	241877		9.999999		241878		758122	00175	100000
7	308824		999999		308825		591175	00204	100000
8	366816		999999		366817		633183	00233	100000
9	417968		999999		417970		582030	00262	100000
10	463725		999998		463727		536273	00291	100000
11	7.505118		9.999998		7.505120		12.494880	90320	99999
12	542906		999997		542909		457091	00349	99999
13	577668		999997		577672		422328	00378	99999
14	609853		999996		609857		390143	00407	99999
15	639816		999996		639820		360180	00436	99999
16	667845		999995		667849		332151	00465	99999
17	694173		999995		694179		305821	00495	99999
18	718997		999994		719003		280997	00524	99999
19	742477		999993		742484		257516	00553	99998
20	764754		999993		764761		235239	00582	99998
21	7.785943		9.999992		7.785951		12.214049	00611	99998
22	806146		999991		806155		193845	00640	99998
23	825451		999990		825460		174540	00669	99998
24	843934		999989		843944		156056	00698	99998
25	861663		999988		861674		138326	00727	99997
26	878695		999988		878708		121292	00756	99997
27	895085		999987		895099		104901	00785	99997
28	910879		999986		910894		089106	00814	99997
29	926119		999985		926134		073866	00844	99996
30	940842		999983		940858		059142	00873	99996
31	7.955082		9.999982		7.955100		12.044900	00902	99996
32	968870	2298	999981	0.2	968889	2298	031111	00931	99996
33	982233	2227	999980	0.2	982253	2227	017747	00960	99995
34	995198	2161	999979	0.2	995219	2161	004781	00989	99995
35	8.007787	2098	999977	0.2	8.007809	2098	11.992191	01018	99995
36	020021	2039	999976	0.2	020045	2039	979955	01047	99995
37	031919	1983	999975	0.2	031945	1983	968055	01076	99994
38	043501	1930	999973	0.2	043527	1930	956473	01105	99994
39	054781	1880	999972	0.2	054809	1880	945191	01134	99994
40	065776	1832	999971	0.2	065806	1832	934194	01164	99993
41	8.076500	1787	9.999969	0.2	8.076531	1787	11.923469	01193	99993
42	086965	1744	999968	0.2	086997	1744	913003	01222	99993
43	097183	1703	999966	0.2	097217	1703	902783	01251	99992
44	107167	1664	999964	0.2	107202	1664	892797	01280	99992
45	116926	1626	999963	0.3	116963	1627	883037	01309	99991
46	126471	1591	999961	0.3	126510	1591	873490	01339	99991
47	135810	1557	999959	0.3	135851	1557	864149	01367	99991
48	144953	1524	999958	0.3	144996	1524	855004	01396	99990
49	153907	1492	999956	0.3	153952	1493	846048	01425	99990
50	162681	1462	999954	0.3	162727	1463	837273	01454	99989
51	8.171280	1433	9.999952	0.3	8.171328	1434	11.828672	01483	99989
52	179713	1405	999950	0.3	179763	1406	820237	01513	99989
53	187985	1379	999948	0.3	188036	1379	811964	01542	99988
54	196102	1353	999946	0.3	196156	1353	803844	01571	99988
55	204070	1328	999944	0.3	204126	1328	795874	01600	99987
56	211895	1304	999942	0.3	211953	1304	788047	01629	99987
57	219581	1281	999940	0.4	219641	1281	780359	01658	99986
58	227134	1259	999938	0.4	227195	1259	772805	01687	99986
59	234557	1237	999936	0.4	234621	1238	765379	01716	99985
60	241855	1216	999934	0.4	241921	1217	758079	01745	99985
	Cosine		Sine		Cotang		Tang.	N. cos.	N. sine

	Sine.	D 10'	Cosine.	D.10''	Tang.	D 10''	Cotang.	N. sine.	N. cos.
0	8.241855	1196	9.999934	0.4	8.241921	1197	11.758079	01742	99985 60
1	249033	1177	999932	0.4	249102	1177	750898	01774	99984 59
2	256034	1158	999929	0.4	253165	1158	743835	01803	99984 58
3	263042	1140	999927	0.4	263115	1140	736885	01832	99983 57
4	269881	1122	999925	0.4	269956	1122	730044	01862	99983 56
5	276314	1105	999922	0.4	276691	1105	723309	01891	99982 55
6	283243	1088	999920	0.4	283323	1089	716677	01920	99982 54
7	289773	1072	999918	0.4	289856	1073	710144	01949	99981 53
8	296207	1056	999915	0.4	296292	1057	703708	01978	99980 52
9	302543	1041	999913	0.4	302634	1042	697366	02007	99980 51
10	308794	1027	999910	0.4	308384	1027	691116	02036	99979 50
11	314954	1012	9.999907	0.4	315046	1013	11.684954	02065	99979 49
12	321027	998	999905	0.4	321122	999	678878	02094	99978 48
13	327016	985	999902	0.4	327114	999	672886	02123	99977 47
14	332924	971	999899	0.5	333025	985	666975	02152	99977 46
15	338753	959	999897	0.5	333856	959	661144	02181	99976 45
16	344504	946	999894	0.5	344610	946	655390	02211	99976 44
17	350181	934	999891	0.5	350289	934	649711	02240	99975 43
18	355783	922	999888	0.5	355895	922	644105	02269	99974 42
19	361315	910	999885	0.5	361430	911	638570	02298	99974 41
20	366777	899	999882	0.5	366895	899	633105	02327	99973 40
21	8.372171	888	9.999879	0.5	8.372292	888	11.627708	02356	99973 39
22	377499	877	999876	0.5	377622	879	622378	02385	99972 38
23	382762	867	999873	0.5	382889	867	617111	02414	99971 37
24	387962	856	999870	0.5	388092	857	611908	02443	99970 36
25	393101	846	999867	0.5	393234	847	606766	02472	99969 35
26	398179	837	999864	0.5	398315	837	601685	02501	99969 34
27	403199	827	999861	0.5	403338	828	596662	02530	99968 33
28	408161	818	999858	0.5	408304	818	591696	02559	99967 32
29	413068	809	999854	0.5	413213	809	586787	02589	99966 31
30	417919	800	999851	0.6	418068	800	581932	02618	99966 30
31	8.422717	791	9.999848	0.6	8.422869	791	11.577131	02647	99965 29
32	427462	782	999844	0.6	427618	783	572382	02676	99964 28
33	432156	774	999841	0.6	432315	774	567685	02705	99963 27
34	436800	766	999838	0.6	436962	766	563038	02734	99963 26
35	441394	758	999834	0.6	441560	758	558440	02763	99962 25
36	445941	750	999831	0.6	446110	750	553890	02792	99961 24
37	450440	742	999827	0.6	450613	743	549387	02821	99960 23
38	454893	735	999823	0.6	455070	735	544930	02850	99959 22
39	459301	727	999820	0.6	459481	728	540519	02879	99959 21
40	463665	720	999816	0.6	463849	720	536151	02908	99958 20
41	8.467985	712	9.999812	0.6	8.468172	713	11.531828	02938	99957 19
42	472263	706	999809	0.6	472454	707	527546	02967	99956 18
43	476498	699	999805	0.6	476693	700	523307	02996	99955 17
44	480693	692	999801	0.6	480892	693	519108	03025	99954 16
45	484848	686	999797	0.7	485050	686	514950	03054	99953 15
46	488963	679	999793	0.7	489170	680	510830	03083	99952 14
47	493040	673	999790	0.7	493250	674	506750	03112	99952 13
48	497078	667	999786	0.7	497293	668	502707	03141	99951 12
49	501080	661	999782	0.7	501298	661	498702	03170	99950 11
50	505045	655	999778	0.7	505267	655	494733	03199	99949 10
51	8.508974	649	9.99977	0.7	8.509200	650	11.490800	03228	99948 9
52	512867	643	999769	0.7	513098	644	486902	03257	99947 8
53	516726	637	999765	0.7	516961	638	483039	03286	99946 7
54	520551	632	999761	0.7	520799	633	479210	03316	99945 6
55	524343	626	999757	0.7	524586	627	475414	03345	99944 5
56	528102	621	999753	0.7	528349	622	471651	03374	99943 4
57	531828	616	999748	0.7	532080	616	467920	03403	99942 3
58	535523	611	999744	0.7	535779	611	464221	03432	99941 2
59	539186	605	999740	0.7	539447	606	460553	03461	99940 1
60	542819	605	999735	0.7	543084		456916	03490	99939 0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.



TABLE II. Log. Sines and Tangents. (2<sup>d</sup>) Natural Sines.

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	8.542819	600	9.999735		8.543084	602	11.456916	03490	99939	60
1	546422	595	999731	0.7	546691	595	453300	03519	99938	59
2	549935	591	999726	0.7	550268	591	449732	03548	99937	58
3	553539	586	999722	0.8	553817	587	446183	03577	99936	57
4	557054	581	999717	0.8	557335	582	442664	03606	99935	56
5	560540	576	999713	0.8	560828	577	439172	03635	99934	55
6	563999	572	999708	0.8	564291	573	435709	03664	99933	54
7	567431	567	999704	0.8	567727	568	432273	03693	99932	53
8	570836	563	999699	0.8	571137	564	428863	03723	99931	52
9	574214	559	999694	0.8	574520	559	425480	03752	99930	51
10	577566	554	999689	0.8	577877	555	422123	03781	99929	50
11	8.580892	550	9.999685	0.8	8.581208	551	11.418792	03810	99927	49
12	584193	546	999680	0.8	584514	547	415486	03839	99926	48
13	587469	542	999675	0.8	587795	543	412205	03868	99925	47
14	590721	538	999670	0.8	591051	539	408949	03897	99924	46
15	593948	534	999665	0.8	594283	535	405717	03926	99923	45
16	597152	530	999660	0.8	597492	531	402508	03955	99922	44
17	600332	526	999655	0.8	600677	527	399323	03984	99921	43
18	603489	522	999650	0.8	603839	523	396161	04013	99919	42
19	606623	519	999645	0.8	606978	523	393022	04042	99918	41
20	609734	515	999640	0.8	610094	519	389906	04071	99917	40
21	8.612823	511	9.999635	0.9	8.613189	512	11.386811	04100	99916	39
22	615891	508	999629	0.9	616262	508	383738	04129	99915	38
23	618937	504	999624	0.9	619313	505	380687	04159	99913	37
24	621962	501	999619	0.9	622343	501	377657	04188	99912	36
25	624965	497	999614	0.9	625352	498	374648	04217	99911	35
26	627948	494	999608	0.9	628340	495	371660	04246	99910	34
27	630911	490	999603	0.9	631308	491	368692	04275	99909	33
28	633854	487	999597	0.9	634256	488	365744	04304	99907	32
29	636776	484	999592	0.9	637184	485	362816	04333	99906	31
30	639680	481	999586	0.9	640093	482	359907	04362	99905	30
31	8.642563	477	9.999581	0.9	8.642982	478	11.357018	04391	99904	29
32	645428	474	999575	0.9	645853	475	354147	04420	99902	28
33	648274	471	999570	0.9	648704	472	351296	04449	99901	27
34	651102	468	999564	0.9	651537	469	348463	04478	99900	26
35	653911	465	999558	1.0	654352	466	345648	04507	99898	25
36	656702	462	999553	1.0	657149	463	342851	04536	99897	24
37	659475	459	999547	1.0	659928	460	340072	04565	99896	23
38	662230	456	999541	1.0	662689	457	337311	04594	99894	22
39	664968	453	999535	1.0	665433	454	334567	04623	99893	21
40	667689	451	999529	1.0	668160	453	331840	04653	99892	20
41	8.670393	448	9.999524	1.0	8.670870	449	11.329130	04682	99890	19
42	673080	445	999518	1.0	673563	446	326437	04711	99889	18
43	675751	442	999512	1.0	676239	443	323761	04740	99888	17
44	678405	440	999506	1.0	678900	442	321100	04769	99886	16
45	681043	437	999500	1.0	681544	438	318456	04798	99885	15
46	683665	434	999493	1.0	684172	435	315828	04827	99883	14
47	686272	432	999487	1.0	686784	433	313216	04856	99882	13
48	688863	429	999481	1.0	689381	430	310619	04885	99881	12
49	691438	427	999475	1.0	691963	428	308037	04914	99879	11
50	693998	424	999469	1.0	694529	425	305471	04943	99878	10
51	8.696543	422	9.999463	1.1	8.697081	423	11.302919	04972	99876	9
52	699073	419	999456	1.1	696617	420	303083	05001	99875	8
53	701589	417	999450	1.1	702139	418	297861	05030	99873	7
54	704090	414	999443	1.1	704246	415	295354	05059	99872	6
55	706577	412	999437	1.1	707140	413	292860	05088	99870	5
56	709049	410	999431	1.1	709618	411	290382	05117	99869	4
57	711507	407	999424	1.1	702083	408	287917	05146	99867	3
58	713952	405	999418	1.1	714534	406	285465	05175	99866	2
59	716383	405	999411	1.1	716972	404	283028	05205	99864	1
60	718800	403	999404	1.1	719395	404	280604	05234	99863	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N.sine.	P

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	8.718800	401	9.999404	1.1	5.719396	402	11.280604	05234	99863	60
1	721204	398	999398	1.1	721806	399	278194	05263	99861	59
2	723595	396	999391	1.1	724204	397	275796	05292	99860	58
3	725972	394	999384	1.1	726588	395	273412	05321	99858	57
4	728337	392	999378	1.1	728959	393	271041	05350	99857	56
5	730388	390	999371	1.1	731317	391	268683	05379	99855	55
6	733027	388	999364	1.1	733663	389	266337	05408	99854	54
7	735354	386	999357	1.2	735996	387	264004	05437	99852	53
8	737667	384	999350	1.2	738317	385	261683	05466	99851	52
9	739969	382	999343	1.2	740626	384	259374	05495	99849	51
10	742259	380	999336	1.2	742922	383	257078	05524	99847	50
11	8.744536	378	9.999329	1.2	8.745207	381	11.254793	05553	99846	49
12	746802	376	999322	1.2	747479	379	252521	05582	99844	48
13	749055	374	999315	1.2	749740	377	250260	05611	99842	47
14	751297	372	999308	1.2	751989	375	248011	05640	99841	46
15	753528	370	999301	1.2	754227	373	245773	05669	99839	45
16	755747	368	999294	1.2	756453	371	243547	05698	99838	44
17	757955	366	999286	1.2	758668	369	241332	05727	99836	43
18	760151	364	999279	1.2	760872	367	239128	05756	99834	42
19	762337	362	999272	1.2	763065	365	236935	05785	99833	41
20	764511	360	999265	1.2	765246	364	234754	05814	99831	40
21	8.766575	359	9.999257	1.2	8.767417	362	11.232583	05843	99829	39
22	768828	357	999250	1.2	769578	360	230422	05873	99827	38
23	770970	355	999242	1.3	771727	358	228273	05902	99826	37
24	773101	353	999235	1.3	773866	356	226134	05931	99824	36
25	775223	352	999227	1.3	775995	355	224005	05960	99822	35
26	777333	352	999220	1.3	778114	353	221886	05989	99821	34
27	779434	350	999212	1.3	780222	351	219778	06018	99819	33
28	781524	348	999205	1.3	782320	350	217680	06047	99817	32
29	783605	347	999197	1.3	784408	348	215592	06076	99815	31
30	785675	345	999189	1.3	786486	346	213514	06105	99813	30
31	8.787736	343	9.999181	1.3	8.788554	345	11.211446	06134	99812	29
32	789787	342	999174	1.3	790613	343	209387	06163	99810	28
33	791828	340	999166	1.3	792662	341	207338	06192	99808	27
34	793859	339	999158	1.3	794701	340	205299	06221	99806	26
35	795881	337	999150	1.3	796731	338	203269	06250	99804	25
36	797894	335	999142	1.3	798752	337	201248	06279	99803	24
37	799897	334	999134	1.3	800763	335	199237	06308	99801	23
38	801892	332	999126	1.3	802765	334	197235	06337	99799	22
39	803876	331	999118	1.3	804858	332	195242	06366	99797	21
40	805852	329	999110	1.3	806742	331	193258	06395	99795	20
41	8.807819	328	9.999102	1.3	8.808717	329	11.191283	06424	99793	19
42	809777	326	999094	1.3	810683	328	189317	06453	99792	18
43	811726	325	999086	1.4	812641	326	187359	06482	99790	17
44	813667	323	999077	1.4	814589	325	185411	06511	99788	16
45	815599	322	999069	1.4	816529	323	183471	06540	99786	15
46	817522	320	999061	1.4	818461	322	181539	06569	99784	14
47	819436	319	999053	1.4	820384	320	179616	06598	99782	13
48	821343	318	999044	1.4	822298	319	177702	06627	99780	12
49	823240	316	999036	1.4	824205	318	175795	06656	99778	11
50	825130	315	999027	1.4	826103	316	173897	06685	99776	10
51	8.827011	313	9.999019	1.4	8.827992	315	11.172008	06714	99774	9
52	828884	312	999010	1.4	829874	314	170126	06743	99772	8
53	830749	311	999002	1.4	831748	312	168252	06773	99770	7
54	832607	309	998993	1.4	833613	311	166387	06802	99768	6
55	834456	308	998984	1.4	835471	310	164529	06831	99766	5
56	836297	307	998976	1.4	837321	308	162679	06860	99764	4
57	838130	306	998967	1.4	839163	307	160837	06889	99762	3
58	839956	304	998958	1.5	840998	306	159002	06918	99760	2
59	841774	303	998950	1.5	842825	304	157175	06947	99758	1
60	843585	302	998941	1.5	844644	303	155356	06976	99756	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (4<sup>o</sup>) Natural Sines.

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.
0	8.843585	300	9.998941	1.5	8.844644	302	11.155356	06976	99756 60
1	845357	299	998932	1.5	846455	301	153545	07005	99754 59
2	847183	298	998923	1.5	848260	299	151740	07034	99752 58
3	848971	297	998914	1.5	850057	298	149943	07063	99750 57
4	850751	295	998905	1.5	851846	297	148154	07092	99748 56
5	852525	294	998896	1.5	853628	296	146372	07121	99746 55
6	854291	293	998887	1.5	855403	295	144597	07150	99744 54
7	856049	292	998878	1.5	857171	294	142829	07179	99742 53
8	857801	291	998869	1.5	858932	293	141068	07208	99740 52
9	859546	290	998860	1.5	860686	292	139314	07237	99738 51
10	861283	288	998851	1.5	862433	291	137567	07266	99736 50
11	8.863014	287	9.998841	1.5	8.864173	289	11.135827	07295	99734 49
12	864738	286	998832	1.5	865906	288	134094	07324	99731 48
13	866455	285	998823	1.6	867632	287	132368	07353	99729 47
14	868165	284	998813	1.6	869351	285	130649	07382	99727 46
15	869868	283	998804	1.6	871064	284	128936	07411	99725 45
16	871565	282	998795	1.6	872770	283	127230	07440	99723 44
17	873255	281	998785	1.6	874469	282	125531	07469	99721 43
18	874938	279	998776	1.6	876162	281	123838	07498	99719 42
19	876615	279	998766	1.6	877849	280	122151	07527	99716 41
20	878285	277	998757	1.6	879529	279	120471	07556	99714 40
21	8.879949	276	9.998747	1.6	8.881202	278	11.118798	07585	99712 39
22	881607	275	998738	1.6	882869	277	117131	07614	99710 38
23	883258	274	998728	1.6	884530	276	115470	07643	99708 37
24	884903	273	998718	1.6	886185	275	113815	07672	99706 36
25	886542	272	998708	1.6	887833	274	112167	07701	99703 35
26	888174	271	998699	1.6	889476	273	110524	07730	99701 34
27	889801	270	998689	1.6	891112	272	108888	07759	99699 33
28	891421	269	998679	1.6	892742	271	107258	07788	99696 32
29	893035	268	998669	1.7	894366	270	105634	07817	99694 31
30	894643	267	998659	1.7	895984	269	104016	07846	99692 30
31	8.896246	266	9.998649	1.7	8.897596	268	11.102404	07875	99689 29
32	897842	265	998639	1.7	899203	267	100797	07904	99687 28
33	899432	264	998629	1.7	900803	266	999197	07933	99685 27
34	901017	263	998619	1.7	902398	265	997602	07962	99683 26
35	902596	262	998609	1.7	903987	264	996013	07991	99680 25
36	904169	261	998599	1.7	905570	263	994430	08020	99678 24
37	905736	260	998589	1.7	907147	262	992853	08049	99676 23
38	907297	259	998578	1.7	908719	261	991281	08078	99673 22
39	908853	258	998568	1.7	910285	260	989715	08107	99671 21
40	910404	257	998558	1.7	911846	259	988154	08136	99668 20
41	8.911949	256	9.998548	1.7	8.913401	258	11.086599	08165	99666 19
42	913488	255	998537	1.7	914951	257	9865049	08194	99664 18
43	915022	255	998527	1.7	916496	256	985055	08223	99661 17
44	916550	254	998516	1.8	918034	255	983606	08252	99659 16
45	918073	253	998505	1.8	919568	254	982162	08281	99657 15
46	919591	252	998495	1.8	921096	253	980719	08310	99654 14
47	921103	251	998485	1.8	922619	252	979281	08339	99652 13
48	922610	250	998474	1.8	924136	251	977843	08368	99649 12
49	924112	249	998464	1.8	925649	250	976405	08397	99647 11
50	925609	249	998453	1.8	927156	249	974968	08426	99644 10
51	8.927100	248	9.998442	1.8	8.928658	248	11.071342	08455	99642 9
52	928587	247	998431	1.8	930155	247	973531	08484	99639 8
53	930058	246	998421	1.8	931647	246	972100	08513	99637 7
54	931544	245	998410	1.8	933134	245	970666	08542	99635 6
55	933015	244	998399	1.8	934616	244	969234	08571	99632 5
56	934481	243	998388	1.8	936093	243	967800	08600	99630 4
57	935942	243	998377	1.8	937565	242	966365	08629	99627 3
58	937398	242	998366	1.8	939032	241	964931	08658	99625 2
59	938850	241	998355	1.8	940494	240	963496	08687	99622 1
60	940293	241	998344	1.8	941952	243	962061	08716	99619 0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.
0	8.940296	240	9.998344	1.9.	8.941952	242	11.058048	08716	99619 60
1	941738	239	998333	1.9	943404	241	056596	08745	99617 59
2	943174	239	998322	1.9	944852	240	055148	08774	99614 58
3	944606	238	998311	1.9	946295	240	053705	08803	99612 57
4	946034	237	998300	1.9	947734	239	052266	08831	99609 56
5	947456	236	998289	1.9	949168	238	050832	08860	99607 55
6	948874	235	998277	1.9	950597	238	049403	08889	99604 54
7	950287	235	998266	1.9	952021	237	047979	08918	99602 53
8	951693	234	998255	1.9	953441	236	046559	08947	99599 52
9	953100	233	998243	1.9	954856	236	045144	08976	99596 51
10	954499	232	998232	1.9	956267	235	043733	09005	99594 50
11	955894	232	9.998220	1.9	8.957674	234	11.042326	09034	99591 49
12	957284	231	998209	1.9	959075	233	040925	09063	99588 48
13	95870	230	998197	1.9	960473	232	039527	09092	99586 47
14	960052	229	998186	1.9	961866	231	038134	09121	99583 46
15	961429	229	998174	1.9	963255	231	036745	09150	99580 45
16	962801	228	998163	1.9	964639	230	035361	09179	99578 44
17	964170	227	998151	1.9	966019	229	033981	09208	99575 43
18	965534	227	998139	2.0	967394	229	032606	09237	99572 42
19	966893	226	998128	2.0	968766	228	031234	09266	99570 41
20	968249	225	998116	2.0	970133	227	029867	09295	99567 40
21	8.969600	224	9.998104	2.0	8.971496	226	11.028504	09324	99564 39
22	970947	224	998092	2.0	972855	226	027145	09353	99562 38
23	972289	223	998080	2.0	974209	225	025791	09382	99559 37
24	973628	222	998068	2.0	975560	224	024440	09411	99556 36
25	974962	222	998056	2.0	976906	224	023094	09440	99553 35
26	976293	221	998044	2.0	978248	224	021752	09469	99551 34
27	977619	220	998032	2.0	979586	223	020414	09498	99548 33
28	978941	220	998020	2.0	980921	222	019079	09527	99545 32
29	980259	219	998008	2.0	982251	222	017749	09556	99542 31
30	981573	218	997996	2.0	983577	221	016423	09585	99540 30
31	8.982883	218	9.997984	2.0	8.984899	220	11.015101	09614	99537 29
32	984189	217	997972	2.0	986217	219	014783	09642	99534 28
33	985491	216	997959	2.0	987532	218	013468	09671	99531 27
34	986789	216	997947	2.0	988842	218	012158	09700	99528 26
35	988083	215	997935	2.1	990149	217	009851	09729	99526 25
36	989374	214	997922	2.1	991451	217	008549	09758	99523 24
37	990660	214	997910	2.1	992750	216	007250	09787	99520 23
38	991943	213	997897	2.1	994045	215	005955	09816	99517 22
39	993222	212	997885	2.1	995337	215	004663	09845	99514 21
40	994497	212	997872	2.1	996624	214	003376	09874	99511 20
41	8.995768	211	9.997860	2.1	8.997908	213	11.002092	09903	99508 19
42	997036	211	997847	2.1	999188	213	002081	09932	99505 18
43	998299	210	997835	2.1	9.000465	212	10.999535	09961	99503 17
44	999560	209	997822	2.1	001738	211	998262	0.999	99500 16
45	0.003816	209	997809	2.1	003007	211	996993	10019	99497 15
46	002039	208	997797	2.1	004272	210	995728	10048	99494 14
47	003318	208	997784	2.1	005534	210	994466	10077	99491 13
48	004563	207	997771	2.1	006792	209	993208	10105	99488 12
49	005805	206	997758	2.1	008047	208	991953	10135	99485 11
50	007044	206	997745	2.1	009298	208	990702	10164	99482 10
51	9.003278	205	9.997732	2.1	9.010546	207	10.989454	10192	99479 9
52	009510	205	997719	2.1	011790	207	988210	10221	99476 8
53	010737	204	997706	2.1	013031	206	686969	10250	99473 7
54	011962	203	997693	2.2	014268	205	985732	10279	99470 6
55	013182	203	997680	2.2	015502	205	984498	10308	99467 5
56	014400	202	997667	2.2	016732	204	983268	10337	99464 4
57	015613	202	997654	2.2	017959	204	982041	10366	99461 3
58	016824	201	997641	2.2	019183	203	980817	10395	99458 2
59	018031	201	997628	2.2	020403	203	979597	10424	99455 1
60	019235	201	997614	2.2	021620	203	978380	10453	99452 0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.

TABLE II. Log. Sines and Tangents. (6<sup>2</sup>) Natural Sines.

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	0.019235	200	9.997614	2.2	9.021620	202	10.978380	10453	99452	60
1	020135	199	997601	2.2	022834	202	977166	10482	99449	59
2	021632	199	997588	2.2	024044	201	975956	10511	99446	58
3	022825	198	997574	2.2	025251	201	974749	10540	99443	57
4	024016	198	997561	2.2	026455	200	973545	10569	99440	56
5	025203	197	997547	2.2	027655	199	972345	10597	99437	55
6	026386	197	997534	2.2	028852	199	971148	10626	99434	54
7	027567	196	997520	2.3	030046	198	969954	10655	99431	53
8	028744	196	997507	2.3	031237	198	968763	10684	99428	52
9	029918	195	997493	2.3	032425	197	967575	10713	99424	51
10	031089	195	997480	2.3	033609	197	966391	10742	99421	50
11	032257	194	9.997466	2.3	9.034791	196	10.965209	10771	99418	49
12	33421	194	997452	2.3	035969	196	964031	10800	99415	48
13	34382	193	997439	2.3	037144	195	962856	10829	99412	47
14	035741	192	997425	2.3	038316	195	961684	10858	99409	46
15	036896	192	997411	2.3	039485	194	960515	10887	99406	45
16	038048	191	997397	2.3	040651	194	959349	10916	99402	44
17	039197	191	997383	2.3	041813	193	958187	10945	99399	45
18	040342	190	997369	2.3	042973	193	957027	10973	99396	42
19	041485	190	997355	2.3	044130	192	955870	11002	99393	41
20	042625	189	997341	2.3	045284	192	954716	11031	99390	40
21	9.043762	189	9.997327	2.4	9.046434	191	10.953566	11060	99386	39
22	044895	188	997313	2.4	047582	191	952418	11089	99383	38
23	046026	188	997299	2.4	048727	191	951273	11118	99380	37
24	047154	187	997285	2.4	049869	190	950131	11147	99377	36
25	048279	187	997271	2.4	051008	189	948992	11176	99374	35
26	049400	186	997257	2.4	052144	189	947856	11205	99370	34
27	050519	186	997242	2.4	053277	188	946723	11234	99367	33
28	051635	185	997228	2.4	054407	188	945593	11263	99364	32
29	052749	185	997214	2.4	055535	187	944465	11291	99360	31
30	053859	184	997199	2.4	056659	187	943341	11320	99357	30
31	9.054966	184	9.997185	2.4	9.057781	186	10.942219	11349	99354	29
32	056071	184	997170	2.4	058900	186	941100	11378	99351	28
33	057172	183	997156	2.4	060016	185	939984	11407	99347	27
34	058271	183	997141	2.4	061130	185	938870	11436	99344	26
35	059367	182	997127	2.4	062240	185	937760	11465	99341	25
36	060460	182	997112	2.4	063348	185	936652	11494	99337	24
37	061551	181	997098	2.4	064453	184	935547	11523	99334	23
38	062639	181	997083	2.5	065556	183	934444	11552	99331	22
39	063724	180	997068	2.5	066655	183	933345	11580	99327	21
40	064806	180	997053	2.5	067752	182	932248	11609	99324	20
41	9.065885	179	9.997039	2.5	9.068846	182	10.931154	11638	99320	19
42	066962	179	997024	2.5	069038	181	930062	11667	99317	18
43	068036	179	997009	2.5	071027	181	928973	11696	99314	17
44	069107	178	996994	2.5	072113	181	927887	11725	99310	16
45	070176	178	996979	2.5	073197	180	926803	11754	99307	15
46	071242	177	996964	2.5	074278	180	925722	11783	99303	14
47	072306	177	996949	2.5	075356	179	924644	11812	99300	13
48	073366	176	996934	2.5	076432	179	923568	11841	99297	12
49	074424	176	996919	2.5	077505	178	922495	11869	99293	11
50	075480	175	996904	2.5	078576	178	921424	11898	99290	10
51	9.076533	175	9.996889	2.5	9.079644	178	10.920356	11927	99286	9
52	077583	175	996874	2.5	080710	177	919290	11956	99283	8
53	078631	174	996858	2.5	081773	177	918227	11985	99279	7
54	079676	174	996843	2.5	082833	176	917167	12014	99276	6
55	080719	173	996828	2.5	083891	176	916109	12043	99272	5
56	081759	173	996812	2.5	084947	175	915053	12071	99269	4
57	082797	172	996797	2.6	086000	175	914000	12100	99265	3
58	083832	172	996782	2.6	087050	175	912950	12129	99262	2
59	084864	172	996766	2.6	088098	174	911902	12158	99258	1
60	085894	172	996751	2.6	089144	174	910856	12187	99255	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine	N. cos.	
0	9.085894	171	9.996751	2.6	9.089144	174	10.910856	12187	99255	60
1	086722	171	996735	2.6	090187	173	909813	12216	99251	59
2	087947	170	996720	2.6	091228	173	908772	12245	99248	58
3	088970	170	996704	2.6	092266	173	907734	12274	99244	57
4	089990	170	996688	2.6	093302	172	906698	12302	99240	56
5	091038	169	996673	2.6	094336	172	905664	12331	99237	55
6	092024	169	996657	2.6	095367	172	904633	12360	99233	54
7	093037	168	996641	2.6	096395	171	903605	12389	99230	53
8	094047	168	996625	2.6	097422	171	902578	12418	99226	52
9	095056	168	996610	2.6	098446	170	901554	12447	99222	51
10	096062	167	996594	2.6	099468	170	900532	12476	99219	50
11	9.097065	167	9.996578	2.7	1.100487	169	10.899513	12504	99215	49
12	098036	166	996562	2.7	101504	169	898496	12533	99211	48
13	099065	166	996546	2.7	102519	169	897481	12562	99208	47
14	100032	166	996530	2.7	103532	168	896468	12591	99204	46
15	101056	165	996514	2.7	104542	168	895458	12620	99200	45
16	102048	165	996498	2.7	105550	168	894450	12649	99197	44
17	103037	164	996482	2.7	106556	167	893444	12678	99193	43
18	104025	164	996465	2.7	107559	167	892441	12706	99189	42
19	105010	164	996449	2.7	108560	166	891440	12735	99186	41
20	105992	163	996433	2.7	109559	166	890441	12764	99182	40
21	9.106973	163	9.996417	2.7	9.110556	166	10.889444	12793	99178	39
22	107951	163	996400	2.7	111551	165	888449	12822	99175	38
23	108927	162	996384	2.7	112543	165	887457	12851	99171	37
24	109901	162	996368	2.7	113533	165	886467	12880	99167	36
25	110873	162	996351	2.7	114521	164	885479	12908	99163	35
26	111842	161	996335	2.7	115507	164	884493	12937	99160	34
27	112809	161	996318	2.7	116491	164	883509	12966	99156	33
28	113774	160	996302	2.8	117472	163	882528	12995	99152	32
29	114737	160	996285	2.8	118452	163	881548	13024	99148	31
30	115698	160	996269	2.8	119429	162	880571	13053	99144	30
31	9.116656	159	9.996252	2.8	9.120404	162	10.879596	13081	99141	29
32	117613	159	996235	2.8	121377	162	878623	13110	99137	28
33	118567	159	996219	2.8	122348	161	877652	13139	99133	27
34	119519	158	996202	2.8	123317	161	876683	13168	99129	26
35	120469	158	996185	2.8	124284	161	875716	13197	99125	25
36	121417	158	996168	2.8	125249	160	874751	13226	99122	24
37	122362	157	996151	2.8	126211	160	873789	13254	99118	23
38	123306	157	996134	2.8	127172	160	872828	13283	99114	22
39	124248	157	996117	2.8	128130	159	871870	13312	99110	21
40	125187	156	996100	2.8	129087	159	870913	13341	99106	20
41	9.126125	156	9.996083	2.9	9.130041	159	10.869959	13370	99102	19
42	127060	156	996066	2.9	130994	158	869007	13399	99098	18
43	127993	155	996049	2.9	131944	158	868056	13427	99094	17
44	128925	155	996032	2.9	132893	158	867107	13456	99091	16
45	129854	154	996015	2.9	133839	157	866161	13485	99087	15
46	130781	154	995998	2.9	134784	157	865216	13514	99083	14
47	131706	154	995980	2.9	135726	157	864274	13543	99079	13
48	132630	153	995963	2.9	136667	156	863333	13572	99075	12
49	133551	153	995946	2.9	137605	156	862395	13600	99071	11
50	134470	153	995928	2.9	138542	156	861458	13629	99067	10
51	9.135387	152	9.995911	2.9	9.139476	155	10.860524	13658	99063	9
52	136303	152	995894	2.9	140409	155	859591	13687	99059	8
53	137216	152	995876	2.9	141340	155	858660	13716	99055	7
54	138128	152	995859	2.9	142269	154	857731	13744	99051	6
55	139037	151	995841	2.9	143196	154	856804	13773	99047	5
56	139944	151	995823	2.9	144121	154	855879	13802	99043	4
57	140850	151	995806	2.9	145044	153	854956	13831	99039	3
58	141754	150	995788	2.9	145966	153	854034	13860	99035	2
59	142655	150	995771	2.9	146885	153	853115	13889	99031	1
60	143555	150	995753	2.9	147803	153	852197	13917	99027	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II.

Log. Sines and Tangents. (8°) Natural Sines.

29

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.143555	150	9.995753	3.0	9.147803	153	10.852197	13917	99027	60
1	144453	149	995735	3.0	148718	152	851282	13946	99023	59
2	145349	149	995717	3.0	149632	152	850368	13975	99019	58
3	146243	149	995699	3.0	150544	152	849456	14004	99015	57
4	147136	149	995681	3.0	151454	151	848546	14033	99011	56
5	148026	148	995664	3.0	152363	151	847637	14061	99006	55
6	148915	148	995646	3.0	153269	151	846731	14090	99002	54
7	149802	148	995628	3.0	154174	151	845826	14119	98998	53
8	150686	147	995610	3.0	155077	150	844923	14148	98994	52
9	151569	147	995591	3.0	155978	150	844022	14177	98990	51
10	152451	147	995573	3.0	156877	150	843123	14205	98986	50
11	9.153330	147	9.995555	3.0	9.157775	150	842225	14234	98982	49
12	154208	146	995537	3.0	158671	149	841329	14263	98978	48
13	155083	146	995519	3.0	159565	149	840435	14292	98973	47
14	155957	146	995501	3.0	160457	149	839543	14320	98969	46
15	156830	145	995482	3.1	161347	148	838653	14349	98965	45
16	157700	145	995464	3.1	162236	148	837764	14378	98961	44
17	158569	145	995446	3.1	163123	148	836877	14407	98957	43
18	159435	144	995427	3.1	164008	148	835992	14436	98953	42
19	160301	144	995409	3.1	164892	147	835108	14464	98948	41
20	161164	144	995390	3.1	165774	147	834226	14493	98944	40
21	9.162025	144	9.995372	3.1	9.166654	147	10.833346	14522	98940	39
22	162885	143	995353	3.1	167532	146	832468	14551	98936	38
23	163743	143	995334	3.1	168409	146	831591	14580	98931	37
24	164600	143	995316	3.1	169284	146	830716	14608	98927	36
25	165454	142	995297	3.1	170157	145	829843	14637	98923	35
26	166307	142	995278	3.1	171029	145	828971	14666	98919	34
27	167159	142	995260	3.1	171899	145	828101	14695	98914	33
28	168008	141	995241	3.2	172767	144	827233	14723	98910	32
29	168856	141	995222	3.2	173634	144	826366	14752	98906	31
30	169702	141	995203	3.2	174499	144	825501	14781	98902	30
31	9.170547	140	9.995184	3.2	9.175362	144	10.824638	14810	98897	29
32	171389	140	995165	3.2	176224	143	823776	14838	98893	28
33	172230	140	995146	3.2	177084	143	822916	14867	98889	27
34	173070	140	995127	3.2	177942	143	822058	14895	98884	26
35	173908	140	995108	3.2	178799	142	821201	14925	98880	25
36	174744	139	995089	3.2	179655	142	820345	14954	98876	24
37	175578	139	995070	3.2	180508	142	819492	14982	98871	23
38	176411	139	995051	3.2	181360	142	818640	15011	98867	22
39	177242	138	995032	3.2	182211	141	817789	15040	98863	21
40	178072	138	995013	3.2	183059	141	816941	15069	98858	20
41	9.178900	138	9.994993	3.2	9.183907	141	10.816093	15097	98854	19
42	179726	137	994974	3.2	184752	141	815248	15126	98849	18
43	180551	137	994955	3.2	185597	140	814403	15155	98845	17
44	181374	137	994935	3.2	186439	140	813561	15184	98841	16
45	182196	137	994916	3.2	187280	140	812720	15212	98836	15
46	183016	136	994896	3.3	188120	140	811880	15241	98832	14
47	183834	136	994877	3.3	188958	139	811042	15270	98827	13
48	184651	136	994857	3.3	189794	139	810206	15299	98823	12
49	185466	136	994838	3.3	190629	139	809371	15327	98818	11
50	186280	135	994818	3.3	191462	139	808538	15356	98814	10
51	9.187092	135	9.994798	3.3	9.192294	138	10.807706	15385	98809	9
52	187903	135	994779	3.3	192134	138	806876	15414	98805	8
53	188712	135	994759	3.3	192953	138	806047	15442	98800	7
54	189519	134	994739	3.3	193780	138	805220	15471	98796	6
55	190325	134	994719	3.3	194606	137	804394	15500	98791	5
56	191130	134	994700	3.3	195430	137	803570	15529	98787	4
57	191933	134	994680	3.3	196253	137	802747	15557	98782	3
58	192734	133	994660	3.3	197074	137	801926	15586	98778	2
59	193534	133	994640	3.3	197894	137	801106	15615	98773	1
60	194332	133	994620	3.3	198713	136	800287	15643	98769	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	7

81 Degrees.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.194332		9.994620		9.199713		10.800287	15643	98769	60
1	195129	133	994600	3.3	204529	136	799471	15672	98764	59
2	195925	133	994580	3.3	201345	136	798655	15701	98760	58
3	196719	132	994560	3.3	202159	135	797841	15730	98755	57
4	197511	132	994540	3.4	202971	135	797029	15758	98751	56
5	198302	132	994519	3.4	203782	135	796218	15787	98746	55
6	199091	132	994499	3.4	204592	135	795408	15816	98741	54
7	199879	131	994479	3.4	205400	134	794600	15845	98737	53
8	200366	131	994459	3.4	206207	134	793793	15873	98732	52
9	201451	131	994438	3.4	207013	134	792987	15902	98728	51
10	202234	130	994418	3.4	207817	134	792183	15931	98723	50
11	203017	130	9.994397		9.208619		10.791381	15959	98718	49
12	203797	130	994377	3.4	209420	133	790580	15988	98714	48
13	204577	130	994357	3.4	210220	133	789780	16017	98709	47
14	205354	129	994336	3.4	211018	133	788982	16046	98704	46
15	206131	129	994316	3.4	211815	133	788185	16074	98700	45
16	206906	129	994295	3.4	212611	132	787389	16103	98695	44
17	207679	129	994274	3.4	213405	132	786595	16132	98690	43
18	208452	128	994254	3.5	214198	132	785802	16160	98686	42
19	209222	128	994233	3.5	214989	132	785011	16189	98681	41
20	209992	128	994212	3.5	215780	131	784220	16218	98676	40
21	9.210760		9.994191		9.216568		10.783432	16246	98671	39
22	211526	127	994171	3.5	217356	131	782644	16275	98667	38
23	212291	127	994150	3.5	218142	131	781858	16304	98662	37
24	213055	127	994129	3.5	218926	130	781074	16333	98657	36
25	213818	127	994108	3.5	219710	130	780290	16361	98652	35
26	214579	127	994087	3.5	220492	130	779508	16390	98648	34
27	215338	126	994066	3.5	221272	130	778728	16419	98643	33
28	216097	126	994045	3.5	222052	130	777948	16447	98638	32
29	216854	126	994024	3.5	222830	129	777170	16476	98633	31
30	217609	126	994003	3.5	223606	129	776394	16505	98629	30
31	9.218363		9.993981		9.224382		10.775618	16533	98624	29
32	219116	125	993960	3.5	225156	129	774844	16562	98619	28
33	219868	125	993939	3.5	225929	129	774071	16591	98614	27
34	220618	125	993918	3.5	226700	128	773300	16620	98609	26
35	221367	125	993896	3.5	227471	128	772529	16648	98604	25
36	222115	124	993875	3.6	228239	128	771761	16677	98600	24
37	222861	124	993854	3.6	229007	128	770993	16706	98595	23
38	223606	124	993832	3.6	229773	127	770227	16734	98590	22
39	224349	124	993811	3.6	230539	127	769461	16763	98585	21
40	225092	123	993789	3.6	231302	127	768698	16792	98580	20
41	9.225833		9.993768		9.232065		10.767935	16820	98575	19
42	226573	123	993746	3.6	232826	127	767174	16849	98570	18
43	227311	123	993725	3.6	233586	126	766414	16878	98565	17
44	228048	123	993703	3.6	234345	126	765655	16906	98561	16
45	228784	122	993681	3.6	235103	126	764897	16935	98556	15
46	229518	122	993660	3.6	235859	126	764141	16964	98551	14
47	230252	122	993638	3.6	236614	126	763386	16992	98546	13
48	230984	122	993616	3.6	237368	125	762632	17021	98541	12
49	231714	122	993594	3.6	238120	125	761880	17050	98536	11
50	232444	121	993572	3.7	238872	125	761128	17078	98531	10
51	9.233172		9.993550		9.239622		10.760378	17107	98526	9
52	233899	121	994528	3.7	240371	125	759629	17136	98521	8
53	234625	121	994506	3.7	241118	124	758882	17164	98516	7
54	235349	120	994484	3.7	241865	124	758135	17193	98511	6
55	236073	120	994462	3.7	242610	124	757390	17222	98506	5
56	236795	120	994440	3.7	243354	124	756646	17250	98501	4
57	237515	120	994418	3.7	244097	124	755903	17279	98496	3
58	238235	120	994396	3.7	244839	123	755161	17308	98491	2
59	238953	119	994374	3.7	245579	123	754421	17336	98486	1
60	239670		994351		246319		753681	17365	98481	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	



TABLE II.

Log. Sines and Tangents. (10°) Natural Sines.

31

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N.sine.	N. cos.	
0	9.239670		9.993351		9.216319		10.753681	17365	98481	60
1	240386	119	993329	3.7	247057	123	752943	17393	98476	59
2	241101	119	993307	3.7	247794	123	752905	17422	98471	58
3	241814	119	993285	3.7	248530	122	751470	17451	98466	57
4	242526	118	993262	3.7	249264	122	750736	17479	98461	56
5	243237	118	993240	3.7	249998	122	750002	17508	98455	55
6	243947	118	993217	3.7	250730	122	749270	17537	98450	54
7	244656	118	993195	3.8	251461	122	748539	17565	98445	53
8	245363	118	993172	3.8	252191	122	747809	17594	98440	52
9	246069	117	993149	3.8	252920	121	747080	17623	98435	51
10	246775	117	993127	3.8	253648	121	746352	17651	98430	50
11	5 247478	117	9.993104	3.8	9.254374		10.745626	17680	98425	49
12	248181	117	993081	3.8	255100	121	744900	17708	98420	48
13	248883	117	993059	3.8	255824	120	744176	17737	98414	47
14	249583	116	993036	3.8	256547	120	743453	17766	98409	46
15	250282	116	993013	3.8	257269	120	742731	17794	98404	45
16	250980	116	992990	3.8	257990	120	742010	17823	98399	44
17	251677	116	992967	3.8	258710	120	741290	17852	98394	43
18	252373	116	992944	3.8	259429	120	740571	17880	98389	42
19	253067	116	992921	3.8	260146	119	739854	17909	98383	41
20	253761	115	992898	3.8	260863	119	739137	17937	98378	40
21	9.254453	115	9.992875	3.8	9.261578		10.738422	17966	98373	39
22	255144	115	992852	3.8	262292	119	737708	17995	98368	38
23	255834	115	992829	3.9	263005	119	736995	18023	98362	37
24	256523	115	992806	3.9	263717	119	736283	18052	98357	36
25	257211	114	992783	3.9	264428	118	735572	18081	98352	35
26	257898	114	992759	3.9	265138	118	734862	18109	98347	34
27	258583	114	992736	3.9	265847	118	734153	18138	98341	33
28	259268	114	992713	3.9	266555	118	733445	18166	98336	32
29	259951	114	992690	3.9	267261	118	732739	18195	98331	31
30	260633	113	992666	3.9	267967	118	732033	18224	98325	30
31	9.261314	113	9.992643	3.9	9.268671		10.731329	18252	98320	29
32	261994	113	992619	3.9	269375	117	731329	18281	98315	28
33	262673	113	992596	3.9	270077	117	730625	18309	98310	27
34	263351	113	992572	3.9	270779	117	729921	18338	98304	26
35	264027	113	992549	3.9	271479	117	729217	18367	98299	25
36	264703	112	992525	3.9	272178	116	728522	18395	98294	24
37	265377	112	992501	3.9	272876	116	727827	18424	98289	23
38	266051	112	992478	3.9	273573	116	727132	18452	98283	22
39	266723	112	992454	4.0	274269	116	726427	18481	98277	21
40	267395	112	992430	4.0	274964	116	725731	18509	98272	20
41	9.268065	111	9.992406	4.0	9.275658		10.724342	18538	98267	19
42	268734	111	992382	4.0	276351	115	725036	18567	98261	18
43	269402	111	992359	4.0	277043	115	724349	18595	98256	17
44	270069	111	992335	4.0	277734	115	723649	18624	98250	16
45	270735	111	992311	4.0	278424	115	722957	18652	98245	15
46	271400	111	992287	4.0	279113	115	722266	18681	98240	14
47	272064	110	992263	4.0	279801	115	721576	18710	98234	13
48	272726	110	992239	4.0	280488	114	720887	18738	98229	12
49	273388	110	992214	4.0	281174	114	720199	18767	98223	11
50	274049	110	992190	4.0	281858	114	719512	18795	98218	10
51	9.274408	110	9.992166	4.0	9.282542		10.717458	18824	98212	9
52	275367	110	992142	4.0	283225	114	718826	18852	98207	8
53	276024	109	992117	4.1	283907	113	718142	18881	98201	7
54	276681	109	992093	4.1	284588	113	717458	18910	98196	6
55	277337	109	992069	4.1	285268	113	716775	18938	98190	5
56	277991	109	992044	4.1	285947	113	716093	18967	98185	4
57	278644	109	992020	4.1	286624	113	715412	18995	98179	3
58	279297	109	991996	4.1	287301	113	714737	19024	98174	2
59	279948	108	991971	4.1	287977	113	714053	19052	98168	1
60	280599	108	991947	4.1	288652	112	713376	19081	98163	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

79 Degrees.

	Sine.	D. 10'	Cos. ac.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	9.280599	105	9.991947	4.1	9.288552	112	10.711348	19081	98163	60
1	281248	108	991922	4.1	289326	112	710674	19109	98157	59
2	281897	108	991897	4.1	289999	112	710001	19138	98152	58
3	282544	108	991873	4.1	290671	112	709329	19167	98146	57
4	283190	108	991848	4.1	291342	112	708658	19195	98140	56
5	283836	107	991823	4.1	292013	112	707987	19224	98135	55
6	284480	107	991799	4.1	292682	111	707318	19252	98129	54
7	285124	107	991774	4.1	293350	111	706650	19281	98124	53
8	285766	107	991749	4.2	294017	111	705983	19309	98118	52
9	286408	107	991724	4.2	294684	111	705316	19338	98112	51
10	287048	107	991699	4.2	295349	111	704651	19366	98107	50
11	9.287687	106	9.991674	4.2	9.296013	111	10.703987	19395	98101	49
12	288326	106	991649	4.2	296677	110	703323	19423	98096	48
13	288964	106	991624	4.2	297339	110	702661	19452	98090	47
14	289600	106	991599	4.2	298001	110	701999	19481	98084	46
15	290236	106	991574	4.2	298662	110	701338	19509	98079	45
16	290870	106	991549	4.2	299322	110	700678	19538	98073	44
17	291504	105	991524	4.2	299980	110	700020	19566	98067	43
18	292137	105	991498	4.2	300638	109	699362	19595	98061	42
19	292768	105	991473	4.2	301295	109	698705	19623	98056	41
20	293399	105	991448	4.2	301951	109	698049	19652	98050	40
21	9.294029	105	9.991422	4.2	9.302607	109	10.697393	19680	98044	39
22	294658	105	991397	4.2	303261	109	697739	19709	98039	38
23	295286	104	991372	4.3	303914	109	697086	19737	98033	37
24	295913	104	991346	4.3	304567	109	696433	19766	98027	36
25	296539	104	991321	4.3	305218	108	695782	19794	98021	35
26	297164	104	991295	4.3	305869	108	695131	19823	98016	34
27	297788	104	991270	4.3	306519	108	694481	19851	98010	33
28	298412	104	991244	4.3	307168	108	693832	19880	98004	32
29	299034	104	991218	4.3	307815	108	693185	19908	97998	31
30	299655	103	991193	4.3	308463	108	692537	19937	97992	30
31	9.300276	103	9.991167	4.3	9.309109	107	10.690891	19965	97987	29
32	300895	103	991141	4.3	309754	107	692024	19994	97981	28
33	301514	103	991115	4.3	310398	107	691362	20022	97975	27
34	302132	103	991090	4.3	311042	107	688958	20051	97969	26
35	302748	103	991064	4.3	311685	107	688315	20079	97963	25
36	303364	102	991038	4.3	312327	107	687673	20108	97958	24
37	303979	102	991012	4.3	312967	107	687033	20136	97952	23
38	304593	102	990986	4.3	313608	106	686392	20165	97946	22
39	305207	102	990960	4.3	314247	106	685753	20193	97940	21
40	305819	102	990934	4.3	314885	106	685115	20222	97934	20
41	9.306430	102	9.990908	4.4	9.315523	106	10.684477	20250	97928	19
42	307041	102	990882	4.4	316159	106	683841	20279	97922	18
43	307650	101	990855	4.4	316795	106	683205	20308	97916	17
44	308259	101	990829	4.4	317430	106	682570	20336	97910	16
45	308867	101	990803	4.4	318064	105	681936	20364	97905	15
46	309474	101	990777	4.4	318697	105	681303	20393	97899	14
47	310080	101	990750	4.4	319329	105	680671	20421	97893	13
48	310685	101	990724	4.4	319961	105	680039	20450	97887	2
49	311289	100	990697	4.4	320592	105	679408	20478	97881	1
50	311893	100	990671	4.4	321222	105	678778	20507	97875	10
51	9.312495	100	9.990644	4.4	9.321851	105	10.678149	20535	97869	9
52	313097	100	990618	4.4	322479	104	677521	20563	97863	-
53	313698	100	990591	4.4	323106	104	676894	20592	97857	-
54	314297	100	990565	4.4	323733	104	676267	20620	97851	6
55	314897	100	990538	4.4	324358	104	675642	20649	97845	5
56	315495	100	990511	4.4	324983	104	675017	20677	97839	4
57	316092	99	990485	4.5	325607	104	674393	20706	97833	3
58	316689	99	990458	4.5	326231	104	673769	20734	97827	2
59	317284	99	990431	4.5	326853	104	673147	20763	97821	1
60	317879	99	990404	4.5	327475	104	672525	20791	97815	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (12°) Natural Sines.

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.
6	9.317873		9.990104		9.327474		10.672526	20791 97815	60
1	318473	99.0	990378	4.5	328035	103	671905	20820 97809	59
2	319111	98.8	990351	4.5	328715	103	671285	20848 97803	58
3	319658	98.7	990324	4.5	329334	103	670366	20877 97797	57
4	320249	98.6	990297	4.5	329953	103	670447	20905 97791	56
5	320840	98.4	990270	4.5	330570	103	669430	20933 97784	55
6	321430	98.3	990243	4.5	331187	103	668813	20962 97778	54
7	322019	98.2	990215	4.5	331803	103	668197	20990 97772	53
8	322607	98.0	990188	4.5	332418	102	667582	21019 97766	52
9	323194	97.9	990161	4.5	333033	102	666967	21047 97760	51
10	323780	97.7	990134	4.5	333646	102	666354	21076 97754	50
11	9.324366	97.6	9.990107	4.6	9.334259	102	10.665741	21104 9774	49
12	324950	97.5	990079	4.6	334871	102	665129	21132 97742	48
13	325534	97.3	990052	4.6	335482	102	664518	21161 97735	47
14	326117	97.2	990025	4.6	336093	102	663907	21189 97729	46
15	326700	97.0	989997	4.6	336702	102	663298	21218 97723	45
16	327281	96.9	989970	4.6	337311	101	662689	21246 97717	44
17	327862	96.8	989942	4.6	337919	101	662081	21275 97711	43
18	328442	96.6	989915	4.6	338527	101	661473	21303 97705	42
19	329021	96.5	989887	4.6	339133	101	660867	21331 97698	41
20	329599	96.4	989860	4.6	339739	101	660261	21360 97692	40
21	9.330176	96.2	9.989832	4.6	9.340344	101	10.659056	21388 97686	39
22	330753	96.0	989804	4.6	340948	101	659052	21417 97680	38
23	331329	95.8	989777	4.6	341552	100	658448	21445 97673	37
24	331903	95.7	989749	4.6	342155	100	657845	21474 97667	36
25	332478	95.6	989721	4.7	342757	100	657243	21502 97661	35
26	333051	95.4	989693	4.7	343358	100	656642	21530 97655	34
27	333624	95.3	989665	4.7	343958	100	656042	21559 97648	33
28	334195	95.1	989637	4.7	344558	100	655442	21587 97642	32
29	334766	95.0	989609	4.7	345157	100	654843	21616 97636	31
30	335337	94.9	989582	4.7	345755	100	654245	21644 97630	30
31	9.335905	94.8	9.989553	4.7	9.346353	99.4	10.653047	21672 97623	29
32	336475	94.6	989525	4.7	346949	99.3	653051	21701 97617	28
33	337043	94.5	989497	4.7	347545	99.2	652455	21729 97611	27
34	337610	94.4	989469	4.7	348141	99.1	651859	21758 97604	26
35	338176	94.3	989441	4.7	348735	99.0	651265	21786 97598	25
36	338742	94.1	989413	4.7	349329	98.8	650671	21814 97592	24
37	339306	94.0	989384	4.7	349922	98.7	650078	21843 97585	23
38	339871	93.9	989356	4.7	350514	98.6	649486	21871 97579	22
39	340434	93.7	989328	4.7	351106	98.5	648894	21899 97573	21
40	340996	93.6	989300	4.7	351697	98.3	648303	21928 97566	20
41	9.341558	93.5	9.989271	4.7	9.352287	98.2	10.647713	21956 97560	19
42	342119	93.4	989243	4.7	352876	98.1	647124	21985 97553	18
43	342679	93.2	989214	4.7	353465	98.0	646535	22013 97547	17
44	343239	93.1	989186	4.7	354053	97.9	645947	22041 97541	16
45	343797	93.0	989157	4.7	354640	97.7	645360	22070 97534	15
46	344355	92.9	989128	4.8	355227	97.6	644773	22098 97528	14
47	344912	92.7	989100	4.8	355813	97.5	644187	22126 97521	13
48	345469	92.6	989071	4.8	356398	97.4	643602	22155 97515	12
49	346024	92.5	989042	4.8	356982	97.3	643018	22183 97508	11
50	346579	92.4	989014	4.8	357566	97.1	642434	22212 97502	10
51	9.347134	92.2	9.988985	4.8	9.358149	97.0	10.641851	22240 97496	9
52	347687	92.1	988956	4.8	358731	96.9	641269	22268 97489	8
53	348240	92.0	988927	4.8	359313	96.8	640687	22297 97483	7
54	348792	91.9	988898	4.8	359893	96.7	640107	22325 97476	6
55	349343	91.7	988869	4.8	360474	96.6	639526	22353 97470	5
56	349893	91.6	988840	4.8	361053	96.5	638947	22382 97463	4
57	3 0443	91.5	988811	4.9	361632	96.4	638368	22410 97457	3
58	3 5992	91.4	988782	4.9	362210	96.3	637790	22438 97450	2
59	3 51540	91.3	988753	4.9	362787	96.2	637213	22467 97444	1
60	352088		988724	4.9	363364	96.1	636636	22495 97437	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine	N. cos.	
0	9.352088		9.988724		9.363364		10.636636	22495	97437	60
1	352635	91.1	988695	4.9	363940	96.0	636060	22523	97430	59
2	353181	91.0	988666	4.9	364515	95.9	635485	22552	97424	58
3	353726	90.9	988636	4.9	365090	95.8	634910	22580	97417	57
4	354271	90.8	988607	4.9	365664	95.7	634336	22608	97411	56
5	354815	90.7	988578	4.9	366237	95.6	633763	22637	97404	55
6	355358	90.5	988548	4.9	366810	95.4	633190	22665	97398	54
7	355901	90.4	988519	4.9	367382	95.3	632618	22693	97391	53
8	356443	90.3	988489	4.9	367953	95.2	632047	22722	97384	52
9	356984	90.2	988460	4.9	368524	95.1	631476	22750	97378	51
10	357524	90.1	988430	4.9	369094	95.0	630906	22778	97371	50
11	9.358064	89.9	9.988401	4.9	9.369663	94.9	10.630337	22807	97365	49
12	358603	89.8	988371	4.9	370232	94.8	629768	22835	97358	48
13	359141	89.7	988342	4.9	370799	94.6	629201	22863	97351	47
14	359678	89.6	988312	4.9	371367	94.5	628633	22892	97345	46
15	360216	89.5	988282	5.0	371933	94.4	628067	22920	97338	45
16	360752	89.3	988252	5.0	372499	94.3	627501	22948	97331	44
17	361287	89.2	988223	5.0	373064	94.2	626936	22977	97325	43
18	361822	89.1	988193	5.0	373629	94.1	626371	23005	97318	42
19	362356	89.0	988163	5.0	374193	94.0	625807	23033	97311	41
20	362889	88.9	988133	5.0	374756	93.9	625244	23062	97304	40
21	9.363422	88.8	9.988103	5.0	9.375319	93.8	10.624681	23090	97298	39
22	363954	88.7	988073	5.0	375881	93.7	624119	23118	97291	38
23	364485	88.5	988043	5.0	376442	93.5	623558	23146	97284	37
24	365016	88.4	988013	5.0	377003	93.4	622997	23175	97278	36
25	365546	88.3	987983	5.0	377563	93.3	622437	23203	97271	35
26	366075	88.2	987953	5.0	378122	93.2	621878	23231	97264	34
27	366604	88.1	987922	5.0	378681	93.1	621319	23260	97257	33
28	367131	88.0	987892	5.0	379239	93.0	620761	23288	97251	32
29	367659	87.9	987862	5.0	379797	92.9	620203	23316	97244	31
30	368185	87.7	987832	5.0	380354	92.8	619646	23345	97237	30
31	9.368711	87.6	9.987801	5.1	9.380910	92.7	10.619090	23373	97230	29
32	369236	87.5	987771	5.1	381466	92.6	618534	23401	97223	28
33	369761	87.4	987740	5.1	382020	92.5	617980	23429	97217	27
34	370285	87.3	987710	5.1	382575	92.4	617425	23458	97210	26
35	370805	87.2	987679	5.1	383129	92.3	616871	23486	97203	25
36	371330	87.1	987649	5.1	383682	92.2	616318	23514	97196	24
37	371852	87.0	987618	5.1	384234	92.1	615766	23542	97189	23
38	372373	86.9	987588	5.1	384786	92.0	615214	23570	97182	22
39	372894	86.7	987557	5.1	385337	91.9	614663	23599	97176	21
40	373414	86.6	987526	5.1	385888	91.8	614112	23627	97169	20
41	9.373933	86.5	9.987496	5.1	9.386438	91.7	10.613562	23656	97162	19
42	374452	86.4	987465	5.1	386438	91.5	613013	23684	97155	18
43	374970	86.3	987434	5.1	387036	91.4	612464	23712	97148	17
44	375487	86.2	987403	5.1	387634	91.3	611916	23740	97141	16
45	376003	86.1	987372	5.2	388231	91.2	611369	23769	97134	15
46	376519	86.0	987341	5.2	388828	91.1	610822	23797	97127	14
47	377035	85.9	987310	5.2	389424	91.0	610276	23826	97120	13
48	377549	85.8	987279	5.2	390020	90.9	609730	23855	97113	12
49	378063	85.7	987248	5.2	390615	90.8	609185	23882	97106	11
50	378577	85.6	987217	5.2	391210	90.7	608640	23910	97100	10
51	9.379089	85.4	9.987186	5.2	9.391903	90.6	10.605097	23938	97093	9
52	379601	85.3	987155	5.2	392447	90.5	607553	23966	97086	8
53	380113	85.2	987124	5.2	392989	90.4	607011	23995	97079	7
54	380624	85.1	987092	5.2	393531	90.3	606469	24023	97072	6
55	381134	85.0	987061	5.2	394073	90.2	605927	24051	97065	5
56	381643	84.9	987030	5.2	394614	90.1	605386	24079	97058	4
57	382152	84.8	986998	5.2	395154	90.0	604846	24108	97051	3
58	382661	84.7	986967	5.2	395694	89.9	604306	24136	97044	2
59	383168	84.6	986936	5.2	396233	89.8	603767	24164	97037	1
60	383675	84.5	986904	5.2	396771	89.7	603229	24192	97030	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	7

TABLE II. Log. Sines and Tangents. (14°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.383675	84.4	9.986904	5.2	9.396771	89.6	10.603229	24192	97030	60
1	384182	84.3	986873	5.3	397309	89.6	602691	24220	97023	59
2	384687	84.2	986841	5.3	397846	89.5	602154	24249	97015	58
3	385192	84.1	986809	5.3	398383	89.5	601617	24277	97008	57
4	385697	84.0	986778	5.3	398919	89.4	601081	24305	97001	56
5	386201	83.9	986746	5.3	399455	89.3	600545	24333	96994	55
6	386704	83.8	986714	5.3	399990	89.2	600010	24362	96987	54
7	387207	83.7	986683	5.3	400524	89.1	599476	24390	96980	53
8	387709	83.6	986651	5.3	401058	88.9	598942	24418	96973	52
9	388210	83.5	986619	5.3	401591	88.8	598409	24446	96966	51
10	388711	83.4	986587	5.3	402124	88.7	597876	24474	96959	50
11	9.389211	83.3	9.986555	5.3	9.402656	88.6	10.597344	24503	96952	49
12	389711	83.2	986523	5.3	403187	88.5	596813	24531	96945	48
13	390210	83.1	986491	5.3	403718	88.4	596282	24559	96937	47
14	390708	83.0	986459	5.3	404249	88.3	595751	24587	96930	46
15	391206	82.8	986427	5.3	404778	88.2	595222	24615	96923	45
16	391703	82.7	986395	5.3	405308	88.1	594692	24644	96916	44
17	392199	82.6	986363	5.4	405836	88.0	594164	24672	96909	43
18	392695	82.5	986331	5.4	406364	87.9	593636	24700	96902	42
19	393191	82.4	986299	5.4	406892	87.8	593108	24728	96894	41
20	393685	82.3	986266	5.4	407419	87.7	592581	24756	96887	40
21	9.394179	82.2	9.986234	5.4	9.407945	87.6	10.592055	24784	96880	39
22	394673	82.1	986202	5.4	408471	87.5	591529	24813	96873	38
23	395166	82.0	986169	5.4	408997	87.4	591003	24841	96866	37
24	395658	81.9	986137	5.4	409521	87.3	590479	24869	96858	36
25	396150	81.8	986104	5.4	410045	87.2	589955	24897	96851	35
26	396641	81.7	986072	5.4	410569	87.1	589431	24925	96844	34
27	397132	81.6	986039	5.4	411092	87.0	588908	24954	96837	33
28	397621	81.5	986007	5.4	411615	86.9	588385	24982	96829	32
29	398111	81.4	985974	5.4	412137	86.8	587863	25010	96822	31
30	398600	81.3	985942	5.4	412658	86.7	587342	25038	96815	30
31	9.399088	81.2	9.985909	5.5	9.413179	86.6	10.586821	25066	96807	29
32	399575	81.1	985876	5.5	413699	86.5	586301	25094	96800	28
33	400062	81.0	985843	5.5	414219	86.4	585781	25122	96793	27
34	400549	80.9	985811	5.5	414738	86.3	585262	25151	96786	26
35	401035	80.8	985778	5.5	415257	86.2	584743	25179	96778	25
36	401520	80.7	985745	5.5	415775	86.1	584225	25207	96771	24
37	402005	80.6	985712	5.5	416293	86.0	583707	25235	96764	23
38	402489	80.5	985679	5.5	416810	85.9	583190	25263	96756	22
39	402972	80.4	985646	5.5	417326	85.8	582674	25291	96749	21
40	403455	80.3	985613	5.5	417842	85.7	582158	25320	96742	20
41	9.403938	80.2	9.985580	5.5	9.418358	85.6	10.581642	25348	96734	19
42	404420	80.1	985547	5.5	418873	85.5	581127	25376	96727	18
43	404901	80.0	985514	5.5	419387	85.4	580613	25404	96719	17
44	405382	79.9	985480	5.5	419901	85.3	580099	25432	96712	16
45	405862	79.8	985447	5.5	420415	85.2	579585	25460	96705	15
46	406341	79.7	985414	5.5	420927	85.1	579073	25488	96697	14
47	406820	79.6	985380	5.5	421440	85.0	578560	25516	96690	13
48	407299	79.5	985347	5.5	421952	84.9	578048	25545	96682	12
49	407777	79.4	985314	5.5	422463	84.8	577537	25573	96675	11
50	408254	79.3	985280	5.5	422974	84.7	577026	25601	96667	10
51	9.408731	79.2	9.985247	5.6	9.423484	84.6	10.576516	25629	96660	9
52	409207	79.1	985213	5.6	423493	84.5	576507	25657	96653	8
53	409682	79.0	985180	5.6	424003	84.4	575997	25685	96645	7
54	410157	78.9	985146	5.6	424511	84.3	575489	25713	96638	6
55	410632	78.8	985113	5.6	425019	84.2	574981	25741	96630	5
56	411106	78.7	985079	5.6	425527	84.1	574474	25769	96623	4
57	411579	78.6	985045	5.6	426034	84.0	573966	25797	96615	3
58	412052	78.5	985011	5.6	426541	83.9	573459	25825	96608	2
59	412524	78.4	984978	5.6	427047	83.8	572952	25853	96600	1
60	412996	78.3	984944	5.6	427552	83.7	572445	25881	96593	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cosine.	
0	9.412993	78.5	9.984944	5.7	9.428052	84.2	10.571948	25882	96593	60
1	413467	78.4	984910	5.7	428557	84	571443	25910	96585	59
2	413938	78.3	984876	5.7	429062	84	570938	25935	96575	58
3	414408	78.3	984842	5.7	429565	83.9	570434	25960	96570	57
4	414878	78.2	984808	5.7	430070	83.8	569930	25994	96562	56
5	415347	78.1	984774	5.7	430573	83.8	569427	26022	96555	55
6	415815	78.0	984740	5.7	431075	83.7	568925	26050	96547	54
7	416283	77.9	984706	5.7	431577	83.6	568423	26079	96540	53
8	416751	77.8	984672	5.7	432079	83.5	567921	26107	96532	52
9	417217	77.7	984637	5.7	432580	83.4	567420	26135	96524	51
10	417684	77.6	984603	5.7	433080	83.3	566920	26163	96517	50
11	9.418150	77.5	9.984569	5.7	9.433580	83.2	10.566420	26191	96509	49
12	418615	77.4	984535	5.7	434080	83.2	566420	26219	96502	48
13	419079	77.3	984500	5.7	434579	83.1	565921	26247	96494	47
14	419544	77.3	984466	5.7	435078	83.0	565422	26275	96486	46
15	420007	77.2	984432	5.8	435576	82.9	564924	26303	96479	45
16	420470	77.1	984397	5.8	436073	82.8	564427	26331	96471	44
17	420933	77.0	984363	5.8	436570	82.8	563930	26359	96463	43
18	421395	76.9	984328	5.8	437067	82.7	563433	26387	96456	42
19	421857	76.8	984294	5.8	437563	82.6	562937	26415	96448	41
20	422318	76.7	984259	5.8	438059	82.5	562441	26443	96440	40
21	9.422778	76.7	9.984224	5.8	9.438554	82.4	10.561446	26471	96433	39
22	423238	76.6	984190	5.8	439048	82.3	560952	26500	96425	38
23	423697	76.5	984155	5.8	439543	82.3	560457	26528	96417	37
24	424156	76.4	984120	5.8	440036	82.2	559964	26556	96410	36
25	424615	76.3	984085	5.8	440529	82.1	559471	26584	96402	35
26	425073	76.2	984050	5.8	441022	82.0	558978	26612	96394	34
27	425530	76.1	984015	5.8	441514	81.9	558486	26640	96386	33
28	425987	76.0	983981	5.8	442006	81.9	557994	26668	96379	32
29	426443	76.0	983946	5.8	442497	81.8	557503	26696	96371	31
30	426899	76.0	983911	5.8	442988	81.7	557012	26724	96363	30
31	9.427354	75.8	9.983875	5.8	9.443479	81.6	10.556521	26752	96355	29
32	427809	75.7	983840	5.9	443968	81.6	556032	26780	96347	28
33	428263	75.6	983805	5.9	444458	81.5	555542	26808	96340	27
34	428717	75.5	983770	5.9	444947	81.4	555053	26836	96332	26
35	429170	75.4	983735	5.9	445435	81.3	554565	26864	96324	25
36	429623	75.3	983.00	5.9	445923	81.2	554077	26892	96316	24
37	430075	75.2	983664	5.9	446411	81.2	553589	26920	96308	23
38	430527	75.2	983629	5.9	446898	81.1	553102	26948	96301	22
39	430978	75.1	983594	5.9	447384	81.0	552616	26976	96293	21
40	431429	75.0	983558	5.9	447870	80.9	552130	27004	96285	20
41	9.431849	74.9	9.983523	5.9	9.448356	80.9	10.551644	27032	96277	19
42	432329	74.9	983487	5.9	448841	80.8	551159	27060	96269	18
43	432778	74.8	983452	5.9	449326	80.7	550674	27088	96261	17
44	433226	74.7	983416	5.9	449810	80.6	550190	27116	96253	16
45	433675	74.6	983381	5.9	450294	80.6	549706	27144	96245	15
46	434122	74.5	983345	5.9	450777	80.5	549223	27172	96238	14
47	434569	74.4	983309	5.9	451260	80.4	548740	27200	96230	13
48	435016	74.4	983273	6.0	451743	80.3	548257	27228	96222	12
49	435462	74.3	983238	6.0	452225	80.2	547775	27256	96214	11
50	435908	74.2	983202	6.0	452706	80.2	547294	27284	96206	10
51	9.436353	74.1	9.983166	6.0	9.453187	80.1	10.546813	27312	96198	9
52	436798	74.0	983130	6.0	453668	80.0	546332	27340	96190	8
53	437242	74.0	983094	6.0	454148	79.9	545852	27368	96182	7
54	437686	73.9	983058	6.0	454628	79.9	545372	27396	96174	6
55	438129	73.8	983022	6.0	455107	79.8	544893	27424	96166	5
56	438572	73.7	982986	6.0	455586	79.7	544414	27452	96158	4
57	439014	73.6	982950	6.0	456064	79.6	543936	27480	96150	3
58	439456	73.6	982914	6.0	456542	79.6	543458	27508	96142	2
59	439897	73.5	982878	6.0	457019	79.5	542981	27536	96134	1
60	440338	73.5	982842	6.0	457496	79.5	542504	27564	96126	0
	Cosine.		Sine.		Cotang.		Tang.	N. cosine.	N. sine.	

TABLE II. Log. Sines and Tangents. (16°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.410338	73.4	9.982842	6.0	9.457496	79.4	10.542504	27564	96126	60
1	440778	73.3	982505	6.0	457973	79.3	542927	27592	96118	59
2	441218	73.2	982769	6.1	458449	79.3	541551	27620	96110	58
3	441658	73.1	982733	6.1	458925	79.2	541075	27648	96102	57
4	442096	73.0	982696	6.1	459400	79.2	540600	27676	96094	56
5	442535	73.0	982660	6.1	459875	79.1	540125	27704	96086	55
6	442973	72.9	982624	6.1	460349	79.0	539651	27731	96078	54
7	443410	72.8	982587	6.1	460823	79.0	539177	27759	96070	53
8	443847	72.7	982551	6.1	461297	78.9	538703	27787	96062	52
9	444284	72.7	982514	6.1	461770	78.8	538230	27815	96054	51
10	444720	72.6	982477	6.1	462242	78.9	537758	27843	96046	50
11	9.445155	72.5	9.982441	6.1	9.462714	78.6	10.537286	27871	96037	49
12	445590	72.4	982404	6.1	463186	78.6	536814	27899	96029	48
13	446025	72.3	982367	6.1	463658	78.5	536342	27927	96021	47
14	446459	72.3	982331	6.1	464129	78.5	535871	27955	96013	46
15	446893	72.2	982294	6.1	464599	78.4	535401	27983	96005	45
16	447326	72.2	982257	6.1	465069	78.3	534931	28011	95997	44
17	447759	72.1	982220	6.1	465539	78.3	534461	28039	95989	43
18	448191	72.0	982183	6.2	466008	78.2	533992	28067	95981	42
19	448623	72.0	982146	6.2	466476	78.1	533524	28095	95972	41
20	449054	71.9	982109	6.2	466945	78.0	533055	28123	95964	40
21	9.449485	71.8	9.982072	6.2	9.467413	78.0	10.532587	28150	95956	39
22	449915	71.7	982035	6.2	467880	77.9	532120	28178	95948	38
23	450345	71.6	981998	6.2	468347	77.8	531653	28206	95940	37
24	450775	71.6	981961	6.2	468814	77.8	531186	28234	95931	36
25	451204	71.5	981924	6.2	469280	77.7	530720	28262	95923	35
26	451632	71.4	981886	6.2	469746	77.6	530254	28290	95915	34
27	452060	71.3	981849	6.2	470211	77.5	529789	28318	95907	33
28	452488	71.3	981812	6.2	470676	77.5	529324	28346	95898	32
29	452915	71.2	981774	6.2	471141	77.4	528859	28374	95890	31
30	453342	71.1	981737	6.2	471605	77.3	528395	28402	95882	30
31	9.453768	71.0	9.981699	6.2	9.472068	77.3	10.527932	28429	95874	29
32	454194	71.0	981662	6.3	472532	77.2	527468	28457	95865	28
33	454619	70.9	981625	6.3	472995	77.1	527005	28485	95857	27
34	455044	70.8	981587	6.3	473457	77.1	526543	28513	95849	26
35	455469	70.7	981549	6.3	473919	77.0	526081	28541	95841	25
36	455893	70.7	981512	6.3	474381	76.9	525619	28569	95832	24
37	456316	70.6	981474	6.3	474842	76.9	525158	28597	95824	23
38	456739	70.5	981436	6.3	475303	76.8	524697	28625	95816	22
39	457162	70.4	981399	6.3	475763	76.8	524237	28653	95807	21
40	457584	70.4	981361	6.3	476223	76.7	523777	28680	95799	20
41	9.458000	70.3	9.981323	6.3	9.476683	76.6	10.523317	28708	95791	19
42	458427	70.2	981285	6.3	477142	76.5	523317	28736	95782	18
43	458848	70.1	981247	6.3	477601	76.5	522858	28764	95774	17
44	459268	70.1	981209	6.3	478059	76.4	522399	28792	95766	16
45	459688	70.0	981171	6.3	478517	76.3	521941	28820	95757	15
46	460108	69.9	981133	6.3	478975	76.3	521483	28848	95749	14
47	460527	69.8	981095	6.4	479432	76.2	521025	28876	95741	13
48	460946	69.8	981057	6.4	479889	76.1	520568	28904	95732	12
49	461364	69.7	981019	6.4	480345	76.1	520111	28932	95724	11
50	461782	69.6	980981	6.4	480801	76.0	519655	28960	95715	10
51	9.462199	69.5	9.980942	6.4	9.481257	75.9	10.519199	28988	95707	9
52	462616	69.5	980904	6.4	481712	75.9	518743	29016	95698	8
53	463032	69.4	980866	6.4	482167	75.8	518288	29044	95690	7
54	463448	69.3	980827	6.4	482621	75.7	517833	29072	95681	6
55	463864	69.3	980789	6.4	483075	75.7	517379	29100	95673	5
56	464279	69.2	980750	6.4	483529	75.6	516925	29128	95664	4
57	464694	69.1	980712	6.4	483982	75.5	516471	29156	95656	3
58	465108	69.0	980673	6.4	484435	75.5	516018	29184	95647	2
59	465522	69.0	980635	6.4	484887	75.4	515565	29212	95639	1
60	465935	68.9	980596	6.4	485339	75.3	515113	29240	95630	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

<i>r</i>	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine	N. cos.	
0	9.465935	68.8	9.980596	6.4	9.485339	75.3	10.514661	29237	95630	60
1	466348	68.8	980558	6.4	485791	75.2	514209	29265	95622	59
2	466761	68.8	980519	6.4	486242	75.1	513758	29293	95613	58
3	467173	68.7	980480	6.5	486693	75.1	513307	29321	95605	57
4	467585	68.6	980442	6.5	487143	75.1	512857	29348	95596	56
5	467996	68.5	980403	6.5	487593	75.0	512407	29376	95588	55
6	468407	68.5	980364	6.5	488043	74.9	511957	29404	95579	54
7	468817	68.4	980325	6.5	488492	74.9	511508	29432	95571	53
8	469227	68.3	980286	6.5	488941	74.8	511059	29460	95562	52
9	469637	68.3	980247	6.5	489390	74.7	510610	29487	95554	51
10	470046	68.2	980208	6.5	489838	74.7	510162	29515	95545	50
11	9.470455	68.0	9.981169	6.5	9.490286	74.6	10.509714	29543	95536	49
12	470863	68.0	980130	6.5	490733	74.6	509277	29571	95528	48
13	471271	68.0	980091	6.5	491180	74.5	508820	29599	95519	47
14	471679	67.9	980052	6.5	491627	74.4	508373	29626	95511	46
15	472086	67.8	980012	6.5	492073	74.4	507927	29654	95502	45
16	472492	67.8	979973	6.5	492519	74.3	507481	29682	95493	44
17	472898	67.7	979934	6.5	492965	74.3	507035	29710	95485	43
18	473304	67.6	979895	6.6	493410	74.2	506590	29737	95476	42
19	473710	67.6	979855	6.6	493854	74.1	506146	29765	95467	41
20	474115	67.5	979816	6.6	494299	74.0	505701	29793	95459	40
21	9.474519	67.4	9.979776	6.6	9.494743	74.0	10.505257	29821	95450	39
22	474923	67.4	979737	6.6	495186	74.0	504814	29849	95441	38
23	475327	67.3	979697	6.6	495630	73.9	504370	29876	95433	37
24	475730	67.2	979658	6.6	496073	73.8	503927	29904	95424	36
25	476133	67.2	979618	6.6	496515	73.7	503485	29932	95415	35
26	476536	67.1	979579	6.6	496957	73.7	503043	29960	95407	34
27	476938	67.0	979539	6.6	497399	73.6	502601	29988	95398	33
28	477340	66.9	979499	6.6	497841	73.6	502159	30015	95389	32
29	477741	66.9	979459	6.6	498282	73.5	501718	30043	95380	31
30	478142	66.8	979420	6.6	498722	73.4	501278	30071	95372	30
31	9.478542	66.7	9.979380	6.6	9.499163	73.3	10.500837	30098	95363	29
32	478942	66.7	979340	6.6	499603	73.3	500837	30126	95354	28
33	479342	66.6	979300	6.6	500042	73.2	499958	30154	95345	27
34	479741	66.5	979260	6.7	500481	73.2	499519	30182	95337	26
35	480140	66.5	979220	6.7	500920	73.1	499080	30209	95328	25
36	480539	66.4	979180	6.7	501359	73.1	498641	30237	95319	24
37	480937	66.3	979140	6.7	501797	73.0	498203	30265	95310	23
38	481334	66.3	979100	6.7	502235	73.0	497765	30292	95301	22
39	481731	66.2	979059	6.7	502672	72.9	497328	30320	95293	21
40	482128	66.1	979019	6.7	503109	72.8	496891	30348	95284	20
41	9.482525	66.0	9.978979	6.7	9.503546	72.8	10.496454	30376	95275	19
42	482921	66.0	978939	6.7	503982	72.7	496018	30403	95266	18
43	483316	65.9	978898	6.7	504418	72.7	495582	30431	95257	17
44	483712	65.9	978858	6.7	504854	72.6	495146	30459	95248	16
45	484107	65.8	978817	6.7	505289	72.5	494711	30486	95240	15
46	484501	65.7	978777	6.7	505724	72.5	494276	30514	95231	14
47	484895	65.7	978736	6.7	506159	72.4	493841	30542	95222	13
48	485289	65.6	978696	6.8	506593	72.4	493407	30570	95213	12
49	485682	65.5	978655	6.8	507027	72.3	492973	30597	95204	11
50	486075	65.5	978615	6.8	507460	72.2	492540	30625	95195	10
51	9.486467	65.4	9.978574	6.8	9.507893	72.2	10.492107	30653	95186	9
52	486860	65.3	978533	6.8	508326	72.1	491674	30680	95177	8
53	487251	65.2	978493	6.8	508759	72.1	491241	30708	95168	7
54	487643	65.2	978452	6.8	509191	72.0	490809	30736	95159	6
55	488034	65.1	978411	6.8	509622	71.9	490378	30765	95150	5
56	488424	65.1	978370	6.8	510054	71.9	489946	30793	95142	4
57	488814	65.0	978329	6.8	510485	71.8	489515	30821	95133	3
58	489204	65.0	978288	6.8	510916	71.8	489084	30849	95124	2
59	489593	64.9	978247	6.8	511346	71.7	488654	30877	95115	1
60	489982	64.8	978206	6.8	511776	71.6	488224	30905	95106	0
	Cosine		Sine.		Cotang.		Tang.	N. cos.	N. sine.	<i>r</i>



TABLE II. Log. Sines and Tangents. (18°) Natural Sines.

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	9.489982	64.8	9.978206	6.8	9.511776	71.6	10.488224	30902	95106	60
1	490371	64.8	978165	6.8	512206	71.6	487794	30929	95097	59
2	490759	64.7	978124	6.8	512635	71.5	487365	30957	95088	58
3	491147	64.6	978083	6.9	513064	71.4	486936	30985	95079	57
4	491535	64.6	978042	6.9	513493	71.4	486507	31012	95070	56
5	491922	64.5	978001	6.9	513921	71.3	486079	31040	95061	55
6	492308	64.4	977959	6.9	514349	71.3	485651	31068	95052	54
7	492695	64.4	977918	6.9	514777	71.2	485223	31095	95043	53
8	493081	64.3	977877	6.9	515204	71.2	484796	31123	95034	52
9	493466	64.2	977835	6.9	515631	71.1	484369	31151	95024	51
10	493851	64.2	977794	6.9	516057	71.0	483943	31178	95015	50
11	9.494236	64.1	9.977752	6.9	9.516484	71.0	10.483516	31206	95006	49
12	494621	64.1	977711	6.9	516910	70.9	483500	31233	94997	48
13	495005	64.0	977669	6.9	517335	70.9	482665	31261	94988	47
14	495388	63.9	977628	6.9	517761	70.8	482239	31289	94979	46
15	495772	63.9	977586	6.9	518185	70.8	481815	31316	94970	45
16	496154	63.8	977544	7.0	518610	70.7	481390	31344	94961	44
17	496537	63.8	977503	7.0	519034	70.6	480966	31372	94952	43
18	496919	63.7	977461	7.0	519458	70.6	480542	31399	94943	42
19	497301	63.7	977419	7.0	519882	70.5	480118	31427	94933	41
20	497682	63.6	977377	7.0	520305	70.5	479695	31454	94924	40
21	9.498064	63.5	9.977335	7.0	9.520728	70.4	10.479272	31482	94915	39
22	498444	63.4	977293	7.0	521151	70.3	478849	31510	94906	38
23	498825	63.4	977251	7.0	521573	70.3	478427	31537	94897	37
24	499204	63.3	977209	7.0	521995	70.3	478005	31565	94888	36
25	499584	63.2	977167	7.0	522417	70.2	477583	31593	94878	35
26	499963	63.2	977125	7.0	522838	70.2	477162	31620	94869	34
27	500342	63.1	977083	7.0	523259	70.1	476741	31648	94860	33
28	500721	63.1	977041	7.0	523680	70.1	476320	31675	94851	32
29	501099	63.0	976999	7.0	524100	70.0	475900	31703	94842	31
30	501476	62.9	976957	7.0	524520	69.9	475480	31730	94833	30
31	9.501854	62.9	9.976914	7.0	9.524939	69.9	10.475061	31758	94823	29
32	502231	62.8	976872	7.1	525359	69.8	474641	31786	94814	28
33	502607	62.8	976830	7.1	525778	69.8	474222	31813	94805	27
34	502984	62.7	976787	7.1	526197	69.7	473803	31841	94795	26
35	503360	62.6	976745	7.1	526615	69.6	473385	31868	94786	25
36	503735	62.6	976702	7.1	527033	69.6	472967	31896	94777	24
37	504110	62.5	976660	7.1	527451	69.6	472549	31923	94768	23
38	504485	62.5	976617	7.1	527868	69.5	472132	31951	94758	22
39	504860	62.4	976574	7.1	528285	69.5	471715	31979	94749	21
40	505234	62.3	976532	7.1	528702	69.4	471298	32006	94740	20
41	9.505608	62.3	9.976489	7.1	9.529119	69.3	10.470881	32034	94730	19
42	505981	62.2	976446	7.1	529535	69.3	470465	32061	94721	18
43	506354	62.2	976404	7.1	529950	69.3	470050	32089	94712	17
44	506727	62.1	976361	7.1	530366	69.2	469634	32116	94702	16
45	507099	62.0	976318	7.1	530781	69.1	469219	32144	94693	15
46	507471	62.0	976275	7.1	531196	69.1	468804	32171	94684	14
47	507843	61.9	976232	7.2	531611	69.0	468389	32199	94674	13
48	508214	61.9	976189	7.2	532025	69.0	467975	32227	94665	12
49	508585	61.8	976146	7.2	532439	68.9	467561	32255	94656	11
50	508956	61.8	976103	7.2	532853	68.9	467147	32282	94646	10
51	9.509326	61.7	9.976060	7.2	9.533266	68.8	10.466734	32309	94637	9
52	509696	61.6	976017	7.2	533679	68.8	466321	32337	94627	8
53	510065	61.6	975974	7.2	534092	68.7	465906	32364	94618	7
54	510434	61.5	975930	7.2	534504	68.7	465490	32392	94609	6
55	510803	61.5	975887	7.2	534916	68.6	465074	32419	94600	5
56	511172	61.4	975844	7.2	535328	68.6	464657	32447	94590	4
57	511540	61.3	975800	7.2	535739	68.5	464241	32474	94580	3
58	511907	61.3	975757	7.2	536150	68.5	463825	32502	94571	2
59	512275	61.2	975714	7.2	536561	68.4	463409	32529	94561	1
60	512642	61.2	975670	7.2	536972		463028	32555	94552	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	9.512642	61.2	9.975370	7.3	9.536972	68.4	10.463028	32557	94552	60
1	513309	61.1	975627	7.3	537382	68.3	462618	32584	94542	59
2	513375	61.1	975583	7.3	537792	68.3	462208	32612	94533	58
3	513741	61.0	975539	7.3	538202	68.2	461798	32639	94523	57
4	514107	60.9	975496	7.3	538611	68.2	461389	32667	94514	56
5	514472	60.9	975452	7.3	539020	68.1	460980	32694	94504	55
6	514837	60.8	975408	7.3	539429	68.1	460571	32722	94495	54
7	515202	60.8	975365	7.3	539837	68.0	460163	32749	94485	53
8	515566	60.7	975321	7.3	540245	68.0	459755	32777	94476	52
9	515930	60.7	975277	7.3	540653	67.9	459347	32804	94466	51
10	516294	60.6	975233	7.3	541061	67.9	458939	32832	94457	50
11	9.516657	60.5	9.975189	7.3	9.541468	67.8	10.458532	32859	94447	49
12	517020	60.5	975145	7.3	541875	67.8	458525	32888	94438	48
13	517382	60.4	975101	7.3	542281	67.7	457719	32914	94428	47
14	517745	60.4	975057	7.3	542688	67.7	457312	32942	94418	46
15	518107	60.3	975013	7.3	543094	67.6	456906	32969	94409	45
16	518468	60.3	974969	7.4	543499	67.6	456501	32997	94399	44
17	518829	60.2	974925	7.4	543905	67.5	456095	33024	94390	43
18	519190	60.1	974880	7.4	544310	67.5	455690	33051	94380	42
19	519551	60.1	974836	7.4	544715	67.4	455285	33079	94370	41
20	519911	60.0	974792	7.4	545119	67.4	454881	33106	94361	40
21	9.520271	60.0	9.974748	7.4	9.545524	67.3	10.454476	33134	94351	39
22	520631	59.9	974703	7.4	545928	67.3	454072	33161	94342	38
23	520990	59.9	974659	7.4	546331	67.2	453669	33189	94332	37
24	521349	59.8	974614	7.4	546735	67.2	453265	33216	94322	36
25	521707	59.8	974570	7.4	547138	67.1	452862	33244	94313	35
26	522066	59.7	974525	7.4	547540	67.1	452460	33271	94303	34
27	522424	59.6	974481	7.4	547943	67.0	452057	33298	94293	33
28	522781	59.6	974436	7.4	548345	67.0	451655	33326	94284	32
29	523138	59.5	974391	7.4	548747	66.9	451253	33353	94274	31
30	523495	59.5	974347	7.5	549149	66.9	450851	33381	94264	30
31	9.523852	59.4	9.974302	7.5	9.549550	66.8	10.450450	33408	94254	29
32	524208	59.4	974257	7.5	549551	66.8	450449	33436	94245	28
33	524564	59.3	974212	7.5	550352	66.7	449648	33463	94235	27
34	524920	59.3	974167	7.5	550752	66.7	449248	33490	94225	26
35	525275	59.2	974122	7.5	551152	66.6	448848	33518	94215	25
36	525630	59.1	974077	7.5	551552	66.6	448448	33545	94206	24
37	525984	59.1	974032	7.5	551952	66.5	448048	33573	94196	23
38	526339	59.0	973987	7.5	552351	66.5	447649	33600	94186	22
39	526693	59.0	973942	7.5	552750	66.5	447250	33627	94176	21
40	527046	58.9	973897	7.5	553149	66.4	446851	33655	94167	20
41	9.527400	58.9	9.973852	7.5	9.553548	66.4	10.446452	33682	94157	19
42	527753	58.8	973807	7.5	553946	66.3	446054	33710	94147	18
43	528105	58.8	973761	7.5	554344	66.3	445656	33737	94137	17
44	528458	58.7	973716	7.6	554741	66.2	445259	33764	94127	16
45	528810	58.7	973671	7.6	555139	66.2	444861	33792	94118	15
46	529161	58.6	973625	7.6	555536	66.1	444464	33819	94108	14
47	529513	58.6	973580	7.6	555933	66.1	444067	33846	94098	13
48	529864	58.5	973535	7.6	556329	66.0	443671	33874	94088	12
49	530215	58.5	973489	7.6	556725	66.0	443275	33901	94078	11
50	530565	58.4	973444	7.6	557121	65.9	442879	33929	94068	10
51	9.530915	58.4	9.973398	7.6	9.557517	65.9	10.442483	33956	94058	9
52	531265	58.3	973352	7.6	557913	65.9	442087	33983	94049	8
53	531614	58.2	973307	7.6	558308	65.8	441692	34011	94039	7
54	531963	58.2	973261	7.6	558702	65.8	441298	34038	94029	6
55	532312	58.1	973215	7.6	559097	65.7	440903	34065	94019	5
56	532661	58.1	973169	7.6	559491	65.7	440509	34093	94009	4
57	533009	58.0	973124	7.6	559885	65.6	440115	34120	93999	3
58	533357	58.0	973078	7.6	560279	65.6	439721	34147	93989	2
59	533704	57.9	973032	7.6	560673	65.5	439327	34175	93979	1
60	534052	57.9	972986	7.7	561066	65.5	438934	34202	93969	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (20°) Natural Sines.

<i>i</i>	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.534052	57.8	9.972986	7.7	9.561066	65.5	10.438934	34202	93969	60
1	534399	57.7	972940	7.7	561459	65.4	438541	34229	93959	59
2	534745	57.7	972894	7.7	561851	65.4	438149	34257	93949	58
3	535092	57.7	972848	7.7	562244	65.3	437756	34284	93939	57
4	535438	57.6	972802	7.7	562636	65.3	437364	34311	93929	56
5	535783	57.6	972755	7.7	563028	65.3	436972	34339	93919	55
6	536129	57.5	972709	7.7	563419	65.2	436581	34366	93909	54
7	536474	57.4	972663	7.7	563811	65.2	436189	34393	93899	53
8	536818	57.4	972617	7.7	564202	65.1	435798	34421	93889	52
9	537163	57.3	972570	7.7	564592	65.1	435408	34448	93879	51
10	537507	57.3	972524	7.7	564983	65.0	435017	34475	93869	50
11	9.537851	57.2	9.972478	7.7	9.565373	65.0	10.434627	34503	93859	49
12	538194	57.2	972431	7.8	565763	64.9	434237	34530	93849	48
13	538538	57.1	972385	7.8	566153	64.9	433847	34557	93839	47
14	538880	57.1	972338	7.8	566542	64.9	433458	34584	93829	46
15	539223	57.1	972291	7.8	566932	64.8	433068	34612	93819	45
16	539565	57.0	972245	7.8	567320	64.8	432680	34639	93809	44
17	539907	56.9	972198	7.8	567709	64.7	432291	34666	93799	43
18	540249	56.9	972151	7.8	568098	64.7	431902	34694	93789	42
19	540590	56.8	972105	7.8	568486	64.6	431514	34721	93779	41
20	540931	56.8	972058	7.8	568873	64.6	431127	34748	93769	40
21	9.541272	56.7	9.972011	7.8	9.569261	64.5	10.430739	34775	93759	39
22	541613	56.7	971964	7.8	569648	64.5	430352	34803	93748	38
23	541953	56.6	971917	7.8	570035	64.5	429965	34830	93738	37
24	542293	56.6	971870	7.8	570422	64.4	429578	34857	93728	36
25	542632	56.5	971823	7.8	570809	64.4	429191	34884	93718	35
26	542971	56.5	971776	7.8	571195	64.3	428805	34912	93708	34
27	543310	56.4	971729	7.9	571581	64.3	428419	34939	93698	33
28	543649	56.4	971682	7.9	571967	64.2	428033	34966	93688	32
29	543987	56.3	971635	7.9	572352	64.2	427648	34993	93677	31
30	544325	56.3	971588	7.9	572738	64.2	427262	35021	93667	30
31	9.544663	56.2	9.971540	7.9	9.573123	64.1	10.426877	35048	93657	29
32	545000	56.2	971493	7.9	573507	64.1	426493	35075	93647	28
33	545338	56.1	971446	7.9	573892	64.0	426108	35102	93637	27
34	545674	56.1	971398	7.9	574276	64.0	425724	35130	93626	26
35	546011	56.0	971351	7.9	574660	63.9	425340	35157	93616	25
36	546347	56.0	971303	7.9	575044	63.9	424956	35184	93606	24
37	546683	55.9	971256	7.9	575427	63.9	424573	35211	93596	23
38	547019	55.9	971208	7.9	575810	63.8	424190	35239	93585	22
39	547354	55.8	971161	7.9	576193	63.8	423807	35266	93575	21
40	547689	55.8	971113	7.9	576576	63.7	423424	35293	93565	20
41	9.548024	55.7	9.971066	8.0	9.576958	63.7	10.423041	35320	93555	19
42	548359	55.7	971018	8.0	577341	63.6	422659	35347	93544	18
43	548693	55.6	970970	8.0	577723	63.6	422277	35375	93534	17
44	549027	55.6	970922	8.0	578104	63.6	421896	35402	93524	16
45	549360	55.5	970874	8.0	578486	63.5	421514	35429	93514	15
46	549693	55.5	970827	8.0	578867	63.5	421133	35456	93503	14
47	550026	55.4	970779	8.0	579248	63.5	420752	35484	93493	13
48	550359	55.4	970731	8.0	579629	63.4	420371	35511	93483	12
49	550692	55.3	970683	8.0	580009	63.4	419991	35538	93472	11
50	551024	55.3	970635	8.0	580389	63.3	419611	35565	93462	10
51	9.551356	55.2	9.970586	8.0	9.580769	63.3	10.419231	35592	93452	9
52	551687	55.2	970538	8.0	581149	63.2	418851	35619	93441	8
53	552018	55.2	970490	8.0	581528	63.2	418472	35647	93431	7
54	552349	55.1	970442	8.0	581907	63.2	418093	35674	93420	6
55	552680	55.1	970394	8.0	582286	63.1	417714	35701	93410	5
56	553010	55.0	970345	8.1	582665	63.1	417335	35728	93400	4
57	553341	55.0	970297	8.1	583043	63.0	416957	35755	93389	3
58	553670	54.9	970249	8.1	583422	63.0	416578	35782	93379	2
59	554000	54.9	970200	8.1	583800	62.9	416200	35810	93368	1
60	554329	54.9	970152	8.1	584177	62.9	415823	35837	93358	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

°	Sine.		Cosine.		Tang.		Cotang.		N. sine.	N. ccs.
	D. 10"	D. 10"	D. 10"	D. 10"	D. 10"	D. 10"	D. 10"	D. 10"		
0	9.554329	54.8	9.970152	8.1	9.584177	62.9	10.415823	35837	93358	60
1	554658	54.8	970103	8.1	-584555	62.9	415445	35864	93348	59
2	554987	54.7	970055	8.1	584932	62.8	415038	35891	93337	58
3	555315	54.7	970006	8.1	585309	62.8	414691	35918	93327	57
4	555643	54.6	969957	8.1	585686	62.7	414314	35945	93316	56
5	555971	54.6	969909	8.1	586062	62.7	413938	35973	93306	55
6	556299	54.5	969860	8.1	586439	62.7	413561	36000	93295	54
7	556626	54.5	969811	8.1	586815	62.6	413185	36027	93285	53
8	556953	54.4	969762	8.1	587190	62.6	412810	36054	93274	52
9	557280	54.4	969714	8.1	587566	62.6	412434	36081	93264	51
10	557606	54.3	969665	8.1	587941	62.5	412059	36108	93253	50
11	9.557932	54.3	9.969616	8.2	9.588316	62.5	10.411684	36135	93243	49
12	558258	54.3	969567	8.2	588691	62.4	411309	36162	93232	48
13	558583	54.2	969518	8.2	589066	62.4	410934	36190	93222	47
14	558909	54.2	969469	8.2	589440	62.3	410560	36217	93211	46
15	559234	54.1	969420	8.2	589814	62.3	410186	36244	93201	45
16	559558	54.1	969370	8.2	590188	62.3	409812	36271	93190	44
17	559883	54.0	969321	8.2	590562	62.2	409438	36298	93180	43
18	560207	54.0	969272	8.2	590935	62.2	409065	36325	93169	42
19	560531	53.9	969223	8.2	591308	62.2	408692	36352	93159	41
20	560855	53.9	969173	8.2	591681	62.1	408319	36379	93148	40
21	9.561178	53.8	9.969124	8.2	9.592054	62.1	10.407946	36406	93137	39
22	561501	53.8	969075	8.2	592426	62.0	407574	36434	93127	38
23	561824	53.7	969025	8.2	592798	62.0	407202	36461	93116	37
24	562146	53.7	968976	8.2	593170	61.9	406829	36488	93106	36
25	562468	53.6	968926	8.3	593542	61.9	406458	36515	93095	35
26	562790	53.6	968877	8.3	593914	61.8	406086	36542	93084	34
27	563112	53.6	968827	8.3	594285	61.8	405715	36569	93074	33
28	563433	53.5	968777	8.3	594656	61.8	405344	36596	93063	32
29	563755	53.5	968728	8.3	595027	61.7	404973	36623	93052	31
30	564075	53.4	968678	8.3	595398	61.7	404602	36650	93042	30
31	9.564396	53.4	9.968628	8.3	9.595768	61.7	10.404232	36677	93031	29
32	564716	53.3	968578	8.3	596138	61.6	404232	36704	93020	28
33	565036	53.3	968528	8.3	596508	61.6	403862	36731	93010	27
34	565356	53.2	968479	8.3	596878	61.6	403492	36758	92999	26
35	565676	53.2	968429	8.3	597247	61.5	403122	36785	92988	25
36	565995	53.1	968379	8.3	597616	61.5	402753	36812	92978	24
37	566314	53.1	968329	8.3	597985	61.5	402384	36839	92967	23
38	566633	53.1	968278	8.3	598354	61.4	402015	36866	92956	22
39	566951	53.0	968228	8.4	598722	61.4	401646	36893	92945	21
40	567269	53.0	968178	8.4	599091	61.3	401278	36920	92935	20
41	9.567587	52.9	9.968128	8.4	9.599459	61.3	10.400909	36947	92924	19
42	567904	52.9	968078	8.4	599827	61.3	400909	36974	92913	18
43	568222	52.8	968027	8.4	600194	61.2	400541	36999	92902	17
44	568539	52.8	967977	8.4	600562	61.2	399806	37025	92891	16
45	568856	52.8	967927	8.4	600929	61.1	399438	37051	92881	15
46	569172	52.7	967876	8.4	601296	61.1	399071	37077	92870	14
47	569488	52.7	967826	8.4	601662	61.1	398704	37103	92859	13
48	569804	52.6	967775	8.4	602029	61.0	398338	37129	92849	12
49	570120	52.6	967725	8.4	602395	61.0	397971	37155	92838	11
50	570435	52.5	967674	8.4	602761	61.0	397605	37181	92827	10
51	9.570751	52.5	9.967624	8.4	9.603127	60.9	10.397239	37207	92816	9
52	571066	52.4	967573	8.4	603493	60.9	396857	37233	92805	8
53	571380	52.4	967522	8.5	603858	60.9	396502	37259	92794	7
54	571695	52.3	967471	8.5	604223	60.8	396147	37285	92784	6
55	572009	52.3	967421	8.5	604588	60.8	395792	37311	92773	5
56	572323	52.2	967370	8.5	604953	60.7	395437	37337	92762	4
57	572636	52.2	967319	8.5	605317	60.7	395082	37363	92751	3
58	572950	52.1	967268	8.5	605682	60.6	394727	37389	92740	2
59	573263	52.1	967217	8.5	606046	60.6	394372	37415	92729	1
60	573575	52.1	967166	8.5	606410	60.6	394017	37441	92718	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II.

Log. Sines and Tangents. (22°) Natural Sines.

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	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.573575	52.1	9.967166	8.5	9.606410	60.6	10.393590	37461	92718	60
1	573888	52.0	967115	8.5	606773	60.6	393227	37488	92707	59
2	574200	52.0	967064	8.5	607137	60.5	392863	37515	92697	58
3	574512	51.9	967013	8.5	607500	60.5	392500	37542	92686	57
4	574824	51.9	966961	8.5	607863	60.4	392137	37569	92675	56
5	575136	51.9	966910	8.5	608225	60.4	391775	37595	92664	55
6	575447	51.8	966859	8.5	608588	60.4	391412	37622	92653	54
7	575758	51.8	966808	8.5	608950	60.4	391050	37649	92642	53
8	576069	51.7	966756	8.5	609312	60.3	390688	37676	92631	52
9	576379	51.7	966705	8.6	609674	60.3	390326	37703	92620	51
10	576689	51.6	966653	8.6	610036	60.3	389964	37730	92609	50
11	9.576999	51.6	9.966602	8.6	9.610397	60.2	10.389603	37757	92598	49
12	577309	51.6	966550	8.6	610759	60.2	389241	37784	92587	48
13	577618	51.5	966499	8.6	611120	60.2	388880	37811	92576	47
14	577927	51.5	966447	8.6	611480	60.1	388520	37838	92565	46
15	578236	51.4	966395	8.6	611841	60.1	388159	37865	92554	45
16	578545	51.4	966344	8.6	612201	60.1	387799	37892	92543	44
17	578853	51.3	966292	8.6	612561	60.0	387439	37919	92532	43
18	579162	51.3	966240	8.6	612921	60.0	387079	37946	92521	42
19	579470	51.3	966188	8.6	613281	60.0	386719	37973	92510	41
20	579777	51.2	966136	8.6	613641	59.9	386359	37999	92499	40
21	9.580085	51.2	9.966085	8.7	9.614000	59.8	10.386000	38026	92488	39
22	580392	51.1	966033	8.7	614359	59.8	385641	38053	92477	38
23	580699	51.1	965981	8.7	614718	59.8	385282	38080	92466	37
24	581005	51.1	965928	8.7	615077	59.8	384923	38107	92455	36
25	581312	51.0	965876	8.7	615435	59.7	384565	38134	92444	35
26	581618	51.0	965824	8.7	615793	59.7	384207	38161	92433	34
27	581924	50.9	965772	8.7	616151	59.7	383849	38188	92422	33
28	582229	50.9	965720	8.7	616509	59.6	383491	38215	92410	32
29	582535	50.9	965668	8.7	616867	59.6	383133	38242	92399	31
30	582840	50.8	965615	8.7	617224	59.6	382776	38268	92388	30
31	9.583145	50.8	9.965563	8.7	9.617582	59.5	10.382418	38295	92377	29
32	583449	50.7	965511	8.7	617939	59.5	382061	38322	92366	28
33	583754	50.7	965458	8.7	618295	59.5	381705	38349	92355	27
34	584058	50.6	965406	8.7	618652	59.4	381348	38376	92344	26
35	584363	50.6	965353	8.8	619008	59.4	380992	38403	92333	25
36	584665	50.6	965301	8.8	619364	59.4	380636	38430	92322	24
37	584968	50.5	965248	8.8	619721	59.3	380279	38456	92310	23
38	585272	50.5	965195	8.8	620076	59.3	379924	38483	92299	22
39	585574	50.4	965143	8.8	620432	59.2	379568	38510	92287	21
40	585877	50.4	965090	8.8	620787	59.2	379213	38537	92276	20
41	9.586179	50.3	9.965037	8.8	9.621142	59.1	10.378858	38564	92265	19
42	586482	50.3	964984	8.8	621497	59.1	378503	38591	92254	18
43	586783	50.3	964931	8.8	621852	59.1	378148	38617	92243	17
44	587085	50.2	964879	8.8	622207	59.0	377793	38644	92231	16
45	587386	50.2	964826	8.8	622561	59.0	377439	38671	92220	15
46	587688	50.1	964773	8.8	622915	59.0	377085	38698	92209	14
47	587989	50.1	964719	8.8	623269	58.9	376731	38725	92198	13
48	588289	50.1	964666	8.9	623623	58.9	376377	38752	92186	12
49	588590	50.0	964613	8.9	623976	58.9	376024	38778	92175	11
50	588890	50.0	964560	8.9	624330	58.8	375670	38805	92164	10
51	9.589190	49.9	9.964507	8.9	9.624683	58.8	10.375317	38832	92152	9
52	589489	49.9	964454	8.9	624687	58.8	374964	38859	92141	8
53	589789	49.9	964400	8.9	625038	58.7	374612	38886	92130	7
54	590088	49.8	964347	8.9	625391	58.7	374259	38912	92119	6
55	590387	49.8	964294	8.9	625743	58.6	373907	38939	92107	5
56	590686	49.7	964240	8.9	626095	58.6	373555	38966	92096	4
57	590984	49.7	964187	8.9	626447	58.6	373203	38993	92085	3
58	591282	49.7	964133	8.9	626799	58.5	372851	39020	92073	2
59	591580	49.6	964080	8.9	627151	58.5	372499	39046	92062	1
60	5.1878		9.4026		627503		372148	39073	92050	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.591878		9.964026		9.627852		10.372148	39073	92050	60
1	592176	49.6	963972	8.9	628203	58.5	371797	39100	92039	59
2	592473	49.5	963919	8.9	628554	58.5	371446	39127	92028	58
3	592770	49.5	963865	8.9	628905	58.5	371095	39153	92016	57
4	593067	49.5	963811	9.0	629255	58.4	370745	39180	92005	56
5	593363	49.4	963757	9.0	629606	58.4	370394	39207	91994	55
6	593659	49.4	963704	9.0	629956	58.3	370044	39234	91982	54
7	593955	49.3	963650	9.0	630306	58.3	369694	39260	91971	53
8	594251	49.3	963596	9.0	630656	58.3	369344	39287	91959	52
9	594547	49.3	963542	9.0	631005	58.3	368995	39314	91948	51
10	594842	49.2	963488	9.0	631355	58.2	368645	39341	91936	50
11	9.595137	49.1	9.963434	9.0	9.631704	58.2	10.368296	39367	91925	49
12	595432	49.1	963379	9.0	632053	58.1	367947	39394	91914	48
13	595727	49.1	963325	9.0	632401	58.1	367599	39421	91902	47
14	595021	49.0	963271	9.0	632750	58.1	367250	39448	91891	46
15	595315	49.0	963217	9.0	633098	58.0	366902	39474	91879	45
16	595609	48.9	963163	9.0	633447	58.0	366553	39501	91868	44
17	595903	48.9	963108	9.1	633795	58.0	366205	39528	91856	43
18	597196	48.9	963054	9.1	634143	57.9	365857	39555	91845	42
19	597490	48.8	962999	9.1	634490	57.9	365510	39581	91833	41
20	597783	48.8	962945	9.1	634838	57.9	365162	39608	91822	40
21	9.598075	48.7	9.962890	9.1	9.635185	57.8	10.364815	39635	91810	39
22	598368	48.7	962836	9.1	635532	57.8	364468	39661	91799	38
23	598660	48.7	962781	9.1	635879	57.8	364121	39688	91787	37
24	598952	48.6	962727	9.1	636226	57.7	363774	39715	91775	36
25	599244	48.6	962672	9.1	636572	57.7	363428	39741	91764	35
26	599536	48.5	962617	9.1	636919	57.7	363081	39768	91752	34
27	599827	48.5	962562	9.1	637265	57.7	362735	39795	91741	33
28	600118	48.5	962508	9.1	637611	57.6	362389	39822	91729	32
29	600409	48.4	962453	9.1	637956	57.6	362044	39848	91718	31
30	600700	48.4	962398	9.2	638302	57.6	361698	39875	91706	30
31	9.600990	48.4	9.962343	9.2	9.638647	57.5	10.361353	39902	91694	29
32	601280	48.3	962288	9.2	638992	57.5	361008	39928	91683	28
33	601570	48.3	962233	9.2	639337	57.5	360663	39955	91671	27
34	601860	48.2	962178	9.2	639682	57.4	360318	39982	91660	26
35	602150	48.2	962123	9.2	640027	57.4	359973	40008	91648	25
36	602439	48.2	962067	9.2	640371	57.4	359629	40035	91636	24
37	602728	48.1	962012	9.2	640716	57.3	359284	40062	91625	23
38	603017	48.1	961957	9.2	641060	57.3	358940	40088	91613	22
39	603305	48.1	961902	9.2	641404	57.3	358596	40115	91601	21
40	603594	48.0	961846	9.2	641747	57.2	358253	40141	91590	20
41	9.603882	48.0	9.961791	9.2	9.642091	57.2	10.357909	40168	91578	19
42	604170	47.9	961735	9.2	642434	57.2	357566	40195	91566	18
43	604457	47.9	961680	9.2	642777	57.2	357223	40221	91555	17
44	604745	47.9	961624	9.3	643120	57.1	356880	40248	91543	16
45	605032	47.8	961569	9.3	643463	57.1	356537	40275	91531	15
46	605319	47.8	961513	9.3	643806	57.1	356194	40301	91519	14
47	605606	47.8	961458	9.3	644148	57.0	355852	40328	91508	13
48	605892	47.7	961402	9.3	644490	57.0	355510	40355	91496	12
49	60.6179	47.7	961346	9.3	644832	57.0	355168	40381	91484	11
50	60.6465	47.6	961290	9.3	645174	56.9	354826	40408	91472	10
51	9.606751	47.6	9.961235	9.3	9.645516	56.9	10.354484	40434	91461	9
52	607036	47.5	961179	9.3	645857	56.9	354483	40461	91449	8
53	607322	47.5	961123	9.3	646199	56.9	353801	40488	91437	7
54	607607	47.5	961067	9.3	646540	56.8	353460	40514	91425	6
55	607892	47.4	961011	9.3	646881	56.8	353119	40541	91414	5
56	608177	47.4	960955	9.3	647222	56.8	352778	40567	91402	4
57	608461	47.4	960899	9.3	647562	56.7	352438	40594	91390	3
58	608745	47.3	960843	9.4	647903	56.7	352097	40621	91378	2
59	609029	47.3	960786	9.4	648243	56.7	351757	40647	91366	1
60	609313	47.3	960730	9.4	648583	56.7	351417	40674	91355	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II.

Log. Sines and Tangents. (24°) Natural Sines.

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.
0	9.603313		9.990730		9.648583		10.351417	4067491355	60
1	603597	47.3	960374	9.4	648923	56.6	351077	4070091343	59
2	603880	47.2	960618	9.4	649263	56.6	350737	4072791331	58
3	610164	47.2	950561	9.4	649602	56.6	350398	4075491319	57
4	610447	47.2	960505	9.4	649942	56.6	350058	4078191307	56
5	610729	47.1	950448	9.4	650281	56.5	349719	4080891295	55
6	611012	47.1	960392	9.4	650620	56.5	349380	4083591283	54
7	611294	47.0	960335	9.4	650959	56.4	349041	4086291272	53
8	611576	47.0	960279	9.4	651297	56.4	348703	4088991260	52
9	611858	46.9	960222	9.4	651636	56.4	348364	4091691248	51
10	612140	46.9	950165	9.4	651974	56.3	348026	4094391236	50
11	9.612421	46.9	9.960109	9.5	9.652312	56.3	10.347688	4097091224	49
12	612702	46.8	960052	9.5	652650	56.3	347350	4099791212	48
13	612983	46.8	959995	9.5	652988	56.3	347012	4102491200	47
14	613264	46.7	959938	9.5	653326	56.2	346674	4105191188	46
15	613545	46.7	959882	9.5	653663	56.2	346337	4107891176	45
16	613825	46.7	959825	9.5	654000	56.2	346000	4110591164	44
17	614105	46.6	959768	9.5	654337	56.1	345663	4113291152	43
18	614385	46.6	959711	9.5	654674	56.1	345326	4115991140	42
19	614665	46.6	959654	9.5	655011	56.1	344989	4118691128	41
20	614944	46.5	959596	9.5	655348	56.1	344652	4121391116	40
21	9.615223	46.5	9.959539	9.5	9.655684	56.0	10.344316	4124091104	39
22	615502	46.5	959482	9.5	656020	56.0	343980	4126791092	38
23	615781	46.4	959425	9.5	656356	56.0	343644	4129491080	37
24	616060	46.4	959368	9.5	656692	56.0	343308	4132191068	36
25	616338	46.4	959310	9.5	657028	55.9	342972	4134891056	35
26	616616	46.3	959253	9.6	657364	55.9	342636	4137591044	34
27	616894	46.3	959195	9.6	657699	55.9	342301	4140291032	33
28	617172	46.2	959138	9.6	658034	55.8	341966	4142991020	32
29	617450	46.2	959081	9.6	658369	55.8	341631	4145691008	31
30	617727	46.2	959023	9.6	658704	55.8	341296	4148390996	30
31	9.618004	46.1	9.958965	9.6	9.659039	55.8	10.340961	4151090984	29
32	618281	46.1	958908	9.6	659373	55.7	340627	4153790972	28
33	618558	46.1	958850	9.6	659708	55.7	340292	4156490960	27
34	618834	46.0	958792	9.6	660042	55.7	339958	4159190948	26
35	619110	46.0	958734	9.6	660376	55.7	339624	4161890936	25
36	619386	46.0	958677	9.6	660710	55.6	339290	4164590924	24
37	619662	45.9	958619	9.6	661043	55.6	338957	4167290912	23
38	619938	45.9	958561	9.6	661377	55.6	338623	4169990900	22
39	620213	45.9	958503	9.6	661710	55.5	338290	4172690888	21
40	620488	45.8	958445	9.7	662043	55.5	337957	4175390876	20
41	9.620763	45.8	9.958387	9.7	9.662376	55.5	10.337624	4178090864	19
42	621038	45.7	958329	9.7	662709	55.4	337291	4180790852	18
43	621313	45.7	958271	9.7	663042	55.4	336958	4183490840	17
44	621587	45.7	958213	9.7	663375	55.4	336625	4186190828	16
45	621861	45.6	958154	9.7	663707	55.4	336293	4188890816	15
46	622135	45.6	958096	9.7	664039	55.3	335961	4191590804	14
47	622409	45.6	958038	9.7	664371	55.3	335629	4194290792	13
48	622682	45.5	957979	9.7	664703	55.3	335297	4196990780	12
49	622956	45.5	957921	9.7	665035	55.3	334965	4199690768	11
50	623229	45.5	957863	9.7	665366	55.2	334634	4202390756	10
51	9.623512	45.4	9.957804	9.7	9.665697	55.2	10.334303	4205090744	9
52	623774	45.4	957746	9.7	666029	55.2	334307	4207790732	8
53	624047	45.4	957687	9.8	666360	55.1	333976	4210490720	7
54	624319	45.3	957628	9.8	666691	55.1	333645	4213190708	6
55	624591	45.3	957570	9.8	667021	55.1	333314	4215890696	5
56	624863	45.3	957511	9.8	667352	55.1	332983	4218590684	4
57	625135	45.2	957452	9.8	667682	55.0	332652	4221290672	3
58	625407	45.2	957393	9.8	668013	55.0	332321	4223990660	2
59	625677	45.2	957335	9.8	668343	55.0	331990	4226690648	1
60	625948	45.2	957276	9.8	668672	55.0	331659	4229390636	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	9.625948	45.1	9.957276	9.8	9.668673	55.0	10.331327	42262	90631	60
1	626219	45.1	957217	9.8	669002	54.9	330998	42288	90613	59
2	626490	45.1	957158	9.8	669332	54.9	330368	42315	90606	58
3	62670	45.0	957099	9.8	669661	54.9	330339	42341	90594	57
4	627030	45.0	957040	9.8	669991	54.8	330009	42367	90582	56
5	627300	45.0	956981	9.8	670320	54.8	329680	42394	90569	55
6	627570	44.9	956921	9.9	670649	54.8	329351	42420	90557	54
7	627840	44.9	956862	9.9	670977	54.8	329023	42446	90545	53
8	628109	44.9	956803	9.9	671306	54.7	328694	42473	90532	52
9	628378	44.8	956744	9.9	671634	54.7	328366	42499	90520	51
10	628647	44.8	956684	9.9	671963	54.7	328037	42525	90507	50
11	9.628916	44.7	9.956625	9.9	9.672291	54.7	10.327709	42552	90495	49
12	629185	44.7	956566	9.9	672619	54.6	327381	42578	90483	48
13	629453	44.7	956506	9.9	672947	54.6	327053	42604	90470	47
14	629721	44.6	956447	9.9	673274	54.6	326726	42631	90458	46
15	629989	44.6	956387	9.9	673602	54.6	326398	42657	90446	45
16	630257	44.6	956327	9.9	673929	54.5	326071	42683	90433	44
17	630524	44.6	956268	9.9	674257	54.5	325743	42709	90421	43
18	630792	44.5	956208	10.0	674584	54.5	325416	42736	90408	42
19	631059	44.5	956148	10.0	674910	54.4	325090	42762	90396	41
20	631326	44.5	956089	10.0	675237	54.4	324763	42788	90383	40
21	9.631593	44.4	9.956029	10.0	9.675564	54.4	10.324436	42815	90371	39
22	631859	44.4	955969	10.0	675890	54.4	324410	42841	90358	38
23	632125	44.4	955909	10.0	676216	54.3	323784	42867	90346	37
24	632392	44.3	955849	10.0	676543	54.3	323457	42894	90334	36
25	632658	44.3	955789	10.0	676869	54.3	323131	42920	90321	35
26	632923	44.3	955729	10.0	677194	54.3	322806	42946	90309	34
27	633189	44.2	955669	10.0	677520	54.2	322480	42972	90296	33
28	633454	44.2	955609	10.0	677846	54.2	322154	42999	90284	32
29	633719	44.2	955548	10.0	678171	54.2	321829	43025	90271	31
30	633984	44.1	955488	10.0	678496	54.2	321504	43051	90259	30
31	9.634249	44.1	9.955428	10.1	9.678821	54.1	10.321179	43077	90246	29
32	634514	44.0	955368	10.1	679146	54.1	320854	43104	90233	28
33	634778	44.0	955307	10.1	679471	54.1	320529	43130	90221	27
34	635042	44.0	955247	10.1	679795	54.1	320205	43156	90208	26
35	635306	43.9	955186	10.1	680120	54.0	319880	43182	90196	25
36	635570	43.9	955126	10.1	680444	54.0	319556	43209	90183	24
37	635834	43.9	955065	10.1	680768	54.0	319232	43235	90171	23
38	636097	43.8	955005	10.1	681092	54.0	318908	43261	90158	22
39	636360	43.8	954944	10.1	681416	53.9	318584	43287	90146	21
40	636623	43.8	954883	10.1	681740	53.9	318260	43313	90133	20
41	9.636886	43.7	9.954823	10.1	9.682063	53.9	10.317937	43340	90120	19
42	637148	43.7	954762	10.1	682387	53.9	317613	43366	90108	18
43	637411	43.7	954701	10.1	682710	53.8	317290	43392	90095	17
44	637673	43.7	954640	10.1	683033	53.8	316967	43418	90082	16
45	637935	43.6	954579	10.1	683356	53.8	316644	43445	90070	15
46	638197	43.6	954518	10.2	683679	53.8	316321	43471	90057	14
47	638458	43.6	954457	10.2	684001	53.7	315999	43497	90045	13
48	638720	43.5	954396	10.2	684324	53.7	315676	43523	90032	12
49	638981	43.5	954335	10.2	684646	53.7	315354	43549	90019	11
50	639242	43.5	954274	10.2	684968	53.7	315032	43575	90007	10
51	9.639503	43.4	9.954213	10.2	9.685290	53.6	10.314710	43602	89994	9
52	639764	43.4	954152	10.2	685612	53.6	314388	43628	89981	8
53	640024	43.4	954090	10.2	685934	53.6	314066	43654	89968	7
54	640284	43.3	954029	10.2	686255	53.6	313745	43680	89956	6
55	640544	43.3	953968	10.2	686577	53.5	313423	43706	89943	5
56	640804	43.3	953906	10.2	686898	53.5	313102	43732	89930	4
57	641064	43.2	953845	10.2	687219	53.5	312781	43759	89918	3
58	641324	43.2	953783	10.2	687540	53.5	312460	43785	89905	2
59	641584	43.2	953722	10.3	687861	53.4	312139	43811	89892	1
60	641842	43.2	953660		688182		311818	43837	89879	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	



TABLE II.

Log. Sines and Tangents. (26°) Natural Sines.

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	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.641842		9.953660		9.688182		10.311818	43837	89879	60
1	642101	43.1	953599	10.3	688502	53.4	311498	43863	89867	59
2	642360	43.1	953537	10.3	688823	53.4	311177	43889	89854	58
3	642618	43.0	953475	10.3	689143	53.3	310857	43916	89841	57
4	642877	43.0	953413	10.3	689463	53.3	310537	43942	89828	56
5	643135	43.0	953352	10.3	689783	53.3	310217	43968	89816	55
6	643393	43.0	953290	10.3	690103	53.3	309897	43994	89803	54
7	643650	42.9	953228	10.3	690423	53.3	309577	44020	89790	53
8	643908	42.9	953166	10.3	690742	53.2	309258	44046	89777	52
9	644165	42.9	953104	10.3	691062	53.2	308938	44072	89764	51
10	644423	42.8	953042	10.3	691381	53.2	308619	44098	89752	50
11	9.644680	42.8	9.952980	10.4	9.691700	53.1	10.308300	44124	89739	49
12	644936	42.8	952918	10.4	692019	53.1	307981	44151	89726	48
13	645193	42.7	952855	10.4	692338	53.1	307662	44177	89713	47
14	645450	42.7	952793	10.4	692656	53.1	307344	44203	89700	46
15	645705	42.7	952731	10.4	692975	53.1	307025	44229	89687	45
16	645962	42.6	952669	10.4	693293	53.0	306707	44255	89674	44
17	646218	42.6	952606	10.4	693612	53.0	306388	44281	89662	43
18	646474	42.6	952544	10.4	693930	53.0	306070	44307	89649	42
19	646729	42.5	952481	10.4	694248	53.0	305752	44333	89636	41
20	646984	42.5	952419	10.4	694566	52.9	305434	44359	89623	40
21	9.647240	42.5	9.952356	10.4	9.694883	52.9	10.305117	44385	89610	39
22	647494	42.4	952294	10.4	695201	52.9	304799	44411	89597	38
23	647749	42.4	952231	10.4	695518	52.9	304482	44437	89584	37
24	648004	42.4	952168	10.5	695836	52.9	304164	44464	89571	36
25	648258	42.4	952105	10.5	696153	52.8	303847	44490	89558	35
26	648512	42.3	952043	10.5	696470	52.8	303530	44516	89545	34
27	648766	42.3	951980	10.5	696787	52.8	303213	44542	89532	33
28	649020	42.3	951917	10.5	697103	52.8	302897	44568	89519	32
29	649274	42.2	951854	10.5	697420	52.7	302580	44594	89506	31
30	649527	42.2	951791	10.5	697736	52.7	302264	44620	89493	30
31	9.649781	42.2	9.951728	10.5	9.698053	52.7	10.301947	44646	89480	29
32	650034	42.2	951665	10.5	698369	52.7	301631	44672	89467	28
33	650287	42.1	951602	10.5	698685	52.6	301315	44698	89454	27
34	650539	42.1	951539	10.5	699001	52.6	300999	44724	89441	26
35	650792	42.1	951476	10.5	699316	52.6	300684	44750	89428	25
36	651044	42.0	951412	10.5	699632	52.6	300368	44776	89415	24
37	651297	42.0	951349	10.6	699947	52.6	300053	44802	89402	23
38	651549	42.0	951286	10.6	700263	52.5	299737	44828	89389	22
39	651800	41.9	951222	10.6	700578	52.5	299422	44854	89376	21
40	652052	41.9	951159	10.6	700893	52.5	299107	44880	89363	20
41	9.652304	41.9	9.951096	10.6	9.701208	52.4	10.28792	44906	89350	19
42	652555	41.8	951032	10.6	701523	52.4	298847	44932	89337	18
43	652806	41.8	950968	10.6	701837	52.4	298531	44958	89324	17
44	653057	41.8	950905	10.6	702152	52.4	298215	44984	89311	16
45	653308	41.8	950841	10.6	702466	52.4	297900	45010	89298	15
46	653558	41.7	950778	10.6	702780	52.3	297585	45036	89285	14
47	653808	41.7	950714	10.6	703095	52.3	297270	45062	89272	13
48	654059	41.7	950650	10.6	703409	52.3	296955	45088	89259	12
49	654309	41.6	950586	10.6	703723	52.3	296640	45114	89245	11
50	654558	41.6	950522	10.6	704036	52.2	296325	45140	89232	10
51	9.654808	41.6	9.950458	10.7	9.704350	52.2	10.295650	45166	89219	9
52	655058	41.6	950394	10.7	704663	52.2	296010	45192	89206	8
53	655307	41.5	950330	10.7	704977	52.2	295695	45218	89193	7
54	655556	41.5	950266	10.7	705290	52.2	295380	45244	89180	6
55	655805	41.5	950202	10.7	705603	52.1	295065	45270	89167	5
56	656054	41.4	950138	10.7	705916	52.1	294750	45296	89153	4
57	656302	41.4	950074	10.7	706228	52.1	294435	45322	89140	3
58	656551	41.4	950010	10.7	706541	52.1	294120	45348	89127	2
59	656799	41.3	949945	10.7	706854	52.1	293805	45374	89114	1
60	65.017		949881	10.7	70.166		293490	45399	89101	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10'	Cotang.	N. sine.	N. cos.	
0	9.657017		9.919881		9.707166		10.292834	45399	89101	60
1	657295	41.3	949815	10.7	707478	52.0	292522	45425	89087	59
2	657542	41.3	949752	10.7	707790	52.0	292210	45451	89074	58
3	657790	41.2	949688	10.7	708102	52.0	291898	45477	89061	57
4	658037	41.2	949623	10.8	708414	51.9	291586	45503	89048	56
5	658284	41.2	949558	10.8	708726	51.9	291274	45529	89035	55
6	658531	41.1	949494	10.8	709037	51.9	290963	45554	89021	54
7	658778	41.1	949429	10.8	709349	51.9	290651	45580	89008	53
8	659025	41.1	949364	10.8	709660	51.9	290340	45606	88995	52
9	659271	41.1	949300	10.8	709971	51.9	290029	45632	88981	51
10	659517	41.0	949235	10.8	710282	51.8	289718	45658	88968	50
11	659763	41.0	949170	10.8	710593	51.8	289407	45684	88955	49
12	660009	40.9	949105	10.8	710904	51.8	289096	45710	88942	48
13	660255	40.9	949040	10.8	711215	51.8	288785	45736	88928	47
14	660501	40.9	948975	10.8	711525	51.8	288475	45762	88915	46
15	660746	40.9	948910	10.8	711835	51.7	288164	45788	88902	45
16	660991	40.8	948845	10.8	712146	51.7	287854	45813	88888	44
17	661235	40.8	948780	10.9	712455	51.7	287544	45839	88875	43
18	661481	40.8	948715	10.9	712766	51.7	287234	45865	88862	42
19	661726	40.7	948650	10.9	713076	51.6	286924	45891	88848	41
20	661970	40.7	948584	10.9	713386	51.6	286614	45917	88835	40
21	9.662214		9.948519		9.713696		10.286304	45942	88822	39
22	662459	40.7	948544	10.9	714005	51.6	285995	45968	88808	38
23	662703	40.6	948488	10.9	714314	51.6	285686	45994	88795	37
24	662946	40.6	948432	10.9	714624	51.5	285376	46020	88782	36
25	663190	40.6	948375	10.9	714933	51.5	285067	46046	88768	35
26	663433	40.5	948319	10.9	715242	51.5	284758	46072	88755	34
27	663677	40.5	948262	10.9	715551	51.5	284449	46097	88741	33
28	663920	40.5	948206	10.9	715860	51.4	284140	46123	88728	32
29	664163	40.5	948149	11.0	716168	51.4	283832	46149	88715	31
30	664406	40.4	948092	11.0	716477	51.4	283523	46175	88701	30
31	9.664648		9.947863		9.716785		10.283215	46201	88688	29
32	664891	40.4	947797	11.0	717093	51.4	282907	46226	88674	28
33	665133	40.3	947731	11.0	717401	51.3	282599	46252	88661	27
34	665375	40.3	947665	11.0	717709	51.3	282291	46278	88647	26
35	665617	40.3	947600	11.0	718017	51.3	281983	46304	88634	25
36	665859	40.2	947533	11.0	718325	51.3	281675	46330	88620	24
37	666100	40.2	947467	11.0	718633	51.3	281367	46355	88607	23
38	666342	40.2	947401	11.0	718940	51.2	281060	46381	88593	22
39	666583	40.2	947335	11.0	719248	51.2	280752	46407	88580	21
40	666824	40.1	947269	11.0	719555	51.2	280445	46433	88566	20
41	9.667065		9.947203		9.719862		10.280138	46458	88553	19
42	667305	40.1	947136	11.1	720169	51.2	279831	46484	88539	18
43	667546	40.1	947070	11.1	720476	51.1	279524	46510	88526	17
44	667786	40.0	947004	11.1	720783	51.1	279217	46536	88512	16
45	668027	40.0	946937	11.1	721089	51.1	278911	46561	88499	15
46	668267	39.9	946871	11.1	721396	51.1	278604	46587	88485	14
47	668506	39.9	946804	11.1	721702	51.0	278298	46613	88472	13
48	668746	39.9	946738	11.1	722009	51.0	277991	46639	88458	12
49	668986	39.9	946671	11.1	722315	51.0	277685	46664	88445	11
50	669225	39.9	946604	11.1	722621	51.0	277379	46690	88431	10
51	9.669464		9.946538		9.722927		10.277073	46716	88417	9
52	669703	39.8	946471	11.1	722932	51.0	276768	46742	88404	8
53	669942	39.8	946404	11.1	723238	50.9	276462	46767	88390	7
54	670181	39.7	946337	11.1	723544	50.9	276156	46793	88377	6
55	670419	39.7	946270	11.2	723849	50.9	275851	46819	88363	5
56	670658	39.7	946203	11.2	724154	50.9	275546	46844	88349	4
57	670896	39.7	946136	11.2	724459	50.8	275241	46870	88336	3
58	671134	39.6	946069	11.2	724765	50.8	274935	46896	88322	2
59	671372	39.6	946002	11.2	725069	50.8	274631	46921	88308	1
60	6.1609		9.945935		725374	50.8	274326	46947	88295	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (28°) Natural Sines.

°	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.671649		9.945935		9.725674		10.274326	46947	88295	60
1	671847	39.6	945868	11.2	725979	50.8	274021	46973	88281	59
2	672054	39.5	945800	11.2	726284	50.8	273716	46999	88267	58
3	672321	39.5	945733	11.2	726588	50.7	273412	47024	88254	57
4	672558	39.5	945665	11.2	726892	50.7	273108	47050	88240	56
5	672795	39.5	945598	11.2	727197	50.7	272803	47076	88226	55
6	673032	39.4	945531	11.2	727501	50.7	272499	47101	88213	54
7	673238	39.4	945464	11.2	727805	50.7	272195	47127	88199	53
8	673505	39.4	945396	11.3	728109	50.6	271891	47153	88185	52
9	673741	39.4	945328	11.3	728412	50.6	271588	47178	88172	51
10	673977	39.3	945261	11.3	728716	50.6	271284	47204	88158	50
11	9.674213	39.3	9.945193	11.3	9.729027	50.6	10.270980	47229	88144	49
12	674448	39.3	945125	11.3	729323	50.6	270777	47255	88130	48
13	674684	39.2	945058	11.3	729626	50.5	270374	47281	88117	47
14	674919	39.2	944990	11.3	729929	50.5	270071	47306	88103	46
15	675155	39.2	944922	11.3	730233	50.5	269767	47332	88089	45
16	675390	39.2	944854	11.3	730535	50.5	269465	47358	88075	44
17	675524	39.1	944786	11.3	730838	50.5	269162	47383	88062	43
18	675859	39.1	944718	11.3	731141	50.4	268859	47409	88048	42
19	676094	39.1	944650	11.3	731444	50.4	268556	47434	88034	41
20	676328	39.1	944582	11.3	731746	50.4	268254	47460	88020	40
21	9.676562	39.0	9.944514	11.4	9.732048	50.4	10.267952	47486	88006	39
22	676795	39.0	944446	11.4	732351	50.4	267649	47511	87993	38
23	677030	39.0	944377	11.4	732653	50.3	267347	47537	87979	37
24	677264	38.9	944309	11.4	732955	50.3	267045	47562	87965	36
25	677498	38.9	944241	11.4	733257	50.3	266743	47588	87951	35
26	677731	38.9	944172	11.4	733558	50.3	266442	47614	87937	34
27	677964	38.8	944104	11.4	733860	50.2	266140	47639	87923	33
28	678197	38.8	944036	11.4	734162	50.2	265838	47665	87909	32
29	678430	38.8	943967	11.4	734463	50.2	265537	47690	87896	31
30	678663	38.8	943899	11.4	734764	50.2	265236	47716	87882	30
31	9.678895	38.7	9.943830	11.4	9.735066	50.2	10.264934	47741	87868	29
32	679128	38.7	943761	11.4	735367	50.2	264633	47767	87854	28
33	679360	38.7	943693	11.4	735668	50.2	264332	47793	87840	27
34	679592	38.7	943624	11.5	735969	50.1	264031	47818	87826	26
35	679824	38.7	943555	11.5	736269	50.1	263731	47844	87812	25
36	680056	38.6	943486	11.5	736570	50.1	263430	47869	87798	24
37	680288	38.6	943417	11.5	736871	50.1	263129	47895	87784	23
38	680519	38.6	943348	11.5	737171	50.1	262829	47920	87770	22
39	680750	38.5	943279	11.5	737471	50.0	262529	47946	87756	21
40	680982	38.5	943210	11.5	737771	50.0	262229	47971	87743	20
41	9.681213	38.5	9.943141	11.5	9.738071	50.0	10.261929	47997	87729	19
42	681443	38.5	943072	11.5	738371	50.0	261629	48022	87715	18
43	681674	38.4	943003	11.5	738671	50.0	261329	48048	87701	17
44	681905	38.4	942934	11.5	738971	49.9	261029	48073	87687	16
45	682135	38.4	942864	11.5	739271	49.9	260729	48099	87673	15
46	682365	38.4	942795	11.5	739570	49.9	260430	48124	87659	14
47	682595	38.3	942726	11.6	739870	49.9	260130	48150	87645	13
48	682825	38.3	942656	11.6	740169	49.9	259831	48175	87631	12
49	683055	38.3	942587	11.6	740468	49.9	259532	48201	87617	11
50	683284	38.3	942517	11.6	740767	49.8	259233	48226	87603	10
51	9.683514	38.2	9.942448	11.6	9.741036	49.8	10.258934	48252	87589	9
52	683743	38.2	942378	11.6	741365	49.8	258635	48277	87575	8
53	683972	38.2	942308	11.6	741664	49.8	258336	48303	87561	7
54	684201	38.2	942239	11.6	741962	49.8	258038	48328	87546	6
55	684430	38.1	942169	11.6	742261	49.7	257739	48354	87532	5
56	684658	38.1	942099	11.6	742559	49.7	257441	48379	87518	4
57	684887	38.1	942029	11.6	742858	49.7	257142	48405	87504	3
58	685115	38.0	941959	11.6	743156	49.7	256844	48430	87490	2
59	685343	38.0	941889	11.6	743454	49.7	256546	48456	87476	1
60	685571	38.0	941819	11.7	743752	49.7	256248	48481	87462	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	7

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.685571	38.0	9.941819	11.7	9.743752	49.6	10.250248	48481	87462	60
1	685799	37.9	941749	11.7	744050	49.6	255950	48506	87448	59
2	686027	37.9	941679	11.7	744348	49.6	255652	48532	87434	58
3	686254	37.9	941609	11.7	744645	49.6	255355	48557	87420	57
4	686482	37.9	941539	11.7	744943	49.6	255057	48583	87406	56
5	686709	37.8	941469	11.7	745240	49.6	254760	48608	87391	55
6	686936	37.8	941398	11.7	745538	49.5	254462	48634	87377	54
7	687163	37.8	941328	11.7	745835	49.5	254165	48659	87363	53
8	687389	37.8	941258	11.7	746132	49.5	253868	48684	87349	52
9	687616	37.7	941187	11.7	746429	49.5	253571	48710	87335	51
10	687843	37.7	941117	11.7	746726	49.5	253274	48735	87321	50
11	9.688069	37.7	9.941046	11.8	9.747023	49.4	10.252977	48761	87306	49
12	688295	37.7	940975	11.8	747319	49.4	252681	48786	87292	48
13	688521	37.6	940905	11.8	747616	49.4	252384	48811	87278	47
14	688747	37.6	940834	11.8	747913	49.4	252087	48837	87264	46
15	688972	37.6	940763	11.8	748209	49.4	251791	48862	87250	45
16	689198	37.6	940693	11.8	748505	49.3	251495	48888	87235	44
17	689423	37.5	940622	11.8	748801	49.3	251199	48913	87221	43
18	689648	37.5	940551	11.8	749097	49.3	250903	48938	87207	42
19	689873	37.5	940480	11.8	749393	49.3	250607	48964	87193	41
20	690098	37.5	940409	11.8	749689	49.3	250311	48989	87178	40
21	9.690323	37.4	9.940338	11.8	9.749985	49.3	10.250015	49014	87164	39
22	690548	37.4	940267	11.8	750281	49.2	249719	49040	87150	38
23	690772	37.4	940196	11.8	750576	49.2	249424	49065	87136	37
24	690996	37.4	940125	11.8	750872	49.2	249128	49090	87121	36
25	691220	37.3	940054	11.9	751167	49.2	248833	49116	87107	35
26	691444	37.3	939982	11.9	751462	49.2	248538	49141	87093	34
27	691668	37.3	939911	11.9	751757	49.2	248243	49166	87079	33
28	691892	37.3	939840	11.9	752052	49.1	247948	49192	87064	32
29	692115	37.2	939768	11.9	752347	49.1	247653	49217	87050	31
30	692339	37.2	939697	11.9	752642	49.1	247358	49242	87036	30
31	9.692562	37.2	9.939625	11.9	9.752937	49.1	10.247063	49268	87021	29
32	692785	37.1	939554	11.9	753231	49.1	246769	49293	87007	28
33	693008	37.1	939482	11.9	753526	49.1	246474	49318	86993	27
34	693231	37.1	939410	11.9	753820	49.0	246180	49344	86978	26
35	693453	37.1	939339	11.9	754115	49.0	245885	49369	86964	25
36	693676	37.0	939267	11.9	754409	49.0	245591	49394	86949	24
37	693898	37.0	939195	12.0	754703	49.0	245297	49419	86935	23
38	694120	37.0	939123	12.0	754997	49.0	245003	49445	86921	22
39	694342	37.0	939052	12.0	755291	49.0	244709	49470	86906	21
40	694564	36.9	938980	12.0	755585	48.9	244415	49495	86892	20
41	9.694786	36.9	9.938908	12.0	9.755878	48.9	10.244123	49521	86878	19
42	695007	36.9	938836	12.0	756172	48.9	243828	49546	86863	18
43	695229	36.9	938763	12.0	756465	48.9	243535	49571	86849	17
44	695450	36.8	938691	12.0	756759	48.9	243241	49596	86834	16
45	695671	36.8	938619	12.0	757052	48.9	242948	49622	86820	15
46	695892	36.8	938547	12.0	757345	48.8	242655	49647	86805	14
47	696113	36.8	938475	12.0	757638	48.8	242352	49672	86791	13
48	696334	36.7	938402	12.0	757931	48.8	242069	49697	86777	12
49	696554	36.7	938330	12.1	758224	48.8	241776	49723	86762	11
50	696775	36.7	938258	12.1	758517	48.8	241483	49748	86748	10
51	9.696995	36.7	9.938185	12.1	9.758810	48.8	10.241190	49773	86733	9
52	697215	36.6	938113	12.1	759102	48.7	240898	49798	86719	8
53	697435	36.6	938040	12.1	759395	48.7	240605	49824	86704	7
54	697654	36.6	937967	12.1	759687	48.7	240313	49849	86690	6
55	697874	36.6	937895	12.1	759979	48.7	240021	49874	86675	5
56	698094	36.5	937822	12.1	760272	48.7	239728	49899	86661	4
57	698313	36.5	937749	12.1	760564	48.7	239436	49924	86646	3
58	698532	36.5	937676	12.1	760856	48.6	239144	49950	86632	2
59	698751	36.5	937604	12.1	761148	48.6	238852	49975	86617	1
60	698970	36.5	937531	12.1	761439	48.6	238561	50000	86603	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (30°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	698970		9.937531		9.761439		10.238561	50000	86603	60
1	699189	36.4	937458	12.1	761731	48.6	238269	50025	86588	59
2	699407	36.4	937385	12.2	762023	48.6	237977	50050	86573	58
3	699625	36.4	937312	12.2	762314	48.6	237686	50076	86559	57
4	699844	36.4	937238	12.2	762605	48.5	237394	50101	86544	56
5	700062	36.3	937165	12.2	762897	48.5	237103	50126	86530	55
6	700280	36.3	937092	12.2	763188	48.5	236812	50151	86515	54
7	700498	36.3	937019	12.2	763479	48.5	236521	50176	86501	53
8	700716	36.3	936946	12.2	763770	48.5	236230	50201	86486	52
9	700933	36.2	936872	12.2	764061	48.5	235939	50227	86471	51
10	701151	36.2	936799	12.2	764352	48.4	235648	50252	86457	50
11	9.701368	36.2	9.936725	12.2	9.764643	48.4	10.235357	50277	86442	49
12	701585	36.2	936652	12.3	764933	48.4	235057	50302	86427	48
13	701802	36.1	936578	12.3	765224	48.4	234776	50327	86413	47
14	702019	36.1	936505	12.3	765514	48.4	234486	50352	86398	46
15	702236	36.1	936431	12.3	765805	48.4	234195	50377	86384	45
16	702452	36.0	936357	12.3	766095	48.4	233905	50403	86369	44
17	702669	36.0	936284	12.3	766385	48.3	233615	50428	86354	43
18	702885	36.0	936210	12.3	766675	48.3	233325	50453	86340	42
19	703101	36.0	936136	12.3	766965	48.3	233035	50478	86325	41
20	703317	36.0	936062	12.3	767255	48.3	232745	50503	86310	40
21	9.703533	35.9	9.935988	12.3	9.767545	48.3	10.232455	50528	86295	39
22	703749	35.9	935914	12.3	767834	48.3	232155	50553	86281	38
23	703964	35.9	935840	12.3	768124	48.2	231876	50578	86266	37
24	704179	35.9	935766	12.4	768413	48.2	231587	50603	86251	36
25	704395	35.9	935692	12.4	768703	48.2	231297	50628	86237	35
26	704610	35.8	935618	12.4	768992	48.2	231008	50654	86222	34
27	704825	35.8	935543	12.4	769281	48.2	230719	50679	86207	33
28	705040	35.8	935469	12.4	769570	48.2	230430	50704	86192	32
29	705254	35.8	935395	12.4	769860	48.1	230140	50729	86178	31
30	705469	35.7	935320	12.4	770148	48.1	229852	50754	86163	30
31	9.705683	35.7	9.935246	12.4	9.770437	48.1	10.229563	50779	86148	29
32	705898	35.7	935171	12.4	770726	48.1	229274	50804	86133	28
33	706112	35.7	935097	12.4	771015	48.1	228985	50829	86119	27
34	706326	35.6	935022	12.4	771303	48.1	228697	50854	86104	26
35	706539	35.6	934948	12.4	771592	48.1	228408	50879	86089	25
36	706753	35.6	934873	12.4	771880	48.0	228120	50904	86074	24
37	706967	35.6	934798	12.5	772168	48.0	227832	50929	86059	23
38	707180	35.5	934723	12.5	772457	48.0	227543	50954	86045	22
39	707393	35.5	934649	12.5	772745	48.0	227255	50979	86030	21
40	707606	35.5	934574	12.5	773033	48.0	226967	51004	86015	20
41	9.707819	35.5	9.934499	12.5	9.773321	48.0	10.226679	51029	86000	19
42	708032	35.4	934424	12.5	773608	47.9	226392	51054	85985	18
43	708245	35.4	934349	12.5	773896	47.9	226104	51079	85970	17
44	708458	35.4	934274	12.5	774184	47.9	225816	51104	85955	16
45	708670	35.4	934199	12.5	774471	47.9	225529	51129	85941	15
46	708882	35.3	934123	12.5	774759	47.9	225241	51154	85926	14
47	709094	35.3	934048	12.5	775046	47.9	224954	51179	85911	13
48	709306	35.3	933973	12.5	775333	47.9	224667	51204	85896	12
49	709518	35.3	933898	12.6	775621	47.8	224379	51229	85881	11
50	709730	35.3	933822	12.6	775908	47.8	224092	51254	85866	10
51	9.709941	35.2	9.933747	12.6	9.776195	47.8	10.223805	51279	85851	9
52	710153	35.2	933671	12.6	776482	47.8	223518	51304	85836	8
53	710364	35.2	933596	12.6	776769	47.8	223231	51329	85821	7
54	710575	35.2	933520	12.6	777055	47.8	222945	51354	85806	6
55	710785	35.1	933445	12.6	777342	47.8	222658	51379	85792	5
56	710997	35.1	933369	12.6	777628	47.7	222372	51404	85777	4
57	711208	35.1	933293	12.6	777915	47.7	222085	51429	85762	3
58	711419	35.1	933217	12.6	778201	47.7	221799	51454	85747	2
59	711629	35.0	933141	12.6	778487	47.7	221512	51479	85732	1
60	711839	35.0	933066	12.6	778774	47.7	221226	51504	85717	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	9.711839	35.0	9.933036	12.6	9.778774	47.7	10.221226	51504	85717	60
1	712050	35.0	932990	12.7	779030	47.7	220940	51529	85702	59
2	712260	35.0	932914	12.7	779346	47.6	220654	51554	85687	58
3	712469	34.9	932833	12.7	779632	47.6	220368	51579	85672	57
4	712679	34.9	932762	12.7	779918	47.6	220082	51604	85657	56
5	712889	34.9	932685	12.7	780203	47.6	219797	51628	85642	55
6	713098	34.9	932609	12.7	780489	47.6	219511	51653	85627	54
7	713308	34.9	932533	12.7	780775	47.6	219225	51678	85612	53
8	713517	34.8	932457	12.7	781060	47.6	218940	51703	85597	52
9	713726	34.8	932380	12.7	781346	47.6	218654	51728	85582	51
10	713935	34.8	932304	12.7	781631	47.5	218369	51753	85567	50
11	9.714144	34.8	9.932228	12.7	9.781916	47.5	10.218084	51778	85551	49
12	714352	34.7	932151	12.7	782201	47.5	217799	51803	85536	48
13	714561	34.7	932075	12.8	782486	47.5	217514	51828	85521	47
14	714769	34.7	931998	12.8	782771	47.5	217229	51852	85506	46
15	714978	34.7	931921	12.8	783056	47.5	216944	51877	85491	45
16	715186	34.7	931845	12.8	783341	47.5	216659	51902	85476	44
17	715394	34.6	931768	12.8	783626	47.4	216374	51927	85461	43
18	715602	34.6	931691	12.8	783910	47.4	216089	51952	85446	42
19	715809	34.6	931614	12.8	784195	47.4	215805	51977	85431	41
20	716017	34.6	931537	12.8	784479	47.4	215521	52002	85416	40
21	9.716224	34.5	9.931460	12.8	9.784764	47.4	10.215236	52026	85401	39
22	716432	34.5	931383	12.8	785048	47.4	214952	52051	85385	38
23	716639	34.5	931306	12.8	785332	47.3	214668	52076	85370	37
24	716846	34.5	931229	12.9	785616	47.3	214384	52101	85355	36
25	717053	34.5	931152	12.9	785900	47.3	214100	52126	85340	35
26	717259	34.4	931075	12.9	786184	47.3	213816	52151	85325	34
27	717466	34.4	930998	12.9	786468	47.3	213532	52175	85310	33
28	717673	34.4	930921	12.9	786752	47.3	213248	52200	85294	32
29	717879	34.4	930843	12.9	787036	47.3	212964	52225	85279	31
30	718085	34.3	930766	12.9	787319	47.2	212681	52250	85264	30
31	9.718291	34.3	9.930688	12.9	9.787603	47.2	10.212397	52275	85249	29
32	718497	34.3	930611	12.9	787886	47.2	212114	52299	85234	28
33	718703	34.3	930533	12.9	788170	47.2	211830	52324	85218	27
34	718909	34.3	930456	12.9	788453	47.2	211547	52349	85203	26
35	719114	34.2	930378	12.9	788736	47.2	211264	52374	85188	25
36	719320	34.2	930300	12.9	789019	47.2	210981	52399	85173	24
37	719525	34.2	930223	13.0	789302	47.1	210698	52423	85157	23
38	719730	34.2	930145	13.0	789585	47.1	210415	52448	85142	22
39	719935	34.1	930067	13.0	789868	47.1	210132	52473	85127	21
40	720140	34.1	929989	13.0	790151	47.1	209849	52498	85112	20
41	9.720345	34.1	9.929911	13.0	9.790433	47.1	10.209567	52522	85096	19
42	720549	34.1	929833	13.0	790716	47.1	209284	52547	85081	18
43	720754	34.0	929755	13.0	790999	47.1	209001	52572	85066	17
44	720958	34.0	929677	13.0	791281	47.1	208719	52597	85051	16
45	721162	34.0	929599	13.0	791563	47.0	208437	52621	85035	15
46	721366	34.0	929521	13.0	791846	47.0	208154	52646	85020	14
47	721570	34.0	929442	13.0	792128	47.0	207872	52671	85005	13
48	721774	33.9	929364	13.1	792410	47.0	207590	52696	84989	12
49	721978	33.9	929286	13.1	792692	47.0	207308	52720	84974	11
50	722181	33.9	929207	13.1	792974	47.0	207026	52745	84959	10
51	9.722385	33.9	9.929129	13.1	9.793256	47.0	10.206744	52770	84943	9
52	722588	33.8	929050	13.1	793538	46.9	206462	52794	84928	8
53	722791	33.8	928972	13.1	793819	46.9	206181	52819	84913	7
54	722994	33.8	928893	13.1	794101	46.9	205899	52844	84897	6
55	723197	33.8	928815	13.1	794383	46.9	205617	52869	84882	5
56	723400	33.8	928736	13.1	794664	46.9	205336	52893	84866	4
57	723603	33.7	928657	13.1	794945	46.9	205055	52918	84851	3
58	723805	33.7	928578	13.1	795227	46.9	204773	52943	84836	2
59	724007	33.7	928499	13.1	795508	46.8	204492	52967	84820	1
60	724210	33.7	928420	13.1	795789	46.8	204211	52992	84805	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (32°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.724210		9.928420		9.795789		10.204211	52992	84805	60
1	724412	33.7	928312	13.2	795070	46.8	203930	53017	84789	59
2	724514	33.6	928263	13.2	796351	46.8	203649	53011	84774	58
3	724816	33.6	928183	13.2	796632	46.8	203368	53036	84759	57
4	725017	33.6	928104	13.2	796913	46.8	203087	53091	84743	56
5	725219	33.6	928025	13.2	797194	46.8	202806	53115	84728	55
6	725420	33.5	927946	13.2	797475	46.8	2.2525	53140	84712	54
7	725622	33.5	927867	13.2	797755	46.8	202245	53164	84697	53
8	725823	33.5	927787	13.2	798036	46.7	201964	53189	84681	52
9	726024	33.5	927708	13.2	798316	46.7	201684	53214	84666	51
10	726225	33.5	927629	13.2	798596	46.7	201404	53238	84650	50
11	9.726426	33.4	9.927549	13.2	9.798877	46.7	10.201123	53263	84635	49
12	726627	33.4	927470	13.3	799157	46.7	200843	53288	84619	48
13	726827	33.4	927390	13.3	799437	46.7	200563	53312	84604	47
14	727027	33.4	927310	13.3	799717	46.7	200283	53337	84588	46
15	727228	33.4	927231	13.3	799997	46.6	200003	53361	84573	45
16	727428	33.3	927151	13.3	800277	46.6	199723	53386	84557	44
17	727628	33.3	927071	13.3	800557	46.6	199443	53411	84542	43
18	727828	33.3	926991	13.3	800836	46.6	199164	53435	84526	42
19	728027	33.3	926911	13.3	801116	46.6	198884	53460	84511	41
20	728227	33.3	926831	13.3	801396	46.6	198604	53484	84495	40
21	9.728427	33.2	9.926751	13.3	9.801675	46.6	10.198325	53509	84480	39
22	728626	33.2	926671	13.3	801955	46.6	198045	53534	84464	38
23	728826	33.2	926591	13.3	802234	46.6	197766	53558	84448	37
24	729024	33.2	926511	13.3	802513	46.5	197487	53583	84433	36
25	729223	33.1	926431	13.4	802792	46.5	197208	53607	84417	35
26	729423	33.1	926351	13.4	803072	46.5	196928	53632	84402	34
27	729621	33.1	926270	13.4	803351	46.5	196649	53656	84386	33
28	729820	33.1	926190	13.4	803630	46.5	196370	53681	84370	32
29	730018	33.0	926110	13.4	803909	46.5	196092	53705	84355	31
30	730216	33.0	926029	13.4	804187	46.5	195813	53730	84339	30
31	9.730415	33.0	9.925949	13.4	9.804466	46.4	10.195534	53754	84324	29
32	730613	33.0	925868	13.4	804745	46.4	195255	53779	84308	28
33	730811	33.0	925788	13.4	805023	46.4	194977	53804	84292	27
34	731009	32.9	925707	13.4	805302	46.4	194698	53828	84277	26
35	731203	32.9	925626	13.4	805580	46.4	194420	53853	84261	25
36	731404	32.9	925545	13.5	805859	46.4	194141	53877	84245	24
37	731602	32.9	925465	13.5	806137	46.4	193863	53902	84230	23
38	731799	32.9	925384	13.5	806415	46.3	193585	53926	84214	22
39	731996	32.8	925303	13.5	806693	46.3	193307	53951	84198	21
40	732193	32.8	925222	13.5	806971	46.3	193029	53975	84182	20
41	9.732390	32.8	9.925141	13.5	9.807249	46.3	10.192751	54000	84167	19
42	732587	32.8	925060	13.5	807527	46.3	192473	54024	84151	18
43	732784	32.8	924979	13.5	807805	46.3	192195	54049	84135	17
44	732980	32.7	924897	13.5	808083	46.3	191917	54073	84120	16
45	733177	32.7	924816	13.5	808361	46.3	191639	54097	84104	15
46	733373	32.7	924735	13.6	808638	46.2	191362	54122	84088	14
47	733569	32.7	924654	13.6	808916	46.2	191084	54146	84072	13
48	733765	32.7	924572	13.6	809193	46.2	190807	54171	84057	12
49	733961	32.6	924491	13.6	809471	46.2	190529	54195	84041	11
50	734157	32.6	924409	13.6	809748	46.2	190252	54220	84025	10
51	9.734353	32.6	9.924328	13.6	9.810025	46.2	10.189975	54244	84009	9
52	734549	32.6	924246	13.6	810302	46.2	189698	54269	83994	8
53	734744	32.5	924164	13.6	810580	46.2	189420	54293	83978	7
54	734939	32.5	924083	13.6	810857	46.2	189143	54317	83962	6
55	735135	32.5	924003	13.6	811134	46.1	188866	54342	83946	5
56	735330	32.5	923919	13.6	811410	46.1	188590	54366	83930	4
57	735525	32.5	923837	13.6	811687	46.1	188313	54391	83915	3
58	735719	32.4	923755	13.7	811964	46.1	188036	54415	83899	2
59	735914	32.4	923673	13.7	812241	46.1	187759	54440	83883	1
60	736109	32.4	923591	13.7	812517	46.1	187483	54464	83867	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.736109		9.923591		9.812517		10.187482	54464	85867	60
1	736303	32.4	923509	13.7	812794	46.1	187206	54488	83851	59
2	736498	32.4	923427	13.7	813070	46.1	186930	54513	83835	58
3	736692	32.4	923345	13.7	813347	46.1	186653	54537	83819	57
4	736886	32.3	923263	13.7	813623	46.0	186377	54561	83804	56
5	737080	32.3	923181	13.7	813899	46.0	186101	54586	83788	55
6	737274	32.3	923098	13.7	814175	46.0	185825	54610	83772	54
7	737467	32.3	923016	13.7	814452	46.0	185548	54635	83756	53
8	737661	32.3	922933	13.7	814728	46.0	185272	54659	83740	52
9	737855	32.2	922851	13.7	815004	46.0	184996	54683	83724	51
10	738048	32.2	922768	13.7	815279	46.0	184721	54708	83708	50
11	9.738241	32.2	9.922686	13.8	9.815555	46.0	10.184445	54732	83692	49
12	738434	32.2	922603	13.8	815831	45.9	184169	54756	83676	48
13	738627	32.2	922520	13.8	816107	45.9	183893	54781	83660	47
14	738820	32.1	922438	13.8	816382	45.9	183618	54805	83645	46
15	739013	32.1	922355	13.8	816658	45.9	183342	54829	83629	45
16	739206	32.1	922272	13.8	816933	45.9	183067	54854	83613	44
17	739398	32.1	922189	13.8	817209	45.9	182791	54878	83597	43
18	739590	32.1	922106	13.8	817484	45.9	182516	54902	83581	42
19	739783	32.0	922023	13.8	817759	45.9	182241	54927	83565	41
20	739975	32.0	921940	13.8	818035	45.9	181965	54951	83549	40
21	9.740167	32.0	9.921857	13.9	9.818310	45.8	10.181690	54975	83533	39
22	740359	32.0	921774	13.9	818585	45.8	181415	54999	83517	38
23	740550	31.9	921691	13.9	818860	45.8	181140	55024	83501	37
24	740742	31.9	921607	13.9	819135	45.8	180865	55048	83485	36
25	740934	31.9	921524	13.9	819410	45.8	180590	55072	83469	35
26	741125	31.9	921441	13.9	819684	45.8	180316	55097	83453	34
27	741315	31.9	921357	13.9	819959	45.8	180041	55121	83437	33
28	741508	31.9	921274	13.9	820234	45.8	179766	55145	83421	32
29	741699	31.8	921190	13.9	820508	45.7	179492	55169	83405	31
30	741889	31.8	921107	13.9	820783	45.7	179217	55194	83389	30
31	9.742080	31.8	9.921023	13.9	9.821057	45.7	10.178943	55218	83373	29
32	742271	31.8	920939	13.9	821332	45.7	178668	55242	83356	28
33	742462	31.8	920856	14.0	821606	45.7	178394	55266	83340	27
34	742652	31.7	920772	14.0	821880	45.7	178120	55291	83324	26
35	742842	31.7	920688	14.0	822154	45.7	177846	55315	83308	25
36	743033	31.7	920604	14.0	822429	45.7	177571	55339	83292	24
37	743223	31.7	920520	14.0	822703	45.7	177297	55363	83276	23
38	743413	31.7	920436	14.0	822977	45.7	177023	55388	83260	22
39	743602	31.6	920352	14.0	823250	45.6	176750	55412	83244	21
40	743792	31.6	920268	14.0	823524	45.6	176476	55436	83228	20
41	9.743982	31.6	9.920184	14.0	9.823798	45.6	10.176202	55460	83212	19
42	744171	31.6	920099	14.0	824072	45.6	175928	55484	83195	18
43	744361	31.5	920015	14.0	824345	45.6	175655	55509	83179	17
44	744550	31.5	919931	14.0	824619	45.6	175381	55533	83163	16
45	744739	31.5	919846	14.1	824893	45.6	175107	55557	83147	15
46	744928	31.5	919762	14.1	825166	45.6	174834	55581	83131	14
47	745117	31.5	919677	14.1	825439	45.6	174561	55605	83115	13
48	745306	31.5	919593	14.1	825713	45.5	174287	55630	83098	12
49	745494	31.4	919508	14.1	825986	45.5	174014	55654	83082	11
50	745683	31.4	919424	14.1	826259	45.5	173741	55678	83066	10
51	9.745871	31.4	9.919339	14.1	9.826532	45.5	10.173468	55702	83050	9
52	746059	31.4	919254	14.1	826805	45.5	173195	55726	83034	8
53	746248	31.3	919169	14.1	827078	45.5	172922	55750	83017	7
54	746436	31.3	919085	14.1	827351	45.5	172649	55775	83001	6
55	746624	31.3	919000	14.1	827624	45.5	172376	55799	82985	5
56	746812	31.3	918915	14.1	827897	45.5	172103	55823	82969	4
57	746999	31.3	918830	14.2	828170	45.4	171830	55847	82953	3
58	747187	31.3	918745	14.2	828442	45.4	171558	55871	82936	2
59	747374	31.2	918659	14.2	828715	45.4	171285	55895	82920	1
60	747562	31.2	918574	14.2	828987	45.4	171013	55919	82904	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	



TABLE II. Log. Sines and Tangents. (34°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine	N. cos.	
0	9.747562		9.918574		9.828987		10.171013	55919	82904	60
1	747749	31.2	918489	14.2	829260	45.4	170740	55943	82887	59
2	747933	31.2	918404	14.2	829532	45.4	170468	55968	82871	58
3	748123	31.1	918318	14.2	829805	45.4	170195	55992	82855	57
4	748310	31.1	918233	14.2	830077	45.4	169923	56016	82839	56
5	748497	31.1	918147	14.2	830349	45.3	169651	56040	82822	55
6	748683	31.1	918062	14.2	830621	45.3	169379	56064	82806	54
7	748870	31.1	917976	14.3	830893	45.3	169107	56088	82790	53
8	749056	31.0	917891	14.3	831165	45.3	168835	56112	82773	52
9	749243	31.0	917805	14.3	831437	45.3	168563	56136	82757	51
10	749426	31.0	917719	14.3	831709	45.3	168291	56160	82741	50
11	9.749615		9.917634		9.831981		10.168019	56184	82724	49
12	749801	31.0	917548	14.3	832253	45.3	167747	56208	82708	48
13	749987	30.9	917462	14.3	832525	45.3	167475	56232	82692	47
14	750172	30.9	917376	14.3	832795	45.3	167204	56256	82675	46
15	750358	30.9	917290	14.3	833068	45.2	166932	56280	82659	45
16	750543	30.9	917204	14.3	833339	45.2	166661	56305	82643	44
17	750729	30.9	917118	14.4	833611	45.2	166389	56329	82626	43
18	750914	30.8	917032	14.4	833882	45.2	166118	56353	82610	42
19	751099	30.8	916946	14.4	834154	45.2	165846	56377	82593	41
20	751284	30.8	916859	14.4	834425	45.2	165575	56401	82577	40
21	9.751469		9.916773		9.834696		10.165304	56425	82561	39
22	751654	30.8	916687	14.4	834967	45.2	165303	56449	82544	38
23	751839	30.8	916600	14.4	835238	45.2	164762	56473	82528	37
24	752023	30.7	916514	14.4	835509	45.2	164491	56497	82511	36
25	752208	30.7	916427	14.4	835780	45.1	164220	56521	82495	35
26	752392	30.7	916341	14.4	836051	45.1	163949	56545	82478	34
27	752576	30.7	916254	14.4	836322	45.1	163678	56569	82462	33
28	752760	30.7	916167	14.5	836593	45.1	163407	56593	82446	32
29	752944	30.6	916081	14.5	836864	45.1	163136	56617	82429	31
30	753128	30.6	915994	14.5	837134	45.1	162866	56641	82413	30
31	9.753312		9.915907		9.837405		10.162595	56665	82396	29
32	753495	30.6	915820	14.5	837675	45.1	162325	56689	82380	28
33	753679	30.6	915733	14.5	837946	45.1	162054	56713	82363	27
34	753862	30.5	915646	14.5	838216	45.1	161784	56736	82347	26
35	754046	30.5	915559	14.5	838487	45.0	161513	56760	82330	25
36	754229	30.5	915472	14.5	838757	45.0	161243	56784	82314	24
37	754412	30.5	915385	14.5	839027	45.0	160973	56808	82297	23
38	754595	30.5	915297	14.5	839297	45.0	160703	56832	82281	22
39	754778	30.4	915210	14.5	839568	45.0	160432	56856	82264	21
40	754960	30.4	915123	14.6	839838	45.0	160162	56880	82248	20
41	9.755143		9.915035		9.840108		10.159892	56904	82231	19
42	755326	30.4	914948	14.6	840378	45.0	159622	56928	82214	18
43	755508	30.4	914860	14.6	840647	45.0	159353	56952	82198	17
44	755690	30.4	914773	14.6	840917	44.9	159083	56976	82181	16
45	755872	30.3	914685	14.6	841187	44.9	158813	57000	82165	15
46	756054	30.3	914598	14.6	841457	44.9	158543	57024	82148	14
47	756236	30.3	914510	14.6	841726	44.9	158274	57047	82132	13
48	756418	30.3	914422	14.6	841996	44.9	158004	57071	82115	12
49	756600	30.3	914334	14.6	842266	44.9	157734	57095	82098	11
50	756782	30.2	914246	14.7	842535	44.9	157465	57119	82082	10
51	9.756963		9.914158		9.842805		10.157195	57143	82065	9
52	757144	30.2	914070	14.7	843074	44.9	156926	57167	82048	8
53	757326	30.2	913982	14.7	843343	44.9	156657	57191	82032	7
54	757507	30.2	913894	14.7	843612	44.9	156388	57215	82015	6
55	757688	30.1	913806	14.7	843882	44.8	156118	57238	81999	5
56	757869	30.1	913718	14.7	844151	44.8	155848	57262	81982	4
57	758050	30.1	913630	14.7	844420	44.8	155580	57286	81965	3
58	758230	30.1	913541	14.7	844689	44.8	155311	57310	81949	2
59	758411	30.1	913453	14.7	844958	44.8	155042	57334	81932	1
60	758591	30.1	913365	14.7	845227	44.8	154773	57358	81915	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10'	Cosine.	D. 10'	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	9.758591	30.1	9.913365	14.7	9.845227	44.8	10.154773	57358	81915	60
1	758772	30.0	913276	14.7	845495	44.8	154504	57381	81899	59
2	758952	30.0	913187	14.8	845764	44.8	154236	57405	81882	58
3	759132	30.0	913099	14.8	846033	44.8	153967	57429	81865	57
4	759312	30.0	913010	14.8	846302	44.8	153698	57453	81848	56
5	759492	30.0	912922	14.8	846570	44.8	153430	57477	81832	55
6	759672	29.9	912833	14.8	846839	44.7	153161	57501	81815	54
7	759852	29.9	912744	14.8	847107	44.7	152893	57524	81798	53
8	760031	29.9	912655	14.8	847376	44.7	152624	57548	81782	52
9	760211	29.9	912566	14.8	847644	44.7	152356	57572	81765	51
10	760390	29.9	912477	14.8	847913	44.7	152087	57596	81748	50
11	9.760569	29.8	9.912388	14.8	9.848181	44.7	10.151819	57619	81731	49
12	760743	29.8	912299	14.9	848449	44.7	151551	57643	81714	48
13	760927	29.8	912210	14.9	848717	44.7	151283	57667	81698	47
14	761106	29.8	912121	14.9	848986	44.7	151014	57691	81681	46
15	761285	29.8	912031	14.9	849254	44.7	150746	57715	81664	45
16	761464	29.8	911942	14.9	849522	44.7	150478	57738	81647	44
17	761642	29.8	911853	14.9	849790	44.7	150210	57762	81631	43
18	761821	29.7	911763	14.9	850058	44.6	149942	57786	81614	42
19	761999	29.7	911674	14.9	850325	44.6	149675	57810	81597	41
20	762177	29.7	911584	14.9	850593	44.6	149407	57833	81580	40
21	9.762356	29.7	9.911495	14.9	9.850861	44.6	10.149139	57857	81563	39
22	762534	29.6	911405	14.9	851129	44.6	148871	57881	81546	38
23	762712	29.6	911315	14.9	851396	44.6	148604	57904	81530	37
24	762889	29.6	911226	15.0	851664	44.6	148336	57928	81513	36
25	763067	29.6	911136	15.0	851931	44.6	148069	57952	81496	35
26	763245	29.6	911046	15.0	852199	44.6	147801	57976	81479	34
27	763422	29.6	910956	15.0	852466	44.6	147534	57999	81462	33
28	763600	29.5	910866	15.0	852733	44.6	147267	58023	81445	32
29	763777	29.5	910776	15.0	853001	44.5	146999	58047	81428	31
30	763954	29.5	910686	15.0	853268	44.5	146732	58070	81412	30
31	9.764131	29.5	9.910596	15.0	9.853535	44.5	10.146465	58094	81395	29
32	764308	29.5	910506	15.0	853802	44.5	146198	58118	81378	28
33	764485	29.4	910415	15.0	854069	44.5	145931	58141	81361	27
34	764662	29.4	910325	15.1	854336	44.5	145664	58165	81344	26
35	764838	29.4	910235	15.1	854603	44.5	145397	58189	81327	25
36	765015	29.4	910144	15.1	854870	44.5	145130	58212	81310	24
37	765191	29.4	910054	15.1	855137	44.5	144863	58236	81293	23
38	765367	29.4	909963	15.1	855404	44.5	144596	58260	81276	22
39	765544	29.3	909873	15.1	855671	44.5	144329	58283	81259	21
40	765720	29.3	909782	15.1	855938	44.4	144062	58307	81242	20
41	9.765896	29.3	9.909691	15.1	9.856204	44.4	10.143796	58330	81225	19
42	766072	29.3	909601	15.1	856471	44.4	143529	58354	81208	18
43	766247	29.3	909510	15.1	856737	44.4	143263	58378	81191	17
44	766423	29.3	909419	15.1	857004	44.4	142996	58401	81174	16
45	766598	29.2	909328	15.2	857270	44.4	142730	58425	81157	15
46	766774	29.2	909237	15.2	857537	44.4	142463	58449	81140	14
47	766949	29.2	909146	15.2	857803	44.4	142197	58472	81123	13
48	767124	29.2	909055	15.2	858069	44.4	141931	58496	81106	12
49	767300	29.2	908964	15.2	858336	44.4	141664	58519	81089	11
50	767475	29.2	908873	15.2	858602	44.3	141398	58543	81072	10
51	9.767649	29.1	9.908781	15.2	9.858868	44.3	10.141132	58567	81055	9
52	767824	29.1	908690	15.2	859134	44.3	140866	58590	81038	8
53	767999	29.1	908599	15.2	859400	44.3	140600	58614	81021	7
54	768173	29.1	908507	15.2	859666	44.3	140334	58637	81004	6
55	768348	29.0	908416	15.3	859932	44.3	140068	58661	80987	5
56	768522	29.0	908324	15.3	860198	44.3	139802	58684	80970	4
57	768697	29.0	908233	15.3	860464	44.3	139536	58708	80953	3
58	768871	29.0	908141	15.3	860730	44.3	139270	58731	80936	2
59	769045	29.0	908049	15.3	861095	44.3	139005	58755	80919	1
60	769219	29.0	907958	15.3	861261	44.3	138739	58779	80902	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (36°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.769219		9.907958		9.861261		10.138739	58779	80902	60
1	769393	29.0	907866	15.3	861527	44.3	138473	58802	80885	59
2	769566	28.9	907774	15.3	861792	44.2	138208	58826	80867	58
3	769740	28.9	907682	15.3	862058	44.2	137942	58849	80850	57
4	769913	28.9	907590	15.3	862323	44.2	137677	58873	80833	56
5	770087	28.9	907498	15.3	862589	44.2	137411	58896	80816	55
6	770260	28.8	907406	15.3	862854	44.2	137146	58920	80799	54
7	770433	28.8	907314	15.4	863119	44.2	136881	58943	80782	53
8	770606	28.8	907222	15.4	863385	44.2	136615	58967	80765	52
9	770779	28.8	907129	15.4	863650	44.2	136350	58990	80748	51
10	770952	28.8	907037	15.4	863915	44.2	136085	59014	80730	50
11	9.771125		9.906945		9.864180		10.135820	59037	80713	49
12	771298	28.8	906852	15.4	864445	44.2	135555	59061	80696	48
13	771470	28.7	906760	15.4	864710	44.2	135290	59084	80679	47
14	771643	28.7	906667	15.4	864975	44.1	135025	59108	80662	46
15	771815	28.7	906575	15.4	865240	44.1	134760	59131	80644	45
16	771987	28.7	906482	15.4	865505	44.1	134495	59154	80627	44
17	772159	28.7	906389	15.5	865770	44.1	134230	59178	80610	43
18	772331	28.6	906296	15.5	866035	44.1	133965	59201	80593	42
19	772503	28.6	906204	15.5	866300	44.1	133700	59225	80576	41
20	772675	28.6	906111	15.5	866564	44.1	133435	59248	80558	40
21	9.772847		9.906018		9.866829		10.133171	59272	80541	39
22	773018	28.6	905925	15.5	867094	44.1	132960	59295	80524	38
23	773190	28.6	905832	15.5	867358	44.1	132695	59318	80507	37
24	773361	28.5	905739	15.5	867623	44.1	132430	59342	80489	36
25	773533	28.5	905645	15.5	867887	44.1	132165	59365	80472	35
26	773704	28.5	905552	15.5	868152	44.0	131899	59389	80455	34
27	773875	28.5	905459	15.5	868416	44.0	131634	59412	80438	33
28	774046	28.5	905366	15.6	868680	44.0	131369	59436	80422	32
29	774217	28.5	905272	15.6	868945	44.0	131105	59459	80405	31
30	774388	28.4	905179	15.6	869209	44.0	13091	59482	80388	30
31	9.774558		9.905085		9.869473		10.130527	59506	80368	29
32	774729	28.4	904992	15.6	869737	44.0	130263	59529	80351	28
33	774899	28.4	904898	15.6	870001	44.0	129999	59552	80334	27
34	775070	28.4	904804	15.6	870265	44.0	129735	59576	80316	26
35	775240	28.4	904711	15.6	870529	44.0	129471	59599	80299	25
36	775410	28.3	904617	15.6	870793	44.0	129207	59622	80282	24
37	775580	28.3	904523	15.6	871057	44.0	128943	59646	80264	23
38	775750	28.3	904429	15.7	871321	44.0	128679	59669	80247	22
39	775920	28.3	904335	15.7	871585	44.0	128415	59693	80230	21
40	776090	28.3	904241	15.7	871849	43.9	128151	59716	80212	20
41	9.776259		9.904147		9.872112		10.127888	59739	80195	19
42	776429	28.2	904053	15.7	872376	43.9	127624	59763	80178	18
43	776598	28.2	903959	15.7	872640	43.9	127360	59786	80160	17
44	776768	28.2	903864	15.7	872903	43.9	127097	59809	80143	16
45	776937	28.2	903770	15.7	873167	43.9	126833	59832	80125	15
46	777107	28.2	903676	15.7	873430	43.9	126570	59856	80108	14
47	777275	28.1	903581	15.7	873694	43.9	126306	59879	80091	13
48	777444	28.1	903487	15.7	873957	43.9	126043	59902	80073	12
49	777613	28.1	903392	15.8	874220	43.9	125780	59926	80056	11
50	777781	28.1	903298	15.8	874484	43.9	125516	59949	80038	10
51	9.777950		9.903202		9.874747		10.125253	59972	80021	9
52	778119	28.1	903108	15.8	875010	43.9	124990	59995	80003	8
53	778287	28.0	903014	15.8	875273	43.8	124727	60019	79986	7
54	778455	28.0	902919	15.8	875536	43.8	124464	60042	79968	6
55	778624	28.0	902824	15.8	875800	43.8	124200	60065	79951	5
56	778792	28.0	902729	15.8	876063	43.8	123937	60089	79934	4
57	778960	28.0	902634	15.8	876326	43.8	123674	60112	79916	3
58	779128	28.0	902539	15.9	876589	43.8	123411	60135	79899	2
59	779295	27.9	902444	15.9	876851	43.8	123149	60158	79881	1
60	779463		902349		877114		122886	60182	79864	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.779463		9.902349		9.877114		10.122886	60182	79864	60
1	779531	27.9	902253	15.9	877377	43.8	122623	60205	79846	59
2	779798	27.9	902158	15.9	877640	43.8	122360	60228	79829	58
3	779936	27.9	902033	15.9	877903	43.8	122097	60251	79811	57
4	780133	27.9	901967	15.9	878165	43.8	121835	60274	79793	56
5	780300	27.8	901872	15.9	878428	43.8	121572	60298	79776	55
6	780467	27.8	901776	15.9	878691	43.8	121309	60321	79758	54
7	780634	27.8	901681	15.9	878953	43.7	121047	60344	79741	53
8	780801	27.8	901585	15.9	879216	43.7	120784	60367	79723	52
9	780968	27.8	901490	15.9	879478	43.7	120522	60390	79706	51
10	781134	27.8	901394	16.0	879741	43.7	120259	60414	79688	50
11	9.781301	27.7	9.901298	16.0	9.880003	43.7	10.119997	60437	79671	49
12	781468	27.7	901202	16.0	880265	43.7	119735	60460	79658	48
13	781634	27.7	901106	16.0	880528	43.7	119472	60483	79635	47
14	781809	27.7	901010	16.0	880790	43.7	119210	60506	79618	46
15	781966	27.7	900914	16.0	881052	43.7	118948	60529	79600	45
16	782132	27.7	900818	16.0	881314	43.7	118686	60553	79583	44
17	782298	27.6	900722	16.0	881576	43.7	118424	60576	79565	43
18	782464	27.6	900626	16.0	881839	43.7	118161	60599	79547	42
19	782630	27.6	900529	16.0	882101	43.7	117899	60622	79530	41
20	782796	27.6	900433	16.1	882363	43.6	117637	60645	79512	40
21	9.782961	27.6	9.900337	16.1	9.882625	43.6	10.117375	60668	79494	39
22	783127	27.6	900242	16.1	882887	43.6	117113	60691	79477	38
23	783292	27.5	900144	16.1	883148	43.6	116852	60714	79459	37
24	783458	27.5	900047	16.1	883410	43.6	116590	60738	79441	36
25	783623	27.5	899951	16.1	883672	43.6	116328	60761	79424	35
26	783788	27.5	899854	16.1	883934	43.6	116066	60784	79406	34
27	783953	27.5	899757	16.1	884196	43.6	115804	60807	79388	33
28	784118	27.5	899660	16.1	884457	43.6	115543	60830	79371	32
29	784282	27.4	899564	16.1	884719	43.6	115281	60853	79353	31
30	784447	27.4	899467	16.2	884980	43.6	115020	60876	79335	30
31	9.784612	27.4	9.899370	16.2	9.885242	43.6	10.114758	60899	79318	29
32	784776	27.4	899273	16.2	885503	43.6	114497	60922	79300	28
33	784941	27.4	899176	16.2	885765	43.6	114235	60945	79282	27
34	785105	27.4	899078	16.2	886026	43.6	113974	60968	79264	26
35	785269	27.3	898981	16.2	886288	43.6	113712	60991	79247	25
36	785433	27.3	898884	16.2	886549	43.5	113451	61015	79229	24
37	785597	27.3	898787	16.2	886810	43.5	113190	61038	79211	23
38	785761	27.3	898689	16.2	887072	43.5	112928	61061	79193	22
39	785925	27.3	898592	16.2	887333	43.5	112667	61084	79176	21
40	786089	27.3	898494	16.3	887594	43.5	112405	61107	79158	20
41	9.786252	27.2	9.898397	16.3	9.887855	43.5	10.112145	61130	79140	19
42	786416	27.2	898299	16.3	888116	43.5	111884	61153	79122	18
43	786579	27.2	898202	16.3	888377	43.5	111623	61176	79105	17
44	786742	27.2	898104	16.3	888639	43.5	111361	61199	79087	16
45	786905	27.2	898006	16.3	888900	43.5	111100	61222	79069	15
46	787069	27.2	897908	16.3	889160	43.5	110840	61245	79051	14
47	787232	27.1	897810	16.3	889421	43.5	110579	61268	79033	13
48	787395	27.1	897712	16.3	889682	43.5	110318	61291	79015	12
49	787557	27.1	897614	16.3	889943	43.5	110057	61314	78998	11
50	787720	27.1	897516	16.3	890204	43.4	109796	61337	78980	10
51	9.787883	27.1	9.897418	16.4	9.890465	43.4	10.109535	61360	78962	9
52	788045	27.1	897320	16.4	890725	43.4	109275	61383	78944	8
53	788208	27.1	897222	16.4	890986	43.4	109014	61406	78926	7
54	788370	27.0	897123	16.4	891247	43.4	108753	61429	78908	6
55	788532	27.0	897025	16.4	891507	43.4	108493	61451	78891	5
56	788694	27.0	896926	16.4	891768	43.4	108232	61474	78873	4
57	788856	27.0	896828	16.4	892028	43.4	107972	61497	78855	3
58	789018	27.0	896729	16.4	892289	43.4	107711	61520	78837	2
59	789180	27.0	896631	16.4	892549	43.4	107451	61543	78819	1
60	789342	27.0	896532	16.4	892810	43.4	107190	61566	78801	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II.

Log. Sines and Tangents. (38°) Natural Sines.

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.789342	26.9	9.896532	16.4	9.892310	43.4	10.107190	61566	78801	60
1	789504	26.9	896433	16.5	893070	43.4	106690	61589	78783	59
2	789665	26.9	896335	16.5	893331	43.4	106669	61612	78765	58
3	789827	26.9	896236	16.5	893591	43.4	106409	61635	78747	57
4	789988	26.9	896137	16.5	893851	43.4	106149	61658	78729	56
5	790149	26.9	896038	16.5	894111	43.4	105889	61681	78711	55
6	790310	26.8	895939	16.5	894371	43.4	105629	61704	78694	54
7	790471	26.8	895840	16.5	894632	43.4	105368	61727	78676	53
8	790632	26.8	895741	16.5	894892	43.3	105108	61749	78658	52
9	790793	26.8	895641	16.5	895152	43.3	104848	61772	78640	51
10	790954	26.8	895542	16.5	895412	43.3	104588	61795	78622	50
11	9.791115	26.8	9.895443	16.6	9.895672	43.3	10.104328	61818	78604	49
12	791275	26.7	895343	16.6	895932	43.3	104068	61841	78586	48
13	791436	26.7	895244	16.6	896192	43.3	103808	61864	78568	47
14	791596	26.7	895145	16.6	896452	43.3	103548	61887	78550	46
15	791757	26.7	895045	16.6	896712	43.3	103288	61909	78532	45
16	791917	26.7	894945	16.6	896971	43.3	103029	61932	78514	44
17	792077	26.7	894846	16.6	897231	43.3	102769	61955	78496	43
18	792237	26.6	894746	16.6	897491	43.3	102509	61978	78478	42
19	792397	26.6	894646	16.6	897751	43.3	102249	62001	78460	41
20	792557	26.6	894546	16.6	898010	43.3	101990	62024	78442	40
21	9.792716	26.6	9.894446	16.7	9.898270	43.3	10.101730	62046	78424	39
22	792876	26.6	894346	16.7	898530	43.3	101470	62069	78405	38
23	793035	26.6	894246	16.7	898789	43.3	101211	62092	78387	37
24	793195	26.5	894146	16.7	899049	43.2	100951	62115	78369	36
25	793354	26.5	894046	16.7	899308	43.2	100692	62138	78351	35
26	793514	26.5	893946	16.7	899568	43.2	100432	62160	78333	34
27	793673	26.5	893846	16.7	899827	43.2	100173	62183	78315	33
28	793832	26.5	893745	16.7	900086	43.2	099914	62206	78297	32
29	793991	26.5	893645	16.7	900346	43.2	099654	62229	78279	31
30	794150	26.4	893544	16.7	900605	43.2	099395	62251	78261	30
31	9.794308	26.4	9.893444	16.8	9.900864	43.2	10.099136	62274	78243	29
32	794467	26.4	893343	16.8	901124	43.2	098876	62297	78225	28
33	794626	26.4	893243	16.8	901383	43.2	098617	62320	78207	27
34	794784	26.4	893142	16.8	901642	43.2	098358	62342	78188	26
35	794942	26.4	893041	16.8	901901	43.2	098099	62365	78170	25
36	795101	26.4	892940	16.8	902160	43.2	097840	62388	78152	24
37	795259	26.3	892839	16.8	902419	43.2	097581	62411	78134	23
38	795417	26.3	892739	16.8	902679	43.2	097321	62433	78116	22
39	795575	26.3	892638	16.8	902938	43.2	097062	62456	78098	21
40	795733	26.3	892536	16.8	903197	43.1	096803	62479	78079	20
41	9.795891	26.3	9.892435	16.9	9.903455	43.1	10.096545	62502	78061	19
42	796049	26.3	892334	16.9	903714	43.1	096286	62524	78043	18
43	796206	26.3	892233	16.9	903973	43.1	096027	62547	78025	17
44	796364	26.2	892132	16.9	904232	43.1	095768	62570	78007	16
45	796521	26.2	892030	16.9	904491	43.1	095509	62592	77988	15
46	796679	26.2	891929	16.9	904750	43.1	095250	62615	77970	14
47	796836	26.2	891827	16.9	905008	43.1	094992	62638	77952	13
48	796993	26.2	891726	16.9	905267	43.1	094733	62660	77934	12
49	797150	26.1	891624	16.9	905526	43.1	094474	62683	77916	11
50	797307	26.1	891523	17.0	905784	43.1	094216	62706	77897	10
51	9.797464	26.1	9.891421	17.0	9.906043	43.1	10.093957	62728	77879	9
52	797621	26.1	891319	17.0	906302	43.1	093698	62751	77861	8
53	797777	26.1	891217	17.0	906560	43.1	093440	62774	77843	7
54	797934	26.1	891115	17.0	906819	43.1	093181	62796	77824	6
55	798091	26.1	891013	17.0	907077	43.1	092923	62819	77805	5
56	798247	26.1	890911	17.0	907336	43.1	092664	62842	77788	4
57	798403	26.0	890809	17.0	907594	43.1	092406	62864	77769	3
58	798560	26.0	890707	17.0	907852	43.1	092148	62887	77751	2
59	798716	26.0	890605	17.0	908111	43.0	091889	62909	77733	1
60	798872	26.0	890503	17.0	908369	43.0	091631	62932	77715	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine	

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.798772	26.0	9.890503	17.0	9.903369	43.0	10.091631	62932	77715	60
1	799028	26.0	890400	17.1	903328	43.0	091372	62955	77696	59
2	799184	26.0	890298	17.1	903883	43.0	091114	62977	77678	58
3	799339	25.9	890195	17.1	904444	43.0	090855	63004	77660	57
4	799495	25.9	890093	17.1	904992	43.0	090598	63022	77641	56
5	799651	25.9	889990	17.1	905550	43.0	090340	63045	77623	55
6	799806	25.9	889888	17.1	906118	43.0	090082	63068	77605	54
7	799962	25.9	889785	17.1	910177	43.0	089823	63090	77586	53
8	800117	25.9	889682	17.1	910435	43.0	089565	63113	77568	52
9	800272	25.8	889579	17.1	910693	43.0	089307	63135	77550	51
10	800427	25.8	889477	17.1	910951	43.0	089049	63158	77531	50
11	9.800582	25.8	9.889374	17.2	9.911209	43.0	10.088791	93180	77513	49
12	800737	25.8	889271	17.2	911467	43.0	088533	63203	77494	48
13	800892	25.8	889168	17.2	911724	43.0	088276	63225	77476	47
14	801047	25.8	889064	17.2	911982	43.0	088018	63248	77458	46
15	801201	25.8	888961	17.2	912240	43.0	087760	63271	77439	45
16	801356	25.7	888858	17.2	912498	43.0	087502	63293	77421	44
17	801511	25.7	888755	17.2	912756	43.0	087244	63316	77402	43
18	801665	25.7	888651	17.2	913014	43.0	086986	63338	77384	42
19	801819	25.7	888548	17.2	913271	42.9	086729	63361	77366	41
20	801973	25.7	888444	17.2	913529	42.9	086471	63383	77347	40
21	9.802128	25.7	9.888341	17.3	9.913787	42.9	10.086213	63405	77329	39
22	802282	25.6	888237	17.3	914044	42.9	085956	63428	77310	38
23	802436	25.6	888134	17.3	914302	42.9	085698	63451	77292	37
24	802589	25.6	888030	17.3	914560	42.9	085440	63473	77273	36
25	802743	25.6	887926	17.3	914817	42.9	085183	63496	77255	35
26	802897	25.6	887822	17.3	915075	42.9	084925	63518	77236	34
27	803050	25.6	887718	17.3	915332	42.9	084668	63540	77218	33
28	803204	25.6	887614	17.3	915590	42.9	084410	63563	77199	32
29	803357	25.5	887510	17.3	915847	42.9	084153	63585	77181	31
30	803511	25.5	887406	17.4	916104	42.9	083896	63608	77162	30
31	9.803664	25.5	9.887302	17.4	9.916362	42.9	10.083638	63630	77144	29
32	803817	25.5	887198	17.4	916619	42.9	083381	63653	77125	28
33	803970	25.5	887093	17.4	916877	42.9	083123	63675	77107	27
34	804123	25.5	886989	17.4	917134	42.9	082866	63698	77088	26
35	804276	25.4	886885	17.4	917391	42.9	082609	63720	77070	25
36	804428	25.4	886780	17.4	917648	42.9	082352	63742	77051	24
37	804581	25.4	886676	17.4	917905	42.9	082095	63765	77033	23
38	804734	25.4	886571	17.4	918163	42.8	081837	63787	77014	22
39	804886	25.4	886466	17.4	918420	42.8	081580	63810	76996	21
40	805039	25.4	886362	17.5	918677	42.8	081323	63832	76977	20
41	9.805191	25.4	9.886257	17.5	9.918934	42.8	10.081066	63854	76959	19
42	805343	25.3	886152	17.5	919191	42.8	080809	63877	76940	18
43	805495	25.3	886047	17.5	919448	42.8	080552	63899	76921	17
44	805647	25.3	885942	17.5	919705	42.8	080295	63922	76903	16
45	805799	25.3	885837	17.5	919962	42.8	080038	63944	76884	15
46	805951	25.3	885732	17.5	920219	42.8	079781	63966	76865	14
47	806103	25.3	885627	17.5	920476	42.8	079524	63989	76847	13
48	806254	25.3	885522	17.5	920733	42.8	079267	64011	76828	12
49	806406	25.2	885416	17.5	920990	42.8	079010	64033	76810	11
50	806557	25.2	885311	17.6	921247	42.8	078753	64056	76791	10
51	9.806709	25.2	9.885205	17.6	9.921503	42.8	10.078497	64078	76772	9
52	806860	25.2	885100	17.6	921760	42.8	078240	64100	76754	8
53	807011	25.2	884994	17.6	922017	42.8	077983	64123	76735	7
54	807163	25.2	884889	17.6	922274	42.8	077726	64145	76717	6
55	807314	25.2	884783	17.6	922530	42.8	077470	64167	76698	5
56	807465	25.1	884677	17.6	922787	42.8	077213	64190	76679	4
57	807615	25.1	884572	17.6	923044	42.8	076956	64212	76661	3
58	807766	25.1	884466	17.6	923300	42.8	076700	64234	76642	2
59	807917	25.1	884360	17.6	923557	42.7	076443	64256	76623	1
60	808067	25.1	884254	17.6	923813		076187	64279	76604	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II. Log. Sines and Tangents. (40°) Natural Sines.

<i>r</i>	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	<i>r</i>
0	9.805037	25.1	9.884254	17.7	9.923813	42.7	10.076187	64279	76604	60
1	808218	25.1	884148	17.7	924070	42.7	075930	64301	76586	59
2	808338	25.1	884042	17.7	924327	42.7	075643	64323	76567	58
3	808519	25.0	883936	17.7	924583	42.7	075417	64346	76548	57
4	808669	25.0	883829	17.7	924840	42.7	075160	64368	76530	56
5	808819	25.0	883723	17.7	925096	42.7	074904	64390	76511	55
6	808969	25.0	883617	17.7	925352	42.7	074648	64412	76492	54
7	809119	25.0	883510	17.7	925609	42.7	074391	64435	76473	53
8	809269	25.0	883404	17.7	925865	42.7	074135	64457	76455	52
9	809419	24.9	883297	17.8	926122	42.7	073878	64479	76436	51
10	809569	24.9	883191	17.8	926378	42.7	073622	64501	76417	50
11	9.809718	24.9	9.883084	17.8	9.926634	42.7	10.073366	64524	76398	49
12	809868	24.9	882977	17.8	926890	42.7	073110	64546	76380	48
13	810017	24.9	882871	17.8	927147	42.7	072853	64568	76361	47
14	810167	24.9	882764	17.8	927403	42.7	072597	64590	76342	46
15	810316	24.8	882657	17.8	927659	42.7	072341	64612	76323	45
16	810465	24.8	882550	17.8	927915	42.7	072085	64635	76304	44
17	810614	24.8	882443	17.8	928171	42.7	071829	64657	76286	43
18	810763	24.8	882336	17.8	928427	42.7	071573	64679	76267	42
19	810912	24.8	882229	17.9	928683	42.7	071317	64701	76248	41
20	811061	24.8	882121	17.9	928940	42.7	071060	64723	76229	40
21	9.811210	24.8	9.882014	17.9	9.929196	42.7	10.070804	64746	76210	39
22	811358	24.7	881907	17.9	929452	42.7	070548	64768	76192	38
23	811507	24.7	881799	17.9	929708	42.7	070292	64790	76173	37
24	811655	24.7	881692	17.9	929964	42.6	070036	64812	76154	36
25	811804	24.7	881584	17.9	930220	42.6	069780	64834	76135	35
26	811952	24.7	881477	17.9	930475	42.6	069525	64856	76116	34
27	812100	24.7	881369	17.9	930731	42.6	069269	64878	76097	33
28	812248	24.7	881261	18.0	930987	42.6	069013	64901	76078	32
29	812396	24.6	881153	18.0	931243	42.6	068757	64923	76059	31
30	812544	24.6	881046	18.0	931499	42.6	068501	64945	76041	30
31	9.812692	24.6	9.880938	18.0	9.931755	42.6	10.068245	64967	76022	29
32	812840	24.6	880830	18.0	932010	42.6	067990	64989	76003	28
33	812988	24.6	880722	18.0	932266	42.6	067734	65011	75984	27
34	813135	24.6	880613	18.0	932522	42.6	067478	65033	75965	26
35	813283	24.6	880505	18.0	932778	42.6	067222	65055	75946	25
36	813430	24.5	880397	18.0	933033	42.6	066967	65077	75927	24
37	813578	24.5	880289	18.1	933289	42.6	066711	65100	75908	23
38	813725	24.5	880180	18.1	933545	42.6	066455	65122	75889	22
39	813872	24.5	880072	18.1	933800	42.6	066200	65144	75870	21
40	814019	24.5	879963	18.1	934056	42.6	065944	65166	75851	20
41	9.814166	24.5	9.879855	18.1	9.934311	42.6	10.065689	65188	75832	19
42	814313	24.5	879746	18.1	934567	42.6	065433	65210	75813	18
43	814460	24.4	879637	18.1	934823	42.6	065177	65232	75794	17
44	814607	24.4	879529	18.1	935078	42.6	064922	65254	75775	16
45	814753	24.4	879420	18.1	935333	42.6	064667	65276	75756	15
46	814900	24.4	879311	18.1	935589	42.6	064411	65298	75738	14
47	815046	24.4	879202	18.2	935844	42.6	064156	65320	75719	13
48	815193	24.4	879093	18.2	936100	42.6	063900	65342	75700	12
49	815339	24.4	878984	18.2	936355	42.6	063645	65364	75681	11
50	815485	24.3	878875	18.2	936610	42.6	063390	65386	75661	10
51	9.815631	24.3	9.878766	18.2	9.936866	42.6	10.063134	65408	75642	9
52	815778	24.3	878766	18.2	937121	42.5	062879	65430	75623	8
53	815924	24.3	878657	18.2	937376	42.5	062624	65452	75604	7
54	816069	24.3	878548	18.2	937632	42.5	062368	65474	75585	6
55	816215	24.3	878438	18.2	937887	42.5	062113	65496	75566	5
56	816361	24.3	878329	18.2	938142	42.5	061858	65518	75547	4
57	816507	24.2	878219	18.3	938398	42.5	061602	65540	75528	3
58	816652	24.2	878109	18.3	938653	42.5	061347	65562	75509	2
59	816798	24.2	877999	18.3	938909	42.5	061092	65584	75490	1
60	816943	24.2	877880	18.3	939163	42.5	060837	65606	75471	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	<i>r</i>

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cctang.	N. sine.	N. cos.	
0	9.816943		9.877780		9.939163		10.030837	65605	75471	60
1	817088	24.2	877670	18.3	939418	42.5	050582	65628	75452	59
2	817233	24.2	877560	18.3	939673	42.5	050327	65650	75433	58
3	817379	24.2	877450	18.3	939928	42.5	060072	65672	75414	57
4	817524	24.2	877340	18.3	940183	42.5	059817	65694	75395	56
5	817668	24.1	877230	18.3	940438	42.5	059562	65716	75375	55
6	817813	24.1	877120	18.4	940694	42.5	059306	65738	75356	54
7	817958	24.1	877010	18.4	940949	42.5	059051	65759	75337	53
8	818103	24.1	876899	18.4	941204	42.5	058796	65781	75318	52
9	818247	24.1	876789	18.4	941458	42.5	058542	65803	75299	51
10	818392	24.1	876678	18.4	941714	42.5	058286	65825	75280	50
11	9.818536		9.876568		9.941958		10.058032	65847	75261	49
12	818681	24.0	876457	18.4	942223	42.5	057777	65869	75241	48
13	818825	24.0	876347	18.4	942478	42.5	057522	65891	75222	47
14	818969	24.0	876236	18.4	942733	42.5	057267	65913	75203	46
15	819113	24.0	876125	18.5	942988	42.5	057012	65935	75184	45
16	819257	24.0	876014	18.5	943243	42.5	056757	65956	75165	44
17	819401	24.0	875904	18.5	943498	42.5	056502	65978	75146	43
18	819545	24.0	875793	18.5	943752	42.5	056248	66000	75126	42
19	819689	23.9	875682	18.5	944007	42.5	055993	66022	75107	41
20	819832	23.9	875571	18.5	944262	42.5	055738	66044	75088	40
21	9.819976		9.875459		9.944517		10.055483	66066	75069	39
22	820120	23.9	875348	18.5	944771	42.5	055229	66088	75050	38
23	820263	23.9	875237	18.5	945026	42.4	054974	66109	75030	37
24	820405	23.9	875126	18.5	945281	42.4	054719	66131	75011	36
25	820550	23.9	875014	18.6	945535	42.4	054465	66153	74992	35
26	820693	23.8	874903	18.6	945790	42.4	054210	66175	74973	34
27	820836	23.8	874791	18.6	946045	42.4	053955	66197	74953	33
28	820979	23.8	874680	18.6	946299	42.4	053701	66218	74934	32
29	821122	23.8	874568	18.6	946554	42.4	053446	66240	74915	31
30	821265	23.8	874456	18.6	946808	42.4	053192	66262	74896	30
31	9.821407		9.874344		9.947053		10.052937	66284	74876	29
32	821550	23.8	874332	18.6	947318	42.4	052682	66305	74857	28
33	821693	23.8	874212	18.7	947572	42.4	052428	66327	74838	27
34	821835	23.7	874099	18.7	947826	42.4	052174	66349	74818	26
35	821977	23.7	873986	18.7	948081	42.4	051919	66371	74799	25
36	822120	23.7	873874	18.7	948336	42.4	051664	66393	74780	24
37	822262	23.7	873762	18.7	948590	42.4	051410	66414	74760	23
38	822404	23.7	873650	18.7	948844	42.4	051156	66436	74741	22
39	822546	23.7	873548	18.7	949099	42.4	050901	66458	74722	21
40	822688	23.7	873435	18.7	949353	42.4	050647	66480	74703	20
41	9.822830		9.873323		9.949507		10.050393	66501	74683	19
42	822972	23.6	873310	18.7	949862	42.4	050138	66523	74663	18
43	823114	23.6	872998	18.8	950116	42.4	049884	66545	74644	17
44	823255	23.6	872885	18.8	950370	42.4	049630	66566	74625	16
45	823397	23.6	872772	18.8	950625	42.4	049375	66588	74606	15
46	823539	23.6	872659	18.8	950879	42.4	049121	66610	74586	14
47	823680	23.6	872547	18.8	951133	42.4	048867	66632	74567	13
48	823821	23.5	872434	18.8	951388	42.4	048612	66653	74548	12
49	823963	23.5	872321	18.8	951642	42.4	048358	66675	74529	11
50	824104	23.5	872208	18.8	951896	42.4	048104	66697	74509	10
51	9.824245		9.872095		9.952159		10.047850	66718	74489	9
52	824386	23.5	871981	18.9	952405	42.4	047595	66740	74470	8
53	824527	23.5	871868	18.9	952659	42.4	047341	66762	74451	7
54	824668	23.5	871755	18.9	952913	42.4	047087	66783	74431	6
55	824808	23.4	871641	18.9	953167	42.3	046833	66805	74412	5
56	824949	23.4	871528	18.9	953421	42.3	046579	66827	74392	4
57	825090	23.4	871414	18.9	953675	42.3	046325	66848	74373	3
58	825230	23.4	871301	18.9	953929	42.3	046071	66870	74353	2
59	825371	23.4	871187	18.9	954183	42.3	045817	66891	74334	1
60	825511	23.4	871073	18.9	954437	42.3	045563	66913	74314	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	



TABLE II.

Log. Sines and Tangents. (42°) Natural Sines.

63

	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	9.825511	23.4	9.871073	19.0	9.954437	42.3	10.045563	66913	74314	60
1	825651	23.3	870060	19.0	954691	42.3	045309	66935	74295	59
2	825791	23.3	870846	19.0	954945	42.3	045055	66956	74276	58
3	825931	3.3	870732	19.0	955200	42.3	044800	66978	74256	57
4	826071	23.3	870618	19.0	955454	42.3	044546	66999	74237	56
5	826211	23.3	870504	19.0	955707	42.3	044293	67021	74217	55
6	826351	23.3	870390	19.0	955961	42.3	044039	67043	74198	54
7	826491	23.3	870276	19.0	956215	42.3	043785	67064	74178	53
8	826631	23.3	870161	19.0	956469	42.3	043531	67086	74159	52
9	826770	23.2	870047	19.0	956723	42.3	043277	67107	74139	51
10	826910	23.2	8.9933	19.1	956977	42.3	043023	67129	74120	50
11	9.8270.9	23.2	9.869318	19.1	9.957231	42.3	10.042769	67151	74100	49
12	827189	23.2	869704	19.1	957485	42.3	042515	67172	74080	48
13	8273.8	23.2	869589	19.1	957739	42.3	042261	67194	74061	47
14	827467	23.2	869474	19.1	957993	42.3	042007	67215	74041	46
15	827606	23.2	869360	19.1	958246	42.3	041754	67237	74022	45
16	827745	23.2	869245	19.1	958500	42.3	041500	67258	74002	44
17	827884	23.1	869130	19.1	958754	42.3	041246	67280	73983	43
18	828023	23.1	869015	19.1	959008	42.3	040992	67301	73963	42
19	828162	23.1	8.8900	19.2	959262	42.3	040738	67323	73944	41
20	828301	23.1	868785	19.2	959516	42.3	040484	67344	73924	40
21	9.828439	23.1	9.868670	19.2	9.959769	42.3	10.040231	67366	73904	39
22	828578	23.1	868555	19.2	960023	42.3	039977	67387	73885	38
23	828716	23.1	868440	19.2	960277	42.3	039723	67409	73866	37
24	828855	23.0	8.83324	19.2	960531	42.3	039469	67430	73846	36
25	828993	23.0	868209	19.2	960784	42.3	039216	67452	73826	35
26	829131	23.0	868093	19.2	961038	42.3	038962	67473	73806	34
27	829269	23.0	867978	19.2	961291	42.3	038709	67495	73787	33
28	829407	23.0	867862	19.3	961545	42.3	038455	67516	73767	32
29	829545	23.0	867747	19.3	961799	42.3	038201	67538	73747	31
30	829683	23.0	867631	19.3	962052	42.3	037948	67559	73728	30
31	9.829821	23.0	9.867515	19.3	9.962306	42.3	10.037694	67580	73708	29
32	829959	22.9	867399	19.3	962560	42.3	037440	67602	73688	28
33	830097	22.9	867283	19.3	962813	42.3	037187	67623	73669	27
34	830234	22.9	867167	19.3	963067	42.3	036933	67645	73649	26
35	830372	22.9	867051	19.3	963320	42.3	036680	67666	73629	25
36	830509	22.9	866935	19.4	963574	42.3	036426	67688	73610	24
37	830646	22.9	866819	19.4	963827	42.3	036173	67709	73590	23
38	830784	22.9	866703	19.4	964081	42.3	035919	67730	73570	22
39	830921	22.8	866586	19.4	964335	42.3	035665	67752	73551	21
40	831058	22.8	866470	19.4	964588	42.2	035412	67773	73531	20
41	9.831195	22.8	9.866353	19.4	9.964842	42.2	10.035158	67795	73511	19
42	831332	22.8	866237	19.4	965095	42.2	034905	67816	73491	18
43	831469	22.8	866120	19.4	965349	42.2	034651	67837	73472	17
44	831605	22.8	866004	19.4	965602	42.2	034398	67859	73452	16
45	831742	22.8	865887	19.5	965855	42.2	034145	67880	73432	15
46	831879	22.8	865770	19.5	966109	42.2	033891	67901	73413	14
47	832015	22.7	865653	19.5	966362	42.2	033638	67923	73393	13
48	832152	22.7	865536	19.5	966616	42.2	033384	67944	73373	12
49	832288	22.7	865419	19.5	966869	42.2	033131	67965	73353	11
50	832425	22.7	865302	19.5	967123	42.2	032877	67987	73333	10
51	9.832561	22.7	9.865185	19.5	9.967376	42.2	10.032624	68008	73314	9
52	832697	22.7	865068	19.5	967629	42.2	032371	68029	73294	8
53	832833	22.7	864950	19.5	967883	42.2	032117	68051	73274	7
54	832969	22.6	864833	19.6	968136	42.2	031864	68072	73254	6
55	833105	22.6	864716	19.6	968389	42.2	031611	68093	73234	5
56	833241	22.6	864598	19.6	968643	42.2	031357	68115	73214	4
57	833377	22.6	864481	19.6	968896	42.2	031104	68136	73195	3
58	833512	22.6	864363	19.6	969149	42.2	030851	68157	73175	2
59	833648	22.6	864245	19.6	969403	42.2	030597	68179	73155	1
60	833783	22.6	864127	19.6	969656	42.2	030344	68200	73135	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

47 Degrees.

°	Sine.	D. 10"	Cosine.	D. 10"	Tang.	D. 10"	Cotang.	N. sine.	N. cos.	
0	833783	22.6	9.864127	19.6	9.969656	42.2	10.030344	68200	73135	60
1	833919	22.5	864010	19.6	969909	42.2	030001	68221	73116	59
2	834054	22.5	863892	19.7	970162	42.2	029838	68242	73096	58
3	834189	22.5	863774	19.7	970416	42.2	029584	68264	73076	57
4	834325	22.5	863656	19.7	970669	42.2	029331	68285	73056	56
5	834460	22.5	863538	19.7	970922	42.2	029078	68306	73036	55
6	834595	22.5	863419	19.7	971175	42.2	028825	68327	73016	54
7	834730	22.5	863301	19.7	971429	42.2	028571	68349	72996	53
8	834865	22.5	863183	19.7	971682	42.2	028318	68370	72976	52
9	834999	22.4	863064	19.7	971935	42.2	028065	68391	72957	51
10	835134	22.4	862946	19.8	972188	42.2	027812	68412	72937	50
11	9.835269	22.4	9.862827	19.8	9.972441	42.2	10.027559	68434	72917	49
12	835403	22.4	862709	19.8	972694	42.2	027306	68455	72897	48
13	835538	22.4	862590	19.8	972948	42.2	027052	68476	72877	47
14	835672	22.4	862471	19.8	973201	42.2	026799	68497	72857	46
15	835807	22.4	862353	19.8	973454	42.2	026546	68518	72837	45
16	835941	22.4	862234	19.8	973707	42.2	026293	68539	72817	44
17	836075	22.3	862115	19.8	973960	42.2	026040	68561	72797	43
18	836209	22.3	861996	19.8	974213	42.2	025787	68582	72777	42
19	836343	22.3	861877	19.8	974466	42.2	025534	68603	72757	41
20	836477	22.3	861758	19.8	974719	42.2	025281	68624	72737	40
21	9.836611	22.3	9.861638	19.9	9.974973	42.2	10.025027	68645	72717	39
22	836745	22.3	861519	19.9	975226	42.2	024774	68666	72697	38
23	836878	22.3	861400	19.9	975479	42.2	024521	68688	72677	37
24	837012	22.2	861280	19.9	975732	42.2	024268	68709	72657	36
25	837146	22.2	861161	19.9	975985	42.2	024015	68730	72637	35
26	837279	22.2	861041	19.9	976238	42.2	023762	68751	72617	34
27	837412	22.2	860922	19.9	976491	42.2	023509	68772	72597	33
28	837546	22.2	860802	19.9	976744	42.2	023256	68793	72577	32
29	837679	22.2	860682	20.0	976997	42.2	023003	68814	72557	31
30	837812	22.2	860562	20.0	977250	42.2	022750	68835	72537	30
31	9.837945	22.2	9.860442	20.0	9.977503	42.2	10.022497	68857	72517	29
32	838078	22.1	860322	20.0	977756	42.2	022244	68878	72497	28
33	838211	22.1	860202	20.0	978009	42.2	021991	68899	72477	27
34	838344	22.1	860082	20.0	978262	42.2	021738	68920	72457	26
35	838477	22.1	859962	20.0	978515	42.2	021485	68941	72437	25
36	838610	22.1	859842	20.0	978768	42.2	021232	68962	72417	24
37	838742	22.1	859721	20.1	979021	42.2	020979	68983	72397	23
38	838875	22.1	859601	20.1	979274	42.2	020726	69004	72377	22
39	839007	22.1	859480	20.1	979527	42.2	020473	69025	72357	21
40	839140	22.0	859360	20.1	979780	42.2	020220	69046	72337	20
41	9.839272	22.0	9.859239	20.1	9.980033	42.2	10.019967	69067	72317	19
42	839404	22.0	859119	20.1	980286	42.2	019714	69088	72297	18
43	839536	22.0	858998	20.1	980538	42.2	019461	69109	72277	17
44	839668	22.0	858877	20.1	980791	42.1	019209	69130	72257	16
45	839800	22.0	858756	20.1	981044	42.1	018956	69151	72236	15
46	839932	22.0	858635	20.2	981297	42.1	018703	69172	72216	14
47	840064	21.9	858514	20.2	981550	42.1	018450	69193	72196	13
48	840196	21.9	858393	20.2	981803	42.1	018197	69214	72176	12
49	840328	21.9	858272	20.2	982056	42.1	017944	69235	72156	11
50	840459	21.9	858151	20.2	982309	42.1	017691	69256	72136	10
51	9.840591	21.9	9.858029	20.2	9.982562	42.1	10.017438	69277	72116	9
52	840722	21.9	857908	20.2	982814	42.1	017186	69298	72096	8
53	840854	21.9	857786	20.2	983067	42.1	016933	69319	72075	7
54	840985	21.9	857665	20.3	983320	42.1	016680	69340	72055	6
55	841116	21.8	857543	20.3	983573	42.1	016427	69361	72035	5
56	841247	21.8	857422	20.3	983826	42.1	016174	69382	72015	4
57	841378	21.8	857300	20.3	984079	42.1	015921	69403	71995	3
58	841509	21.8	857178	20.3	984331	42.1	015669	69424	71974	2
59	841640	21.8	857056	20.3	984584	42.1	015416	69445	71954	1
60	841771	21.8	856934	20.3	984837	42.1	015163	69466	71934	0
	sine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE II.

Log. Sines and Tangents. (44°) Natural Sines.

65

	Sine.	D. 10''	Cosine.	D. 10''	Tang.	D. 10''	Cotang.	N. sine.	N. cos.	
0	9.841771		9.856934		9.984837		10.015163	69466	71934	60
1	841902	21.8	856812	20.3	985090	42.1	0'4910	69487	71914	59
2	842033	21.8	856690	20.4	985343	42.1	014657	69508	71894	58
3	842163	21.8	856568	20.4	985596	42.1	014404	69529	71873	57
4	842294	21.7	856446	20.4	985848	42.1	014152	69549	71853	56
5	842424	21.7	856323	20.4	986101	42.1	013899	69570	71833	55
6	842555	21.7	856201	20.4	986354	42.1	013646	69591	71813	54
7	842685	21.7	856078	20.4	986607	42.1	013393	69612	71792	53
8	842815	21.7	855956	20.4	986860	42.1	013140	69633	71772	52
9	842946	21.7	855833	20.4	987112	42.1	012888	69654	71752	51
10	843076	21.7	855711	20.4	987365	42.1	012635	69675	71732	50
11	9.843205	21.7	9.855588	20.5	9.987618	42.1	10.012382	69696	71711	49
12	843336	21.6	855465	20.5	987871	42.1	012129	69717	71691	48
13	843466	21.6	855342	20.5	988123	42.1	011877	69737	71671	47
14	843595	21.6	855219	20.5	988376	42.1	011624	69758	71650	46
15	843725	21.6	855096	20.5	988629	42.1	011371	69779	71630	45
16	843855	21.6	854973	20.5	988882	42.1	011118	69800	71610	44
17	843984	21.6	854850	20.5	989134	42.1	010866	69821	71590	43
18	844114	21.5	854727	20.6	989387	42.1	010613	69842	71569	42
19	844243	21.5	854603	20.6	989640	42.1	010360	69862	71549	41
20	844372	21.5	854480	20.6	989893	42.1	010107	69883	71529	40
21	9.844502	21.5	9.854356	20.6	9.990145	42.1	10.009855	69904	71508	39
22	844631	21.5	854233	20.6	990398	42.1	009602	69925	71488	38
23	844760	21.5	854109	20.6	990651	42.1	009349	69946	71468	37
24	844889	21.5	853986	20.6	990903	42.1	009097	69966	71447	36
25	845018	21.5	853862	20.6	991156	42.1	008844	69987	71427	35
26	845147	21.5	853738	20.6	991409	42.1	008591	70008	71407	34
27	845276	21.5	853614	20.6	991662	42.1	008338	70029	71386	33
28	845405	21.4	853490	20.7	991914	42.1	008086	70049	71366	32
29	845533	21.4	853366	20.7	992167	42.1	007833	70070	71345	31
30	845662	21.4	853242	20.7	992420	42.1	007580	70091	71325	30
31	9.845790	21.4	9.853118	20.7	9.992672	42.1	10.007328	70112	71305	29
32	845919	21.4	852994	20.7	992925	42.1	007075	70132	71284	28
33	846047	21.4	852869	20.7	993178	42.1	006822	70153	71264	27
34	846175	21.4	852745	20.7	993430	42.1	006570	70174	71243	26
35	846304	21.4	852620	20.7	993683	42.1	006317	70195	71223	25
36	846432	21.4	852496	20.7	993936	42.1	006064	70215	71203	24
37	846560	21.3	852371	20.8	994189	42.1	005811	70236	71182	23
38	846688	21.3	852247	20.8	994441	42.1	005559	70257	71162	22
39	846816	21.3	852122	20.8	994694	42.1	005306	70277	71141	21
40	846944	21.3	851997	20.8	994947	42.1	005053	70298	71121	20
41	9.847071	21.3	9.851872	20.8	9.995199	42.1	10.004801	70319	71101	19
42	847199	21.3	851747	20.8	995452	42.1	004548	70339	71080	18
43	847327	21.3	851622	20.8	995705	42.1	004295	70360	71059	17
44	847454	21.3	851497	20.8	995957	42.1	004043	70381	71039	16
45	847582	21.2	851372	20.9	996210	42.1	003790	70401	71019	15
46	847709	21.2	851246	20.9	996463	42.1	003537	70422	70998	14
47	847836	21.2	851121	20.9	996715	42.1	003285	70443	70978	13
48	847964	21.2	850996	20.9	996968	42.1	003032	70463	70957	12
49	848091	21.2	850870	20.9	997221	42.1	002779	70484	70937	11
50	848218	21.2	850745	20.9	997473	42.1	002527	70505	70916	10
51	9.848345	21.2	9.850519	20.9	9.997726	42.1	10.002274	70525	70896	9
52	848472	21.1	850493	20.9	997979	42.1	002021	70546	70875	8
53	848599	21.1	850368	21.0	998231	42.1	001769	70567	70855	7
54	848726	21.1	850242	21.0	998484	42.1	001516	70587	70834	6
55	848852	21.1	850116	21.0	998737	42.1	001263	70608	70813	5
56	848979	21.1	849990	21.0	998989	42.1	001011	70628	70793	4
57	849105	21.1	849864	21.0	999242	42.1	000758	70649	70772	3
58	849232	21.1	849738	21.0	999495	42.1	000505	70670	70752	2
59	849359	21.1	849611	21.0	999748	42.1	000253	70690	70731	1
60	849485	21.1	849485	21.0	10.000000	42.1	000000	70711	70.11	0
	Cosine.		Sine.		Cotang.		Tang.	N. cos.	N. sine.	

TABLE III.

## LOGARITHMS OF NUMBERS.

FROM 1 TO 200,

INCLUDING TWELVE DECIMAL PLACES.

N.	Log.	N.	Log.	N.	Log.
1	000000 000090	41	612783 856720	81	908485 018879
2	301029 995664	42	623249 290398	82	913813 852384
3	477121 254720	43	633468 455580	83	919078 092376
4	602059 991328	44	643452 676485	84	924279 286062
5	698970 004336	45	653212 513775	85	929418 925714
6	778151 250384	46	662757 831682	86	934498 451244
7	845098 040014	47	672097 857926	87	939519 252619
8	903089 983992	48	681241 237376	88	944482 672150
9	954242 509439	49	690195 080028	89	949390 006645
10	Same as to 1.	50	Same as to 5.	90	Same as to 9.
11	041392 685158	51	707570 176098	91	959041 392321
12	079181 246048	52	716003 343635	92	963787 827346
13	113943 352307	53	724275 869601	93	968482 948554
14	146128 035678	54	732393 759823	94	973127 853600
15	176091 259056	55	740362 689494	95	977723 605889
16	204119 982656	56	748188 027006	96	982271 233040
17	230448 921378	57	755874 855672	97	986771 734266
18	255272 505103	58	763427 993563	98	991226 075692
19	278753 600953	59	770852 011642	99	995635 194598
20	Same as to 2.	60	Same as to 6	100	Same as to 10.
21	322219 2947	61	785329 835011	101	004321 373783
22	342422 680822	62	792391 699498	102	008600 171762
23	361727 836018	63	799340 549453	103	012837 224705
24	380211 241712	64	806179 973984	104	017033 339299
25	397940 008672	65	812913 356643	105	021189 299070
26	414973 347971	66	819543 935542	106	025305 865265
27	431363 764159	67	826074 802701	107	029383 777685
28	447158 031342	68	832508 912706	108	033423 755487
29	462397 997899	69	838849 090737	109	037426 497941
30	Same as to 3.	70	Same as to 7.	110	Same as to 11.
31	491361 693834	71	851258 348719	111	045322 978787
32	505149 978320	72	857332 496431	112	049218 022670
33	518513 939878	73	863322 860120	113	053078 443483
34	531478 917042	74	869231 719731	114	056904 851336
35	544068 044350	75	875061 263392	115	060397 840354
36	556302 500767	76	880813 592281	116	064457 989227
37	568201 724967	77	886490 725172	117	068185 861746
38	579783 596617	78	892094 602690	118	071882 007306
39	591064 607026	79	897627 091290	119	075546 961393
40	Same as to 4.	80	Same as to 8.	120	Same as to 12.

OF NUMBERS.

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N.	Log.	N.	Log.	N.	Log.
121	082785 370316	148	170261 715395	175	243038 048686
122	086359 830675	149	173186 268412	176	245512 667814
123	089906 111439	150	176091 259056	177	247973 266362
124	093421 685162	151	178976 947293	178	250420 002309
125	096910 013008	152	181843 587945	179	252853 030980
126	100370 545118	153	184691 430818	180	255272 505103
127	103803 720956	154	187520 710836	181	257678 574869
128	107209 969648	155	190331 698170	182	260071 387585
129	110589 710299	156	193124 588354	183	262451 089730
130	Same as to 13.	157	195899 652409	184	264817 823010
131	117271 295656	158	198657 086954	185	267171 728403
132	120573 931206	159	201397 124320	186	269512 944218
133	123851 640937	160	204119 982656	187	271841 606536
134	127104 798365	161	206825 876032	188	274157 849264
135	130333 768495	162	209515 014543	189	276461 804173
136	133538 908370	163	212187 604404	190	278753 600953
137	136720 567156	164	214843 848048	191	281033 367248
138	139879 086401	165	217483 944214	192	283301 228704
139	143014 800254	166	220108 088040	193	285557 399008
140	146128 035678	167	222716 471148	194	287801 729930
141	149219 112655	168	225309 281726	195	290054 611362
142	152288 344383	169	227886 704614	196	292256 071356
143	155336 037465	170	230448 921378	197	294466 226162
144	158362 492095	171	232996 110392	198	296665 190262
145	161368 002235	172	235528 446908	199	298853 076410
146	164352 855784	173	238046 103129		
147	167317 334748	174	240549 248283		

LOGARITHMS OF THE PRIME NUMBERS

FROM 200 TO 1543,

INCLUDING TWELVE DECIMAL PLACES.

N.	Log.	N.	Log.	N.	Log.
201	303196 057420	277	442479 769064	379	578639 209968
203	307496 037913	281	448706 319905	383	583198 773968
207	315970 345457	283	451786 435524	389	589949 601326
209	320146 286111	293	466867 620354	397	598790 503763
211	324282 455298	307	487138 375477	401	603144 372620
223	348304 863048	311	492760 389027	409	611723 308007
227	356025 857193	313	495544 337546	419	622214 022966
229	359835 482340	317	501059 262218	421	624282 095836
233	367355 921026	331	519827 993776	431	634477 270161
239	378397 900948	337	527629 900871	433	636487 896353
241	382077 042575	347	540329 474791	439	642424 520242
251	399673 721481	349	542825 426959	443	646403 726223
257	400933 123331	353	47774 705388	449	652246 341003
263	419955 748490	359	555094 448578	457	659916 200070
269	429752 280032	367	564666 064252	461	663700 925390
271	432969 290874	373	571708 831809	463	665580 991018

N.	Log.	N.	Log.	N.	Log.
467	6.9310 880566	821	914343 157119	1171	0.8856 895072
479	680335 513414	823	915399 835212	1181	0.2249 807613
487	687228 961215	827	917505 509553	1187	0.7447 0 718955
491	691081 492123	829	918554 530550	1193	0.7664 0 443670
499	695100 545623	839	923761 960829	1201	0.9543 007385
503	701567 985056	853	930949 031168	1213	0.8383 0 800845
509	706717 782337	857	932980 821923	1217	0.8529 0 578210
521	716837 723300	859	933993 163331	1223	0.8742 0 458017
523	718501 688867	863	936010 795715	1229	0.8955 1 882866
541	733197 265107	877	942399 593356	1231	0.9025 8 052912
547	737987 326333	881	944975 908412	1237	0.9236 9 699609
557	745855 195174	883	945960 703578	1249	0.9656 2 438356
563	750508 394851	887	947923 619832	1259	1.0002 5 729204
569	755112 266395	907	957607 287060	1277	1.0519 0 896808
571	756636 108243	911	959518 376973	1279	1.0687 0 542460
577	761175 813156	919	963315 511386	1283	1.0822 6 656362
587	768638 101248	929	968015 713994	1289	1.1025 2 917337
593	773054 693364	937	971739 590888	1291	1.1092 6 242517
599	777426 822389	941	973589 623427	1297	1.1293 9 986066
601	778874 472002	947	976349 979003	1301	1.1427 7 296540
607	783138 691075	953	979092 900638	1303	1.1494 4 415712
613	787460 474518	967	985426 474083	1307	1.1627 5 587564
617	790285 164033	971	987219 229908	1319	1.2024 4 795568
619	791690 649020	977	989894 563719	1321	1.2090 2 817604
631	800029 359244	983	992553 517832	1327	1.2287 0 922849
641	806858 029519	991	996073 654485	1361	1.3385 8 125188
643	808210 972924	997	998695 158312	1367	1.3576 8 514554
647	810934 280369	1009	003891 166237	1373	1.3767 0 537223
653	814913 181275	1013	005609 445360	1381	1.4019 3 678544
659	818885 414594	1019	008174 184006	1399	1.4581 7 714122
661	810201 459486	1021	009025 742087	1409	1.4891 0 994096
673	828015 064224	1031	013258 665284	1423	1.5320 4 896557
677	830588 668635	1033	014100 321520	1427	1.5442 4 012366
683	834420 703682	1039	016615 547557	1429	1.5503 2 228774
691	839478 047374	1049	020775 488194	1433	1.5624 6 402184
701	845718 017967	1051	021602 716028	1439	1.5806 0 793919
709	850646 235183	1061	025715 383901	1447	1.6046 8 531109
719	856728 890383	1063	026533 264523	1451	1.6166 7 412427
727	861534 410359	1069	028977 705209	1453	1.6226 5 614286
733	865103 974742	1087	036229 544086	1459	1.6405 5 291883
739	868644 488395	1091	037824 750588	1471	1.6761 2 672629
743	870988 813761	1093	038620 161950	1481	1.7055 5 058512
751	855639 937004	1097	040206 627575	1483	1.7114 1 151014
757	879095 879500	1103	042595 512440	1487	1.7231 0 968489
761	881384 656771	1109	044931 546119	1489	1.7289 4 731332
769	885926 339801	1117	048053 173116	1493	1.7405 9 807708
773	888179 493918	1123	050379 756261	1499	1.7580 1 632866
787	895974 732359	1129	052693 941925	1511	1.7926 4 464329
797	901458 321396	1151	051075 323630	1523	1.8269 9 903324
809	907948 521612	1153	061829 307295	1531	1.8497 5 190807
811	909020 854211	1163	065579 714728	1543	1.8836 5 926053

## AUXILIARY LOGARITHMS.

N.	Log.	N.	Log.
1.009	003891166237	1.019	000390689248
1.008	003460532110	1.003	000347296884
1.007	003029470554	1.007	000303899784
1.006	002598080685	1.003	00260498547
1.005	002166051756	1.005	00217092970
1.004	001733712775	1.004	00173683057
1.003	001300933020	1.003	000130268804
1.002	000867721529	1.002	00008685211
1.001	000434077479	1.001	000043427277

## C

N.	Log.	N.	Log.
1.00009	000039083266	1.00009	00003908628
1.00008	000034740691	1.00008	000003474338
1.00007	000030398072	1.00007	000003040047
1.00006	000026055410	1.00006	000002605756
1.00005	000021712704	1.00005	000002171464
1.00004	000017371430	1.00004	000001737173
1.00003	000013028638	1.00003	000001302880
1.00002	000008685802	1.00002	000000868587
1.00001	000004342923	1.00001	000000434294

N.	Log.
1.0000001	000000043429 (a)
1.00000031	000000004343 (o)
1.000000001	000000000434 (p)
1.0000000001	000000000043 (q)

$$m=0.4342944819 \quad \log. -1.637784298.$$

By the preceding tables—and the auxiliaries *A*, *B*, and *C*, we can find the logarithm of any number, true to at least ten decimal places.

But some may prefer to use the following direct formula, which may be found in any of the standard works on algebra:

$$\text{Log. } (z+1) = \text{log. } z + 0.8685889638 \left( \frac{1}{2z+1} \right)$$

The result will be true to twelve decimal places, if *z* be over 2000.

The log. of composite numbers can be determined by the combination of logarithms, already in the table, and the prime numbers from the formula.

Thus, the number 5083 is a prime number, find its logarithm.

We first find the log. of the number 3082. By factoring, we discover that this is the product of 46 into 67.

Log. 46,	1.6627578316
Log. 67,	1.8260748027
Log. 3082	3.4888326343
Log. 3083=3.4888326343+	$\frac{0.8685889638}{6165}$

## NUMBERS AND THEIR LOGARITHMS,

OFTEN USED IN COMPUTATIONS.

Circumference of a circle to dia. 1	} = 3.14159265	Log. 0.4971499
Surface of a sphere to diameter 1		
Area of a circle to <i>radius</i> 1	} = .7853982	—1.8950899
Area of a circle to diameter 1		
Capacity of a sphere to diameter 1	= .5235988	—1.7189986
Capacity of a sphere to radius 1	= 4.1887902	0.6220886
Arc of any circle equal to the radius	= 57°29'578	1.7581226
Arc equal to radius expressed in sec.	= 206264"8	5.3144251
Length of a degree, (radius unity)	= .01745329	—2.2418773
12 hours expressed in seconds,	= 43200	4.6354837
Complement of the same,	= 0.00002315	—5.3645163
360 degrees expressed in seconds,	= 1296000	6.1126050

A gallon of distilled water, when the temperature is 62° Fahrenheit, and Barometer 30 inches, is  $277.\frac{274}{1000}$  cubic inches.

$$\sqrt{277.274} = 16.651542 \text{ nearly.}$$

$$\sqrt{\frac{277.274}{.775398}} = 18.78925284$$

$$\sqrt{231} = 15.198684.$$

$$\sqrt{282} = 16.792855.$$

$$\sqrt{\frac{282}{.785398}} = 18.948708.$$

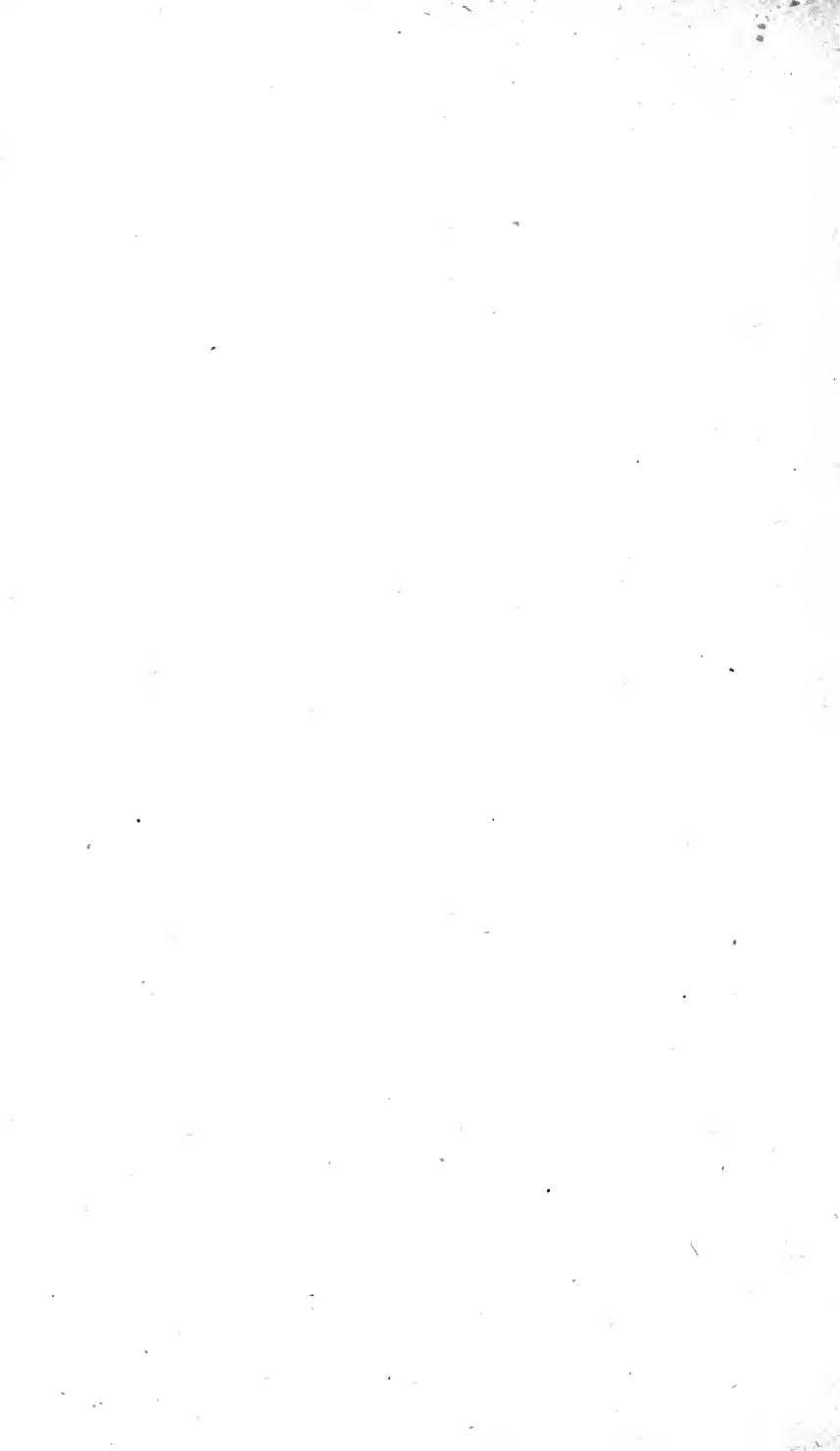
The French Metre = 3.2808992, English *feet* linear measure, = 39.3707904 inches, the length of a pendulum vibrating seconds.















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